## Friction measurements on phaseseparated thin films with a modified atomic force microscope

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THE study of chemical phase separation in multicomponent thin organic films typically involves the addition of a dye which is selectively more soluble in one of the phases, thereby making it possible to probe the domain structures by fluorescence microscopy  $^{1-4}$ . The resolution of this approach is generally limited to tens of micrometres. The atomic force microscope, on the other hand, has recently proved useful for imaging organic thin films down to the atomic scale  $^{5-9}$ , but this technique provides details of the overall film topography, rather than the chemical composition. Here we show that the recently developed friction force microscope  $^{10-13}$ , which simultaneously measures both the normal and lateral forces on the scanning tip, can be used to image and identify compositional domains with a resolution of  $\sim$ 5 Å. Although the topography of the individual domains can be imaged with a standard atomic force microscope, it is the additional information provided by the friction measurement that allows them to be chemically differentiated.

Scanning probe microscopes such as the scanning tunnelling microscope (STM) and atomic force microscope (AFM) have been used to analyse surfaces on many levels, from molecular arrangements at interfaces to electronic structures in semiconductors. These methods are rather insensitive to chemical composition; with the STM, electronic states around the Fermi energy are probed, whereas AFM images are interpreted as maps of the total charge density 15,16. Some elemental characterization has been possible with scanning tunnelling spectroscopy on samples such as GaAs<sup>17</sup>, adsorbates on semiconductors and metals Por more detailed information, core levels have to be sensed, and this is not possible with the STM 18,20.

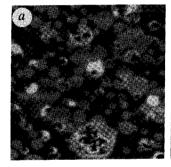
Frictional forces can influence AFM image contrast when it is operating in the repulsive contact mode 10,11. Those measurements show that frictional forces vary on an atomic scale and that a friction force coefficient for a tungsten tip on a graphite sample can be determined 10. These observations led to the construction of a friction force microscope (FFM) where both the normal and lateral forces are measured simultaneously but separately over homogeneous surfaces 11-13. In this instrument, the bending and torsion of a cantilever-type spring are correlated with the normal and lateral forces exerted by the sample, while the fine resolution of an AFM is maintained. Here, we extend the use of the FFM to samples composed of distinctly different chemical species and demonstrate that the FFM can distinguish between these components.

From macroscopic measurements it is well known that friction depends strongly on material. Various types of apparatus have been used to measure frictional properties as a function of temperature, sliding velocity and normal load<sup>21-23</sup>. The FFM represents a simplified device for experiments on sliding friction under boundary conditions: an idealized single asperity on a thin multilayer film. With the FFM the lateral (friction) forces acting on the probing tip can be measured over a localized

contact area of a few square nanometres between probing tip and sample.

To demonstrate that on the nanometre scale, frictional properties are sensitive to changes in surface properties on chemical modification<sup>24,25</sup>, we have chosen Langmuir-Blodgett (LB) films because of their solid-like behaviour, their use in previous work on boundary lubrication<sup>21</sup> and their well-defined, non-random structure<sup>26</sup>, so that the results would be straightforward to interpret. But the FFM technique is applicable to a wide range of materials, for the study of material-specific friction and as a means of identifying materials on this very small scale from their different frictional responses. Few, if any, other techniques can probe material properties directly and nondestructively on so small a scale with such good resolution ( $\sim$ 5 Å). Its usefulness has been demonstrated on layered materials such as mica<sup>12</sup> and graphite<sup>10</sup>. Here we demonstrate that the technique can be used to distinguish between components in a multicomponent system, as we assess not only the differential friction between two molecular classes (fluorocarbon and hydrocarbon), but also that between organic adsorbate and inorganic (silicon) substrate.

Figure 1a shows a  $5.0 \times 5.0 \, \mu m^2$  top-view AFM image of a 50:50 molar mixture of arachidic acid and partially fluorinated carboxylic acid bound ionically to a common cationic polymer (see Fig. 2). Round island-like structures are observed, 100 nm to 1  $\mu$ m in diameter and  $\sim 1.6$  nm in height above the surrounding film. We assign the higher circular domains in Fig. 1a to the hydrocarbons and the surrounding flat film to the fluorocarbons, partly on the basis of their different molecular lengths and partly because of their different frictional behaviours (see below). With molecular lengths of  $\sim 2.5$  nm and  $\sim 2.0$  nm for the arachidic acid and the fluorocarbon-terminated acid,



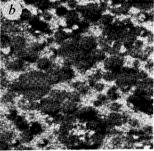


FIG. 1 The LB films are prepared as described elsewhere  $^{37,38}$ . Briefly, a 1:1 molar mixture of perhydro arachidic acid ( $C_{19}H_{39}COOH$ ) and partially fluorinated carboxylic acid, ( $C_9F_{19}C_2H_4OC_2H_4COOH$ ), is introduced in organic solvent to an aqueous subphase containing poly(4-vinyl-N-methylpyridinium) cationic polymer. The complex of anionic surfactants and cationic polymer is transferred by the LB technique onto a hydrophobized silicon (100) surface to form a bilayer system. Pretreatment of the silicon surface is explained elsewhere<sup>39</sup>. The deposition of the LB films is carried out in a Langmuir trough at room temperature. The FFM cantilevers used here are microfabricated from Si<sub>3</sub>N<sub>4</sub> and have normal and torsion spring constants of  $0.2\,N\,m^{-1}$  and  $200\,N\,m^{-1}$ , respectively. The resolution of the instrument is  $0.1\,\text{\AA}$  in the normal direction and  $10^{-10}\,N$  in the friction force. The measurements are done at minimal normal load, of the order of  $10^{-9}$ – $10^{-8}$  N. a, AFM image  $(5 \times 5 \,\mu\text{m}^2)$  of the surface of a bilayer prepared from a mixture of the fluorocarbon and hydrocarbon carboxylates (1:1 molar). The image represents the topography. The circular domains are assigned to the hydrocarbon component and the surrounding flat film to the partially fluorinated component. The difference in height between these two regions is  $\sim$ 1.6 nm. Holes of ~5 nm in depth are observed only in the 'island-like' circular hydrocarbon domains, whereas the fluorinated film remains fairly uniform and unbroken. b, Friction force measurement (also covering  $5 \times 5 \ \mu m^2$ ) done simultaneously with the topography image in a. The lateral force image indicates higher friction (brighter contrast) over the fluorinated regions. Highest friction is measured on the silicon surface (at the bottom of the holes in the film). No difference in contrast (friction) is observed between the hydrocarbon layers of different height.

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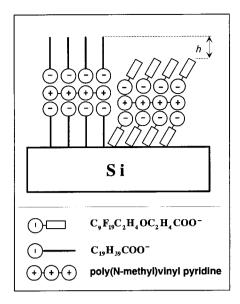


FIG. 2 Schematic view of the LB bilayer system imaged by AFM in Fig. 1. The 'h' represents the height difference between the hydrocarbon and fluorocarbon species (see text).

respectively, we expect a difference in height of  $\sim 1.0$  nm between domains of the two components in this bilayer LB system. Figure 1a shows a step height from flat film to island of 1.6 nm; the slightly greater difference could be due to a greater tilt angle in the fluorocarbon domains<sup>27</sup>.

In other experiments, AFM images have been recorded on LB bilayer films composed of a single carboxylic acid component, one from arachidate and one from the partially fluorinated carboxylate<sup>9</sup>. The fluorinated acid film contains fewer defects than the arachidic acid film9. These results support the assignment of the circular domains to the hydrocarbon component, as holes are observed only in the circular domains in the mixed films. These holes are ~5.0 nm in depth, consistent with the thickness of a bilayer. Furthermore, increasing the force while scanning disrupts the hydrocarbon but not the fluorinated areas, in both the one- and two-component films. The fluorinated sites show good resistance to rupture during sliding, in agreement with tribology experiments using macroscopic measurement techniques<sup>23</sup>

Lateral force measurements (Fig. 1b) made simultaneously with the topography measurements (Fig. 1a) indicate roughly four times higher friction over the fluorinated regions than over the hydrocarbon regions. Holes in the film reveal the silicon substrate. The silicon, appearing as dark (low) areas in the topography image, shows a friction force a factor of 10 higher than the hydrocarbon domains in the lateral force image. This difference in friction agrees well with other experiments on both macroscopic and nanometre scales<sup>28-30</sup>. In sum, from the FFM measurements on these phase-separated LB films, the relative frictions of the hydrocarbon, fluorocarbon and silicon surfaces are shown to be 1:4:10. In the range of nondestructive forces applied in this study,  $\sim 10^{-9}-10^{-8}$  N, no dependence of the friction on load is observed.

The differences in friction are not due to changes in topography. This is demonstrated particularly well by the ability of the friction measurements to identify the scattered islands of extraneous' material sitting atop hydrocarbon domains. Whereas normal force measurement determines only the geometry of the island, lateral force measurement determines its composition. The frictional response of the island corresponds to that of the circular hydrocarbon domains, thereby allowing it to be identified as hydrocarbon in nature. This assignment would not be possible with the normal AFM alone.

The friction on the fluorinated areas is higher than on the hydrocarbons. From the performance of fluorine-containing lubricants, such as teflon (PTFE), a reduction in friction might be expected. But it is known from surface force apparatus

experiments<sup>23</sup> that fluorinated LB films have larger shear strengths (friction force divided by the real area of contact in shear) than their hydrogen-containing counterparts. The higher friction measured with the FFM over the fluorocarbon is attributed, at least in part, to the greater stiffness and closer packing<sup>31</sup> of the fluorocarbon moiety.

These observations of friction and robustness on the scale of nanometres can be applied to the study of tribology, particularly boundary lubrication. Boundary lubrication, as established by , deals with the layers of lubricant closest to the solid surfaces undergoing frictional contact, and is of importance in most surface-on-surface sliding mechanisms. The particular advantage of the fluorinated film is its resistance to rupture as known from both the surface force apparatus and AFM measurements. The good performance of fluorocarbons as lubricants can therefore be attributed to high stability towards applied stress, and a reduced friction (compared with unlubricated surfaces) which reduces the wear to very low values (reduction of  $10,000)^{33}$ 

In nanometre-scale friction and topography measurements, local elasticity plays a role. In our on-going work, we measure a greater elasticity on the molecular scale for the hydrocarbon moieties than the fluorocarbon moieties, evidence for the increased stiffness of fluorinated segments<sup>31</sup>. This is consistent with the higher in-plane cohesive binding that we observe in the fluorocarbon domains, also attributed to the higher barriers for trans/gauche isomerization in the stiffer fluorocarbon chains<sup>34,35</sup>. Even though our observation of lower friction on the hydrocarbon film suggests that hydrocarbon acids could be more effective lubricants than the fluorinated compounds, our comparative measurements show that pure arachidate films and domains are more disrupted by sliding friction than their fluorocarbon counterparts<sup>9,36</sup>. We propose that a good lubricating mixture would have a fluorinated component to offer good rupture resistance and a hydrocarbon component to contribute low friction, as in the mixture used here. 

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