

# Tsunami Hazard Assessment of Bainbridge Island, Washington

## Project Report

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**Vasily V. Titov, Diego Arcas, Christopher W. Moore**  
Pacific Marine Environment Laboratory, NOAA, Seattle

**Randall J. LeVeque, Loyce M. Adams, Frank I. González**  
University of Washington

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[http://depts.washington.edu/ptha/WA\\_EMD\\_Bainbridge/](http://depts.washington.edu/ptha/WA_EMD_Bainbridge/)

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# 1 Introduction

This report documents the results of a study supported by the Washington State Emergency Management Division of the tsunami hazard along the coast of Bainbridge Island, WA. One earthquake source from the Seattle Fault and one from the Cascadia Subduction Zone were considered. Results include inundation depths and times of arrival that will be useful to coastal communities, as well as tsunami current speeds and momentum flux.

In this collaborative project between the UW Tsunami Modeling group and the NOAA Center for Tsunami Research at PMEL, a comparison has also been performed between the results obtained by the two groups using two different computer codes:

- The UW group used GeoClaw Version 5.5.0 [4].
- The PMEL group used MOST GPU v2.6.3.

Both software packages solve the two-dimensional shallow water equations over variable topography and bathymetry with the addition of bottom friction in the form of a Manning coefficient. Identical sea floor deformations were used by the two groups to initiate the tsunami. The same finest grid resolution ( $1/3$  arcsecond resolution in both longitude and latitude) was also used around the study region described in Section 2.

In principle the two codes should produce very similar results. Exact agreement is not expected because there are numerous differences in the numerical methods that are implemented to discretize the shallow water equations, in the algorithms used to handle wetting and drying at margins of the flow, in the coarser level grids that surround the study region, and in numerous other details. These differences are described in more detail in Sections 6 and 7. In addition, slightly different values of the Manning coefficient were used (0.025 for GeoClaw and 0.03 for MOST).

The conclusion of our comparison is that the two codes do give very similar results, well within the expected variance in view of the model differences. This is discussed in more detail in Section 8. Some sensitivity studies were also performed to explore the effect of varying parameters within a single model, see Section C. We found that variations in GeoClaw results when the finest computational grid resolution is varied from  $1/3''$  to  $2/3''$  or  $1/6''$ , or when the Manning coefficient is varied to nearby values, are roughly of the same magnitude as the variations between the GeoClaw and MOST results. Given that the two models discretize the topography (and the shallow water equations) differently, and that different values of the Manning coefficient were used in the simulations, this suggests that variations between the models are within acceptable limits.

This is an important verification exercise for each code, and is particularly important in view of the fact that the PMEL and UW groups are, in other on-going projects, modeling different portions of the Washington State coastline in support of the new generation of hazard maps being produced by DNR. This study suggests that the results produced by the two groups should be similar also in other regions, and hence seamless integration of the modeling results into hazard products should be possible with little concern that different results would be obtained by the other group.

## 2 Study area

Figure 1 shows the study area surrounding Bainbridge Island. [[TODO: Add figure and discuss computational domain for each source, grid resolutions.]]

Figure 1: Add figure of study area with locations marked.

### 3 Earthquake Sources

Two earthquake sources were considered for this study: a Cascadia Subduction Zone (CSZ) megathrust event with moment magnitude Mw 9.0 (denoted CSZ-L1), and a potential Seattle Fault rupture denoted SF-L.

The CSZ-L1 event creates very large waves along the outer coast and a substantial wave that propagates into the Strait of Juan de Fuca (SJdF) and into Puget Sound, affecting parts of Bainbridge Island, starting about 2 hours after the earthquake. No subsidence or uplift is produced by CSZ-L1 in Puget Sound. There is little significant flooding on the island from this event, but some very strong currents are generated, particularly in Agate Pass at the north end of the island and around Point White in the south; see Figure 4.

The Seattle Fault cuts across Puget Sound (through Seattle and Bainbridge Island) and can create a tsunami that affects the island immediately. The northern portion of the island subsides, increasing the level of flooding in Eagle Harbor and other coastal regions to the north. The southern portion of the island is uplifted and very little inundation is observed in these regions. However, very strong currents are observed in many locations all around the island; see Figure 3.

These two earthquake sources are described in more detail in the sections below. Other potential sources have not been considered in this study. In particular the smaller Seattle Fault event SF-S that has been used in some past tsunami studies in Puget Sound was found to have negligible impact and was not modeled in detail. Several other fault zones cross Puget Sound, but potential sources from these faults have not been considered.

#### 3.1 Cascadia megathrust event CSZ-L1

The probability that an earthquake of magnitude 8 or greater will occur on the Cascadia Subduction Zone (CSZ) in the next 50 years has been estimated to be 10-14% (Petersen, et. al., 2002 [9]). The last such event occurred in 1700 (Satake, et al., 2003 [10]; Atwater, et al., 2005 [1]) and future events are expected to generate a destructive tsunami that will inundate Washington Pacific coast communities within tens of minutes after the earthquake main shock. Waves will travel through the Strait of Juan de Fuca and start arriving at Bainbridge Island roughly 2 hours and 15 minutes after the earthquake.

The potential CSZ event used in this study is the L1 scenerio developed by Witter, et al. (2013) [12]; crustal deformation for the region of interest is shown in Figure 2. The L1 source is one of 15 seismic scenarios used in a hazard assessment study of Bandon, OR, based on an analysis of data spanning 10,000 years. This scenario has been adopted by Washington State as the “worst considered case” for many inundation modeling studies and subsequent evacuation map development; it is used because the standard engineering planning horizon is 2500 years and Witter, et al. in 2013 [12] estimated that L1 has a mean recurrence period of approximately 3333 years, with the highest probability of occurrence of all events considered with magnitude greater than Mw9.

The original L1 source was developed for studies on the Oregon coast and was truncated at around 48N. An extension of this developed by PMEL has been used in this study. The seafloor deformation is shown in Figure 2.

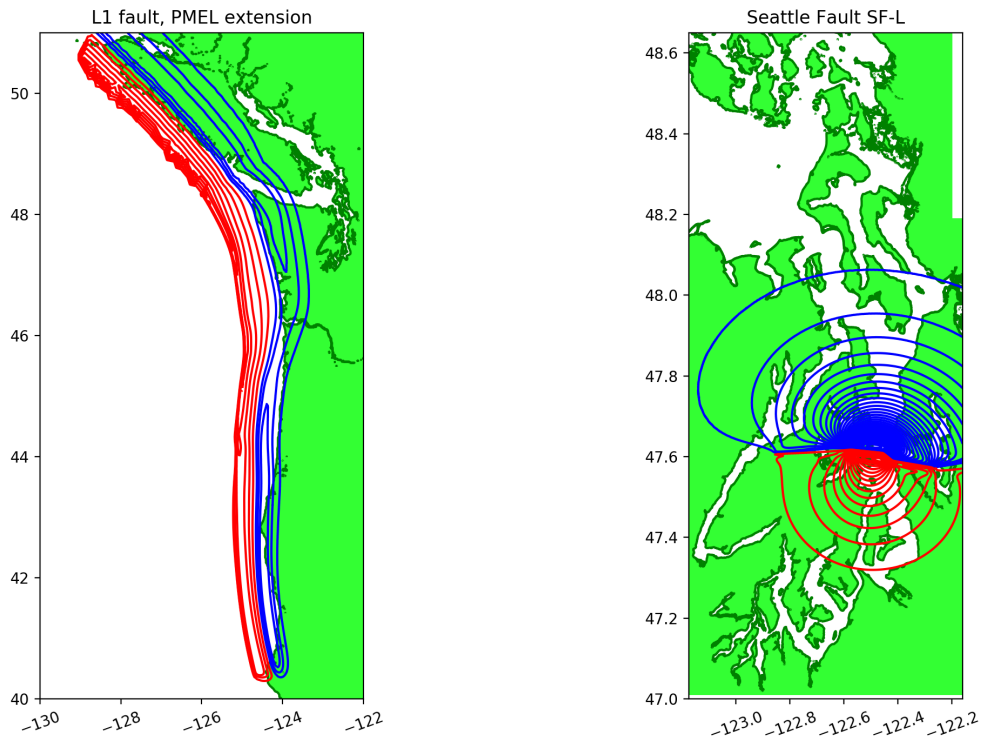


Figure 2: Left: Surface deformation of the L1 source, with maximum uplift 15.08 m and maximum subsidence  $-3.98$  m. Red contours show uplift (2 meter interval), blue contours show subsidence (1 meter interval). Right: Surface deformation of the SF-L source, with maximum uplift 8.37 m and maximum subsidence  $-1.78$  m. Red contours show uplift at levels 0.5, 1, 1.5, ... meters, blue contours show subsidence at levels  $-0.05$ ,  $-0.1$ , ... meters. [[TODO: Add zoomed view of SF-L around Bainbridge.]]

## 3.2 Seattle Fault event SF-L

Figure 2 shows contours of uplift and subsidence due to a hypothetical event on the Seattle fault that we denote by SF-L. Earlier tsunami hazard studies have referred to this as a Mw 7.3 event. However, when we tried to recreate the deformation field by applying the Okada model to the subfault parameters listed in [3], we determined that the magnitude should be Mw 7.54, as discussed in Appendix E of the Snohomish County report, [7]. Regardless of the proper magnitude, we are using the deformation file provided by PMEL that has been used for the previous tsunami hazard analyses of Everett [3].

Due to uncertainty about the magnitude, in [7] the SF-L notation was adopted for this larger Seattle Fault scenario, and we continue to use that here. The deformation was originally chosen to match observed uplift and subsidence at a few points around Puget Sound. Since the original specification of this deformation, many new observations have been made and improved models for the subfault geometry have also been produced. A new model for SF-L is now under development and in the future this could perhaps be used to update the results of the current study.

A smaller Seattle Fault scenario (SF-S) was also initially considered, but found to produce a very small tsunami.

## 4 Topography and Bathymetry

### 4.1 1/3 Arc-second DEMs

Output from the model was requested at grid points spaced 1/3" in longitude and 1/3" in latitude, with the points aligned with cell centers of the 1/3" DEM files that are available for the Puget Sound region. (Note that 1/3" in latitude is approximately 10.3 m. At this latitude, 1/3" in longitude is approximately 6.9 m).

Several topography DEMs provided by NCEI have been used in this study. The Puget Sound 1/3" DEM covers the Bainbridge Island region. In addition, the Port Townsend 1/3" DEM and the Strait of Juan de Fuca 1/3" DEM are used for coverage of the Strait, and etopo1 data (1 arcminute) is used for the portion of the Pacific Ocean needed for modeling the L1 source.

## 5 Modeling uncertainties and limitations

Both MOST and GeoClaw use the shallow water equations to model the tsunami, which is an approximation of the three-dimensional fluid dynamics, but one that has been found to be sufficiently accurate for inundation studies of this nature in previous studies, including validation and benchmarking workshops. However, it is only an approximation to the correct physics. A number of other assumptions or approximations are also made in both models, as summarized below.

### 5.1 Tide stage and sea level rise

The simulations were conducted with the background sea level set to MHW. This value is conservative, in the sense that the severity of inundation will generally increase with a higher background sea level. Larger tide levels do occasionally occur, but the assumption of MHW is standard practice in studies of this type. Potential sea level rise over the coming decades was not taken into account in this modeling.

### 5.2 Subsidence and uplift

The Seattle Fault cuts across Bainbridge Island, and so the SF-L event induces significant subsidence to the north and uplift to the south of the fault. This ground motion is taken into account in both tsunami

models, and it is the underwater vertical motion that generates the tsunami. For both events, the details of the motion depend on the hypothetical earthquake source used, and this is the biggest source of uncertainty in the model results since the next earthquake may be very different from the ones that have been modeled.

### 5.3 Structures

Buildings were not included in the simulations, the topographic DEMs provided for this study are “bare earth”. The presence of structures will alter tsunami flow patterns and generally impede inland flow. To some extent the lack of structures in the model is therefore a conservative feature, in that their inclusion would generally reduce inland penetration of the tsunami wave. However, as in the case of the friction coefficient, impeding the flow can also result in deeper flow in some areas. It can also lead to higher fluid velocities, particularly in regions where the flow is channelized, such as when flowing up streets that are bounded by buildings.

### 5.4 Bottom friction

Mannings coefficient of friction was set to 0.025 in GeoClaw and to 0.03 in MOST, standard values used in tsunami modeling that corresponds to gravelly earth. This choice is conservative in some sense, because the presence of trees, structures and vegetation would justify the use of a larger value, which might tend to reduce the inland flow. On the other hand, larger friction values can lead to deeper flow in some areas, since the water may pile up more as it advances more slowly across the topography. A sensitivity study varying the Manning coefficient presented in Section C.2.

### 5.5 Tsunami modification of bathymetry and topography

Severe scouring and deposition are known to occur during a tsunami, undermining structures and altering the flow pattern of the tsunami itself. Again, this movement of material requires an expenditure of tsunami energy that tends to reduce the inland extent of inundation. On the other hand, if natural berms or ridges along the coastline (or man-made levies or dikes) are eroded by the tsunami, then some areas can experience much more extensive flooding. There is no erosion or deposition included in the simulations presented here.

## 6 The GeoClaw model

The GeoClaw model is part of Clawpack [4], and has undergone extensive verification and validation (e.g. [2, 8]), and has been accepted as a validated model by the U.S. National Tsunami Hazard Mitigation Program (NTHMP) after conducting multiple benchmark tests as part of an NTHMP benchmarking workshop [6].

GeoClaw uses finite volume methods with adaptive mesh refinement. The finest grid resolution near regions of interest was set to the desired resolution of  $1/3''$  by  $1/3''$ . The specified topography DEM files is viewed as providing pointwise values. From these values a piecewise bilinear interpolating function is constructed in two dimensions and this function is integrated over the finite volume cells actually used in the computation. The finest grid was aligned so that cell centers agree with DEM points, but the actual topography value used by GeoClaw in each cell is an average of the piecewise bilinear function in this cell and will not agree exactly with the DEM value at the cell center.

Away from the study region, coarser computational grids are used...

[[TODO: Describe other things specific to this model.]]



## 7 The MOST model

MOST (Method Of Splitting Tsunami) is a suite of numerical simulation codes to simulate three processes of tsunami evolution: generation by earthquake, transoceanic propagation, and inundation onto dry land. The model uses finite difference numerical scheme to solve the nonlinear shallow water equation (Titov and Gonzalez, 1997; Titov et al., 2016). The MOST model has been extensively tested against a number of laboratory experiments and benchmarks (Synolakis et al., 2007; Titov and Gonzalez, 1997; Titov and Synolakis, 1998; Titov et al., 2016) as part of the NSF-funded tsunami modeling benchmark workshops. Additional testing have been conducted for MOST as part of the operational testing and evaluation for implementation into NOAA Tsunami Warning System operational tsunami forecast as part Short-term Inundation Forecast for Tsunamis (SIFT) capability of the Tsunami Warning Centers (Titov et al., 2016). The MOST has been operational forecast model at NOAAs TWCs since 2012.

MOST uses a set of three nested grids, referred to as A, B, and C grids, each of which becomes successively finer in resolution as they telescope into the community of interest. A separate propagation model was used to compute the propagation from the L1 source offshore Cascadia and tsunami propagation into the Strait of Juan de Fuca and further into the Puget Sound. The propagation model is run with 34 arc-second resolution. The offshore area is covered by the largest and lower-resolution A grid with the resolution of 30 arc-seconds, grid B of 2 arc-seconds. The highest resolution C grids has the same resolution (1/3 arc-second) and extent for both models.

## 8 Results and model comparison

### 8.1 Maximum depth and speed maps

The primary products of this work that will go into hazard maps produced by DNR are the maximum flooding depth over the entire tsunami event, at each point on shore, and the maximum flow speed, both at points on shore and in the harbors and water ways surrounding the island. Hence a comparison of these maxima is of primary interest. Figures 3 and 4 show the results for the SF-L and CSZ L1 event respectively.

In the appendices we present more detailed view of these comparisons over a few regions of particular interest, along with some selected transects to make it easier to compare and judge the results. In addition, time series of the depth (or water surface) and speed at selected synthetic gauge locations provide a way to compare the time evolution of the different simulations.

In general we have found excellent agreement between results produced by the two different codes. As we expected, the water depth generally agrees better than the speeds, both in terms of maximum values and in the time series at gauge locations. It is well known that current speeds vary much more dramatically in both space and time than fluid depth [?]. [\[\[TODO: Cite NTHMP currents workshop paper, what else?\]\]](#) For example, vortices generated at a harbor entrance produce concentrated regions of very high velocity even though the surface elevation may differ only slightly from the surrounding water. The path that a vortex takes away from the point of generation can be very sensitive to small changes in the flow, and may result in very different maximum speed or time series at any given point if the input data is changed slightly, or if the numerical method used to compute the flow is changed. As a result of this, one can identify several points where GeoClaw and MOST produce quite different speeds. In general, however, the overall patterns of maximum speed in a given region are very similar between the two codes.

To help determine whether the differences seen between the GeoClaw and MOST results are within reasonable limits, we have also performed some sensitivity studies in which one of the codes (GeoClaw) is used to simulate a Seattle Fault tsunami over a restricted portion of the Island, using a variety of slightly perturbed data. In Section C.1 we vary the resolution of the finest computational grid (from the requested 1/3 arcsecond resolution to 1/6 or 2/3 arcseconds). In Section C.2 the Manning coefficient of friction is varied from the value  $n = 0.025$  used in GeoClaw for this study to values  $n = 0.02$  and  $n = 0.03$ . The general pattern of the results is fairly robust to each of these changes, which gives some confidence in the

general validity of modeling results based on the particular set of parameters specified for this study.

Moreover, the differences between the GeoClaw and MOST results when using essentially the same set of parameters are often smaller than the differences induced by the parameter variations used in these sensitivity studies. This gives confidence that the two software packages are correctly implemented and are both giving a good approximation to the true solution of the shallow water equations with the specified set of parameters.

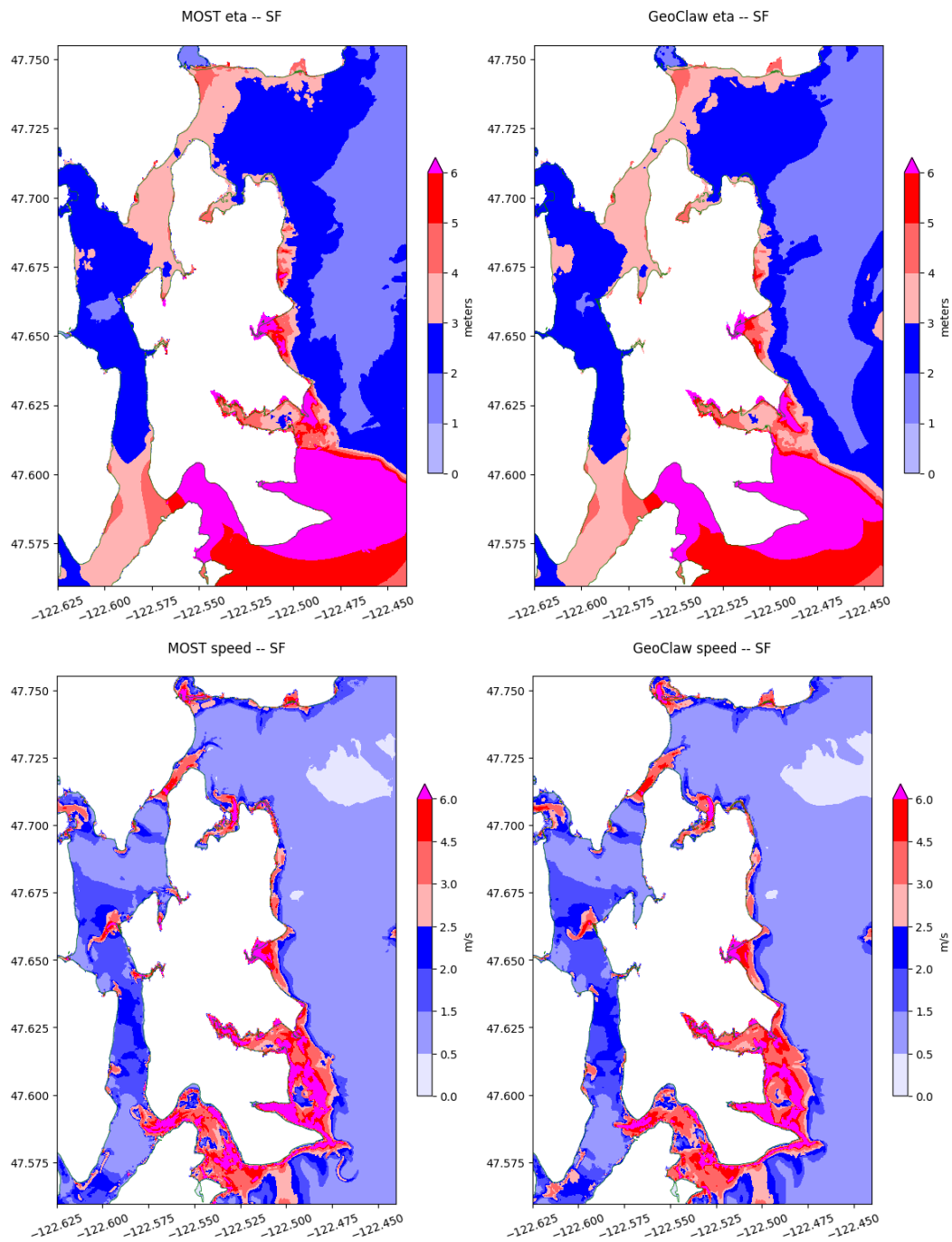


Figure 3: Comparison of results for the SF-L event. Maximum surface elevation (top) and flow speed (bottom) for MOST (left) and GeoClaw (right) simulations.

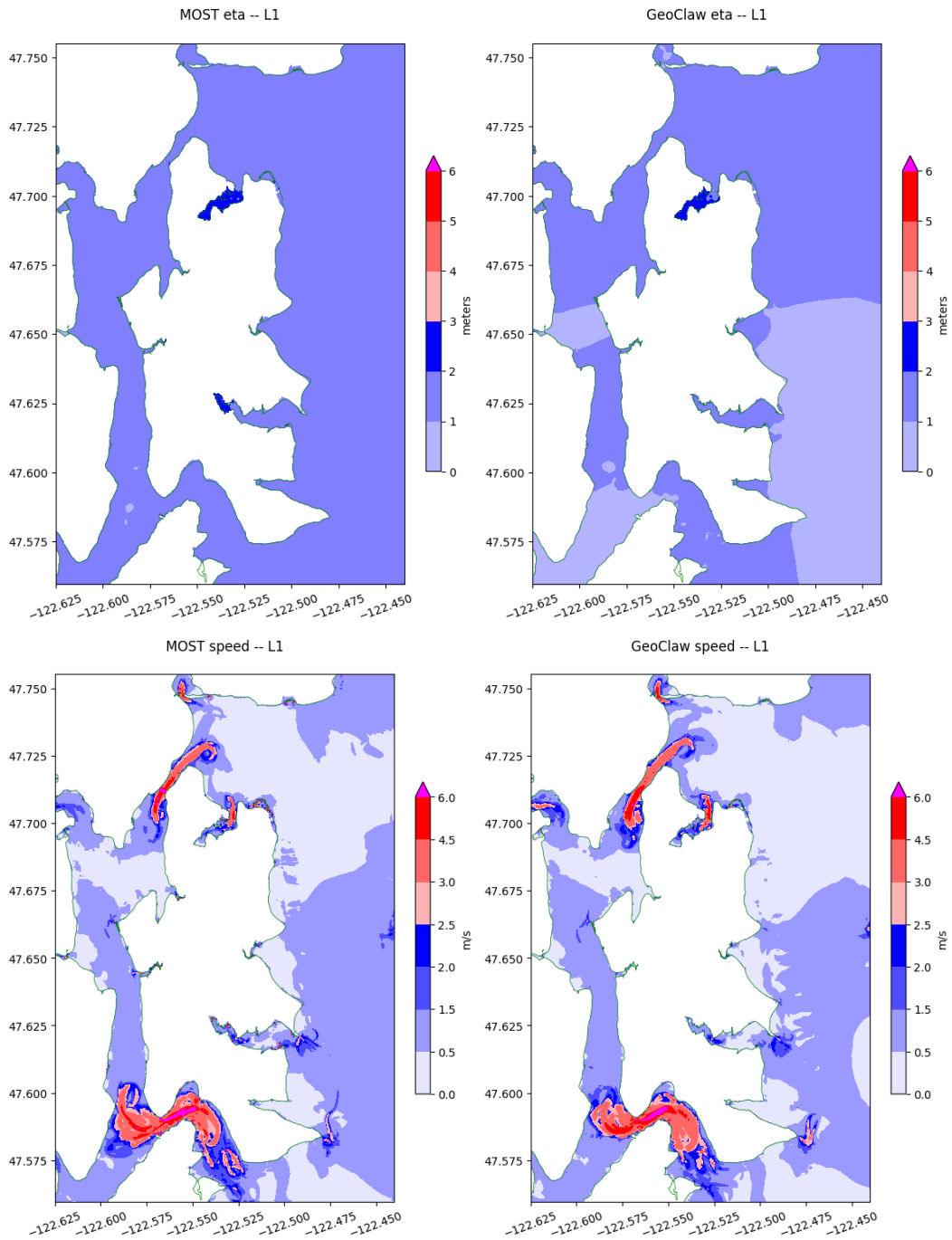


Figure 4: Comparison of results for the CSZ L1 event. Maximum surface elevation (top) and flow speed (bottom) for MOST (left) and GeoClaw (right) simulations.

## 8.2 Gauge comparisons for SF-L

The following plots show time series at several synthetic tide gauge locations around Bainbridge Island, with locations indicated in Figure 1. Only the surface elevation is shown in these plots. The simulations were run for three hours of simulated time, but the largest waves arrive at most Bainbridge Island locations within the first hour, so for each gauge we also show an expanded view of the first 60 minutes in which it is easier to compare the results.

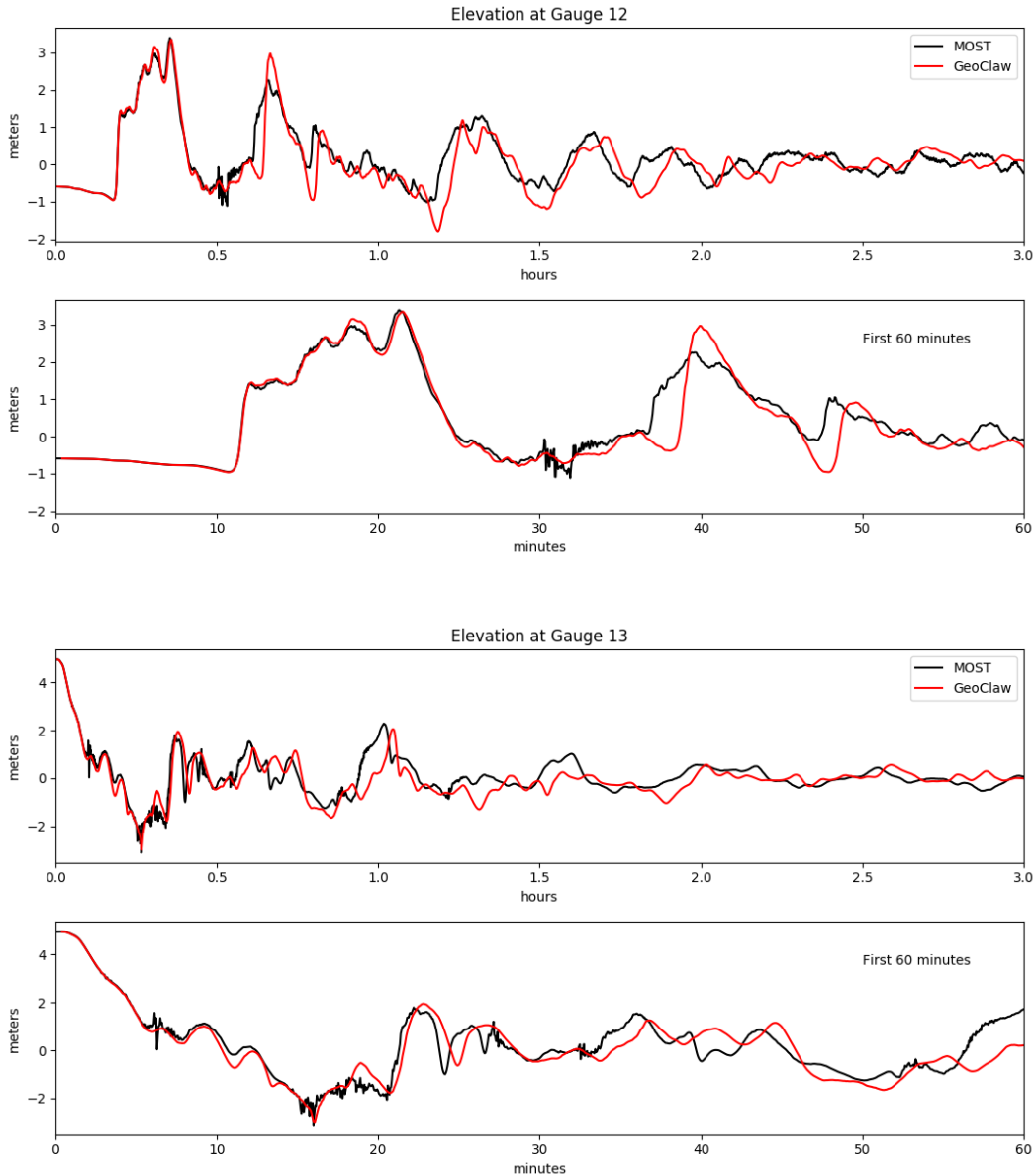


Figure 5: Comparison of MOST and GeoClaw gauge results for SF-L, over 3 hours and zoomed in on the first 60 minutes. Gauges 12 (WA 305 bridge, Agate Pass) and 13 (Point White).

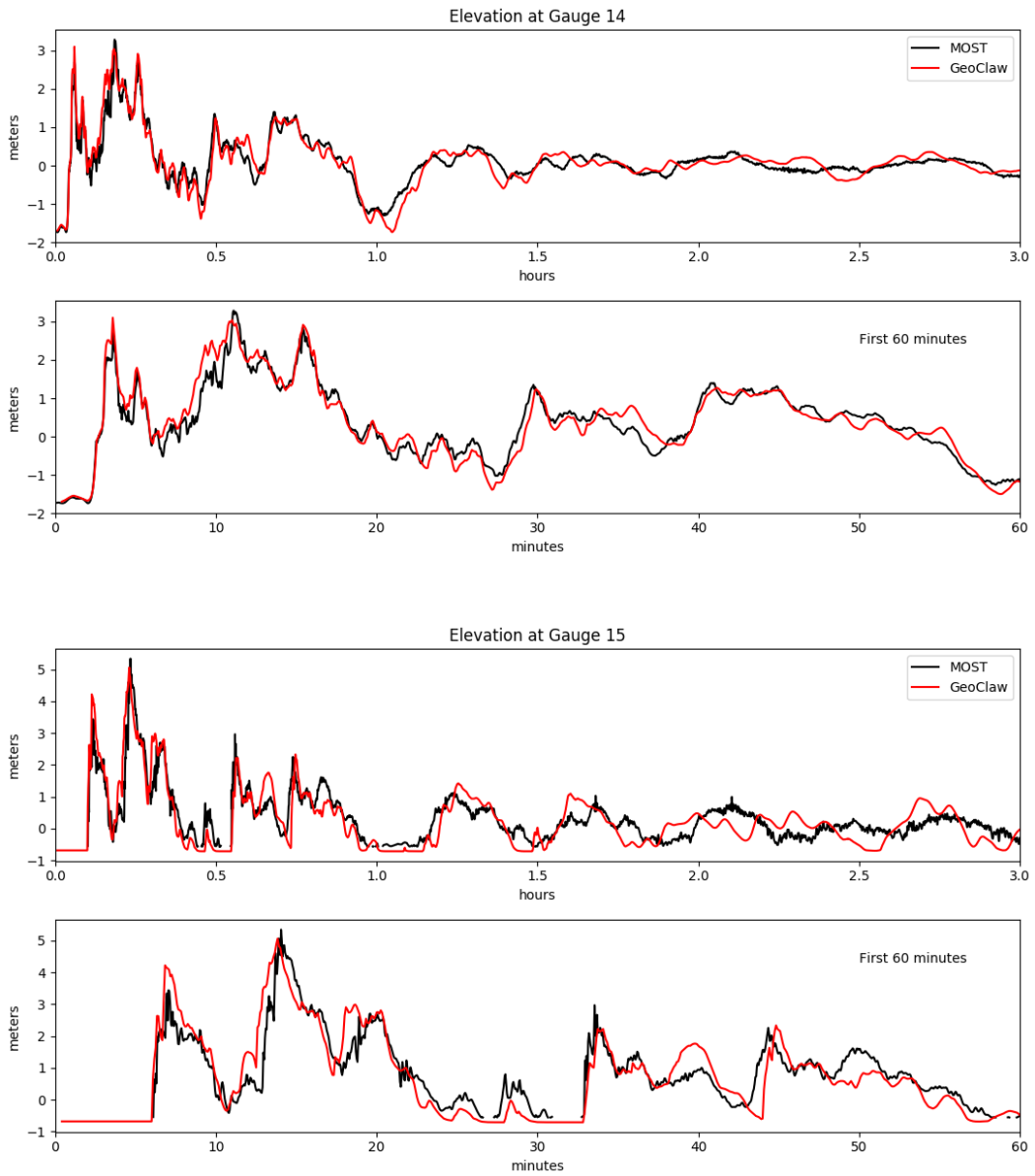


Figure 6: Comparison of MOST and GeoClaw gauge results for SF-L, over 3 hours and zoomed in on the first 60 minutes. Gauges 14 (Winslow Ferry Terminal) and 15 (Strawberry Park).

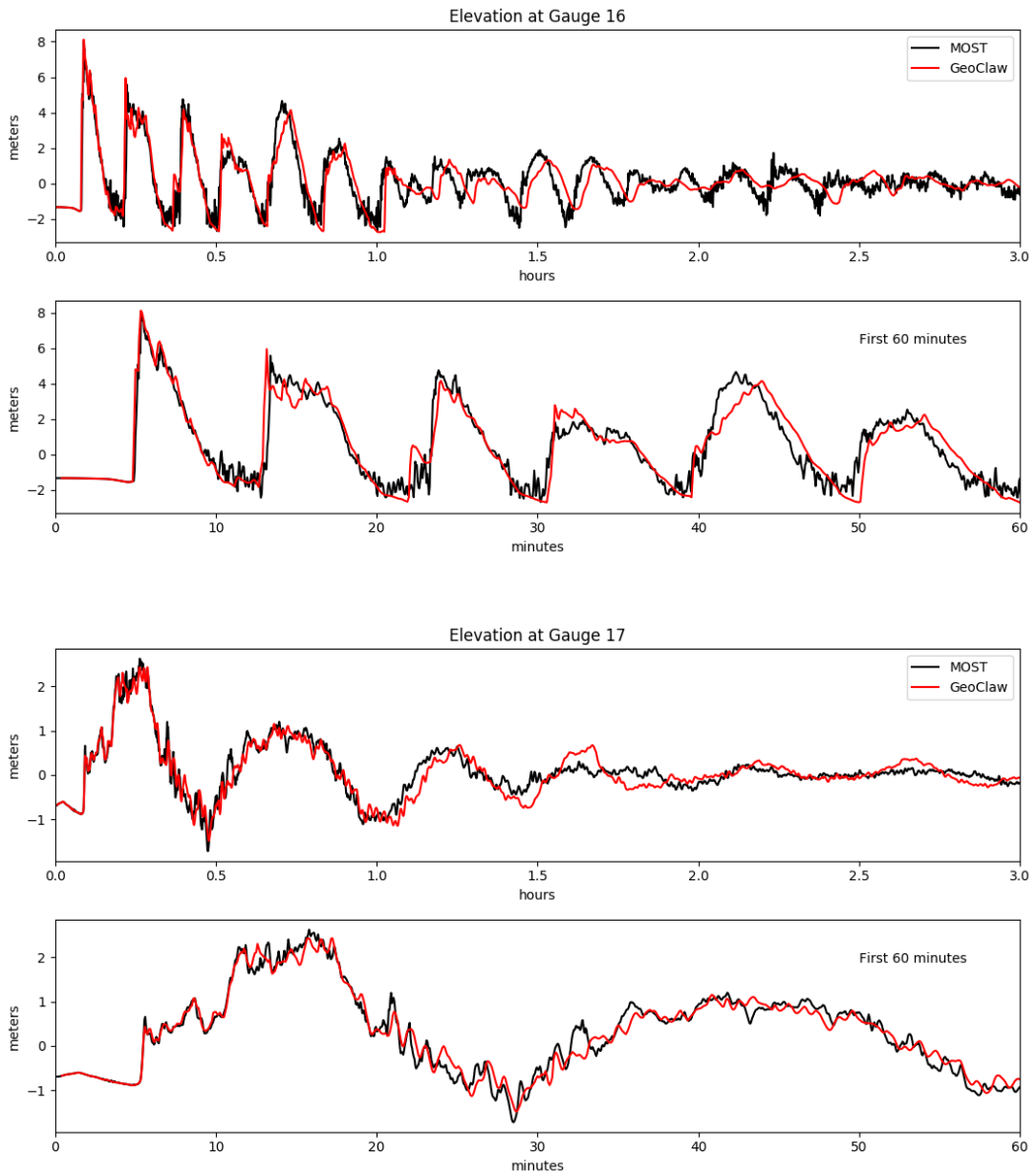


Figure 7: Comparison of MOST and GeoClaw gauge results for SF-L, over 3 hours and zoomed in on the first 60 minutes. Gauges 16 (Murden Cove) and 17 (Hedley Spit).

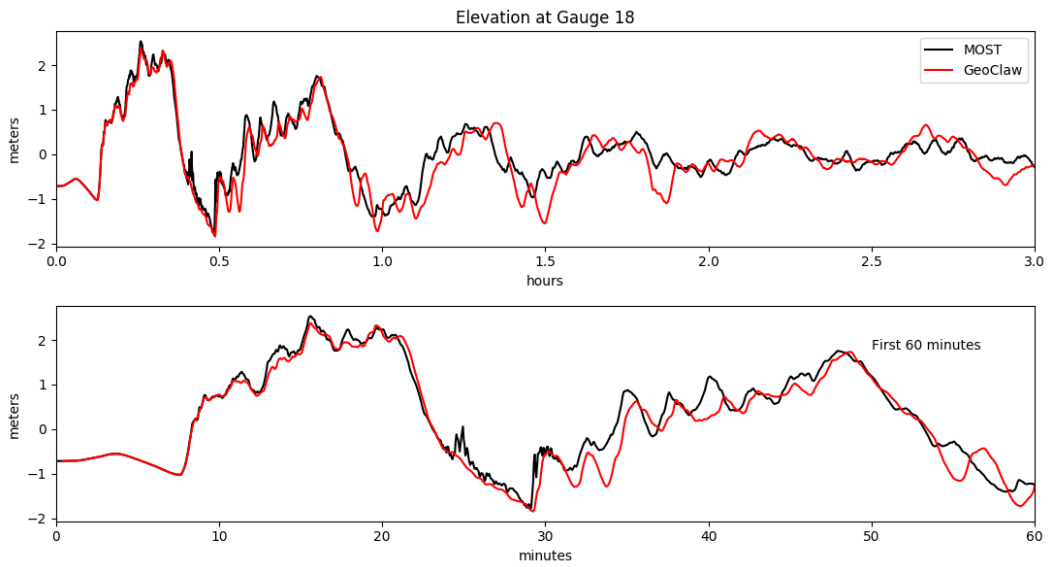


Figure 8: Comparison of MOST and GeoClaw gauge results for SF-L, over 3 hours and zoomed in on the first 60 minutes. Gauge 18 (Port Madison).



### 8.3 Gauge comparisons for L1

The following plots show time series at several synthetic tide gauge locations around Bainbridge Island, with locations indicated in Figure 1. Only the surface elevation is shown in these plots. The positive wave of the tsunami from the L1 source does not arrive at Bainbridge Island until more than 2 hours after the earthquake, although a draw down of water is seen starting about an hour after the event. This is due to the fact that there is subsidence extending east of the trench into the Strait of Juan de Fuca, giving a leading negative wave propagating into the Puget Sound. The uplift occurs west of the trench and so the positive wave arrives later.

In the GeoClaw simulations the tide gauges were not turned on until 1.5 hours after the earthquake since the finest levels of grid refinement around Bainbridge are introduced only at this time.

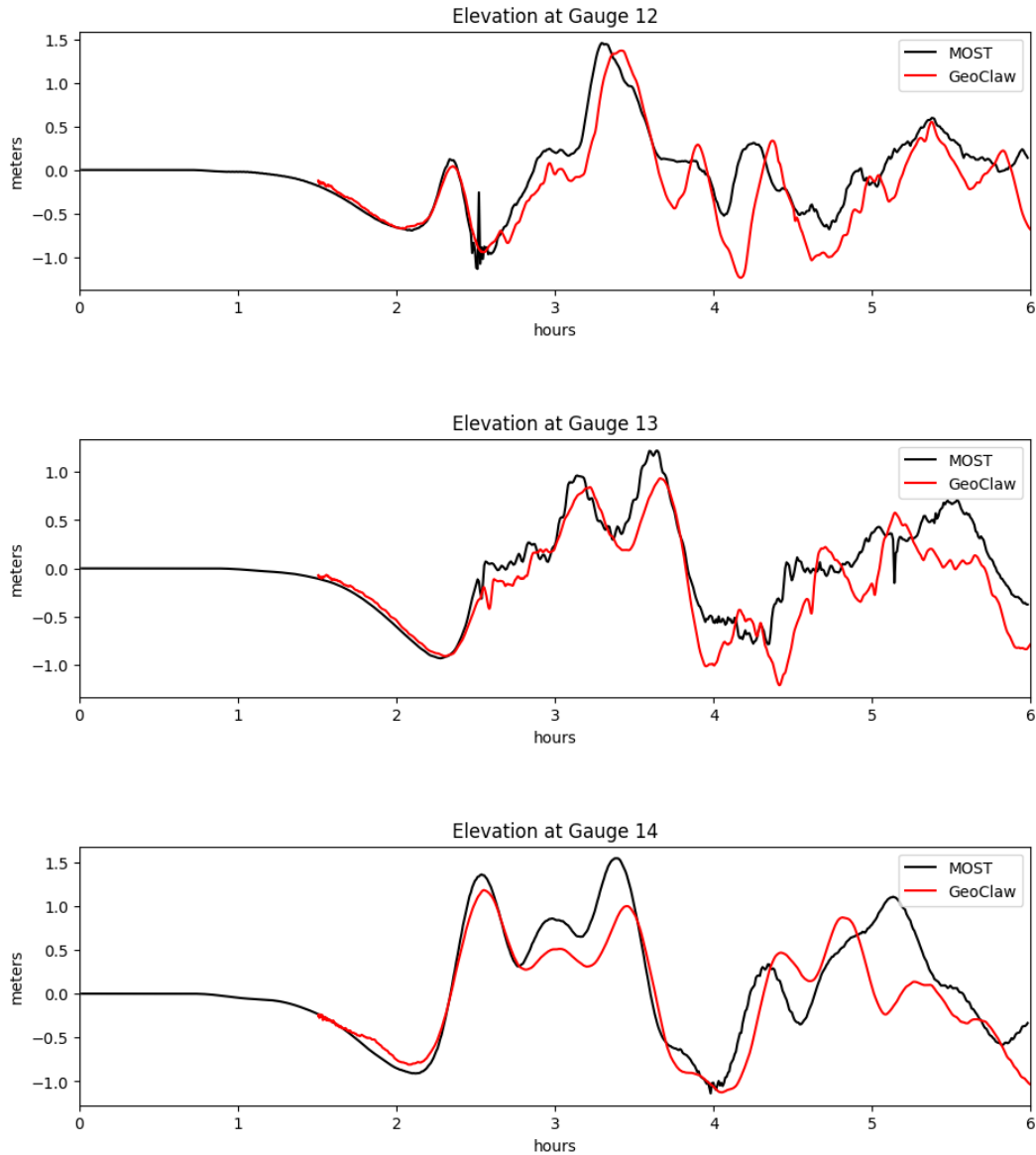


Figure 9: Comparison of MOST and GeoClaw gauge results for L1 over 6 hours. Gauges 12 (WA 305 bridge, Agate Pass), 13 (Point White), and 14 (Winslow Ferry Terminal).

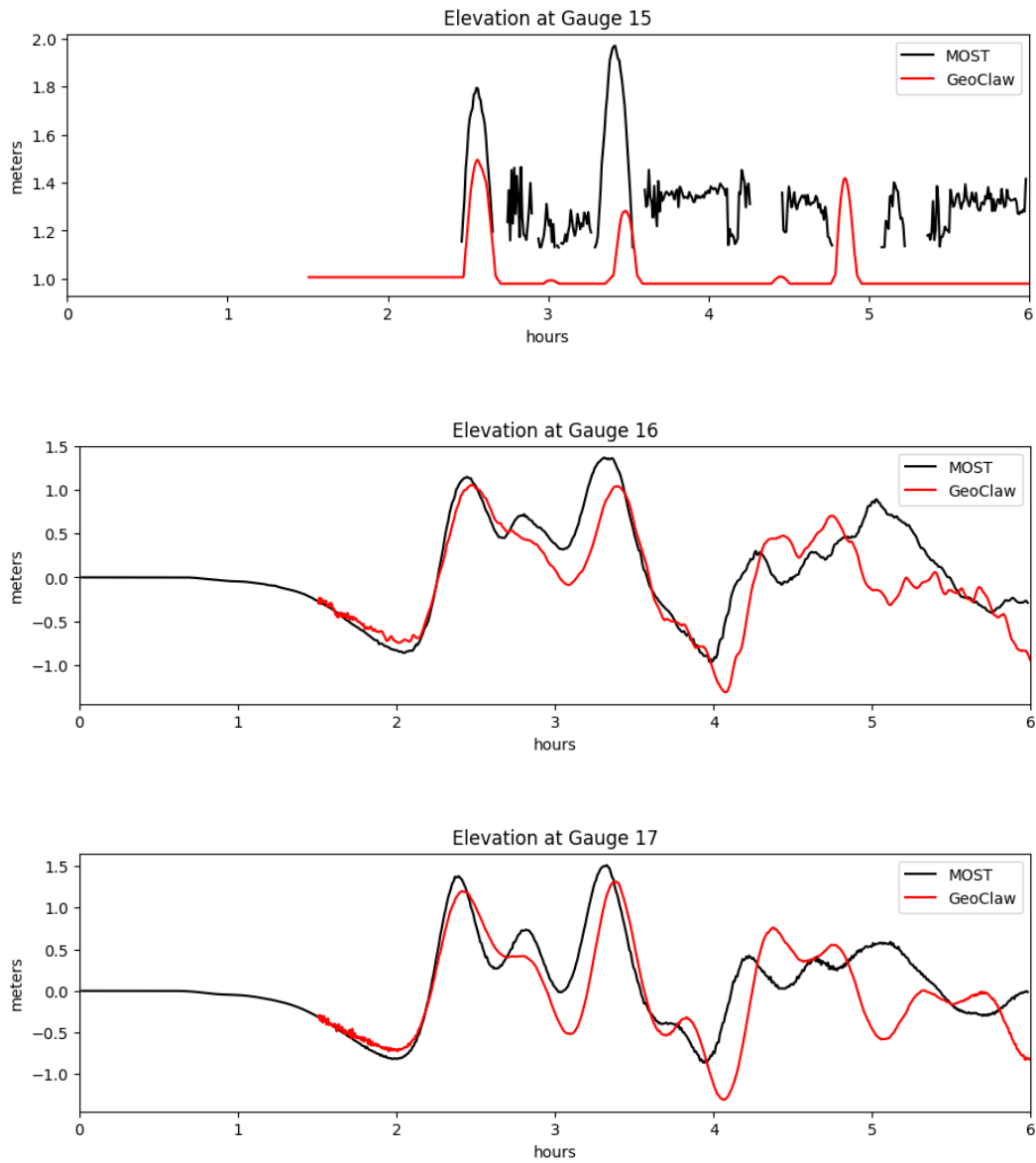


Figure 10: Comparison of MOST and GeoClaw gauge results for L1 over 6 hours. Gauges 15 (Strawberry Park), 16 (Murden Cove), and 17 (Hedley Spit). [[TODO: Add MOST results at “Gauge 15 offshore” for comparison. ]]

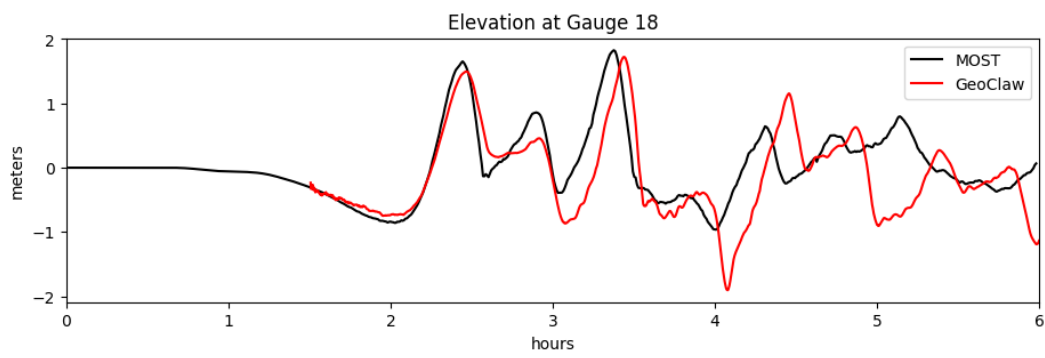


Figure 11: Comparison of MOST and GeoClaw gauge results for L1 over 6 hours. Gauge 18 (Port Madison).

# Appendices

## A Additional comparisons of results for SF-L

This appendix contains additional plots comparing the results obtained with MOST and those obtained with GeoClaw, for the Seattle Fault event SF-L. Section A.1 shows zoomed in views of the plots from Figure 3 along with cross sections of the solution on a few transects.

### A.1 Zoomed views and transect plots

The plots in the next sections first show a zoomed view of one portion of Bainbridge Island, with several transect locations indicated.

Then the following plots show vertical slices along these transects. The top plot in each pair shows the maximum surface elevation of the flow over the full simulation time. (black curve is MOST, red is GeoClaw). These plots also show the slice of the final topography, after the earthquake as green/brown. The green part shows what portion was initially above MHW before the earthquake, the brown portion was initially below MHW, so the interface between green and brown indicates the initial shoreline position. The blue shows the water after it has settled down to MHW again, long after the earthquake, so it hits the topography at the new coastline. If it's brown at this point then the land was uplifted, while if the ground is green at the new shoreline then it subsided and some of the original green land is now below MHW.

Note that in locations where the ground was uplifted (south of Eagle Harbor, roughly), the maximum surface elevation generally agrees with the original shoreline location (e.g. at Point White at the SW corner of Bainbridge). This indicates that the maximum elevation occurred immediately after the earthquake. The water rose with the land initially, and then flowed away towards the subsided regions.

The bottom plot in each pair of transect slices shows the maximum flow speed over the same range of latitudes as in the top plot. In general the speeds are less smooth and do not agree between MOST and GeoClaw quite as well as the elevations. This is expected due to the extreme sensitivity of the flow speeds.

### A.1.1 Seattle Fault SF-L, Eagle Harbor

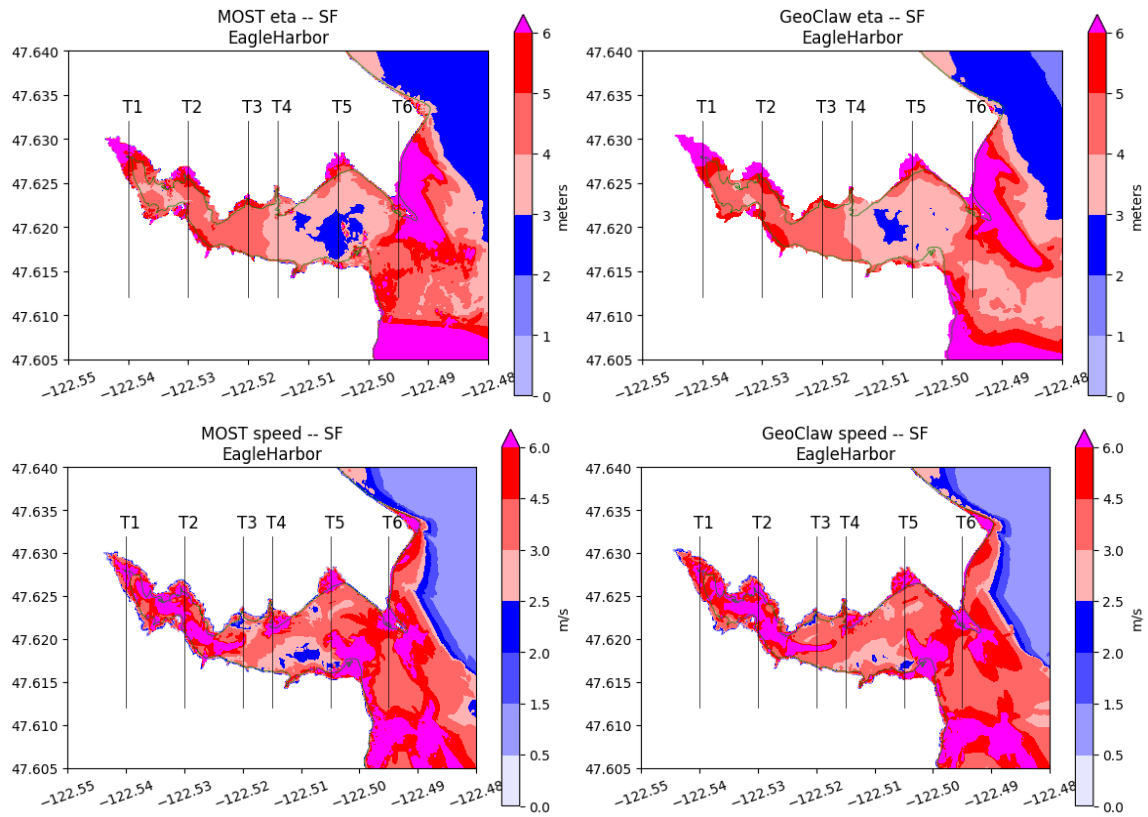


Figure 12: Comparison of MOST and GeoClaw results for the SF-L event in Eagle Harbor. Also shown is the location of transects. The following plots show cross sections of the maximum surface and speed along these transects.

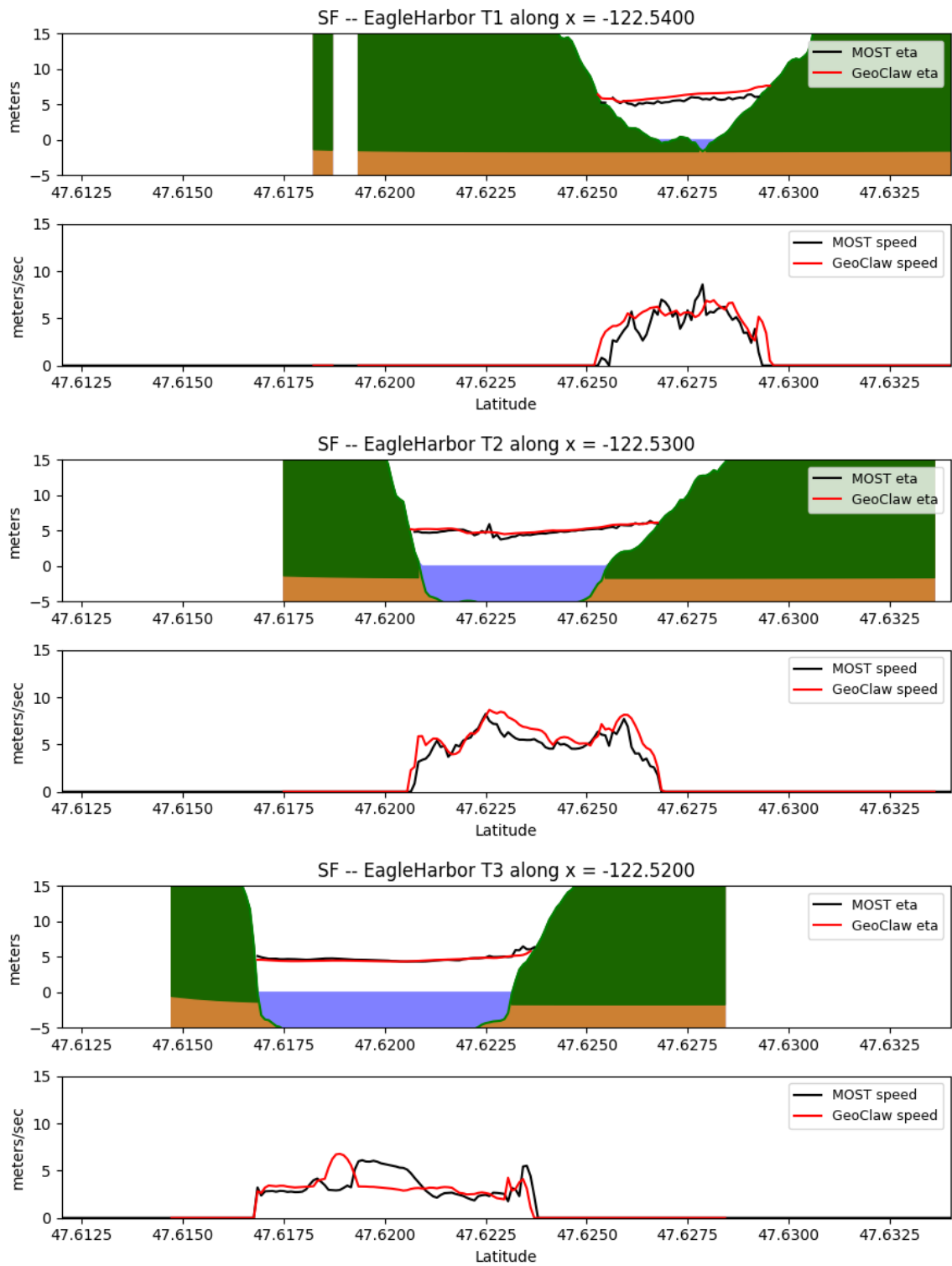


Figure 13: Comparison of MOST and GeoClaw results along Eagle Harbor transects T1–T3. [[TODO: Fix the plots so land above 40 m elevation shows up as green/brown rather than being masked out?]]

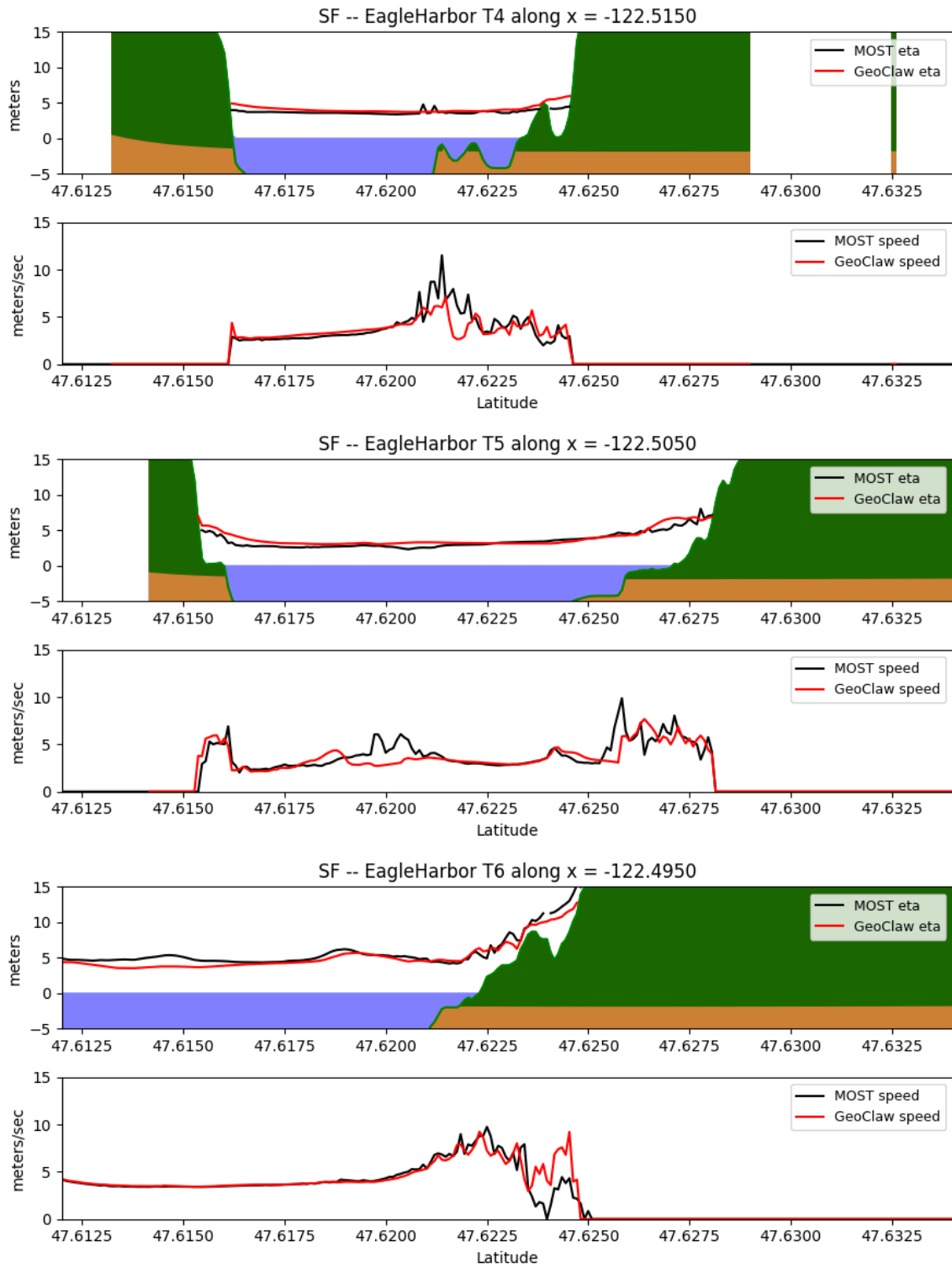


Figure 14: Comparison of MOST and GeoClaw results along Eagle Harbor transects T4–T6.

### A.1.2 Seattle Fault SF-L, Murden Cove

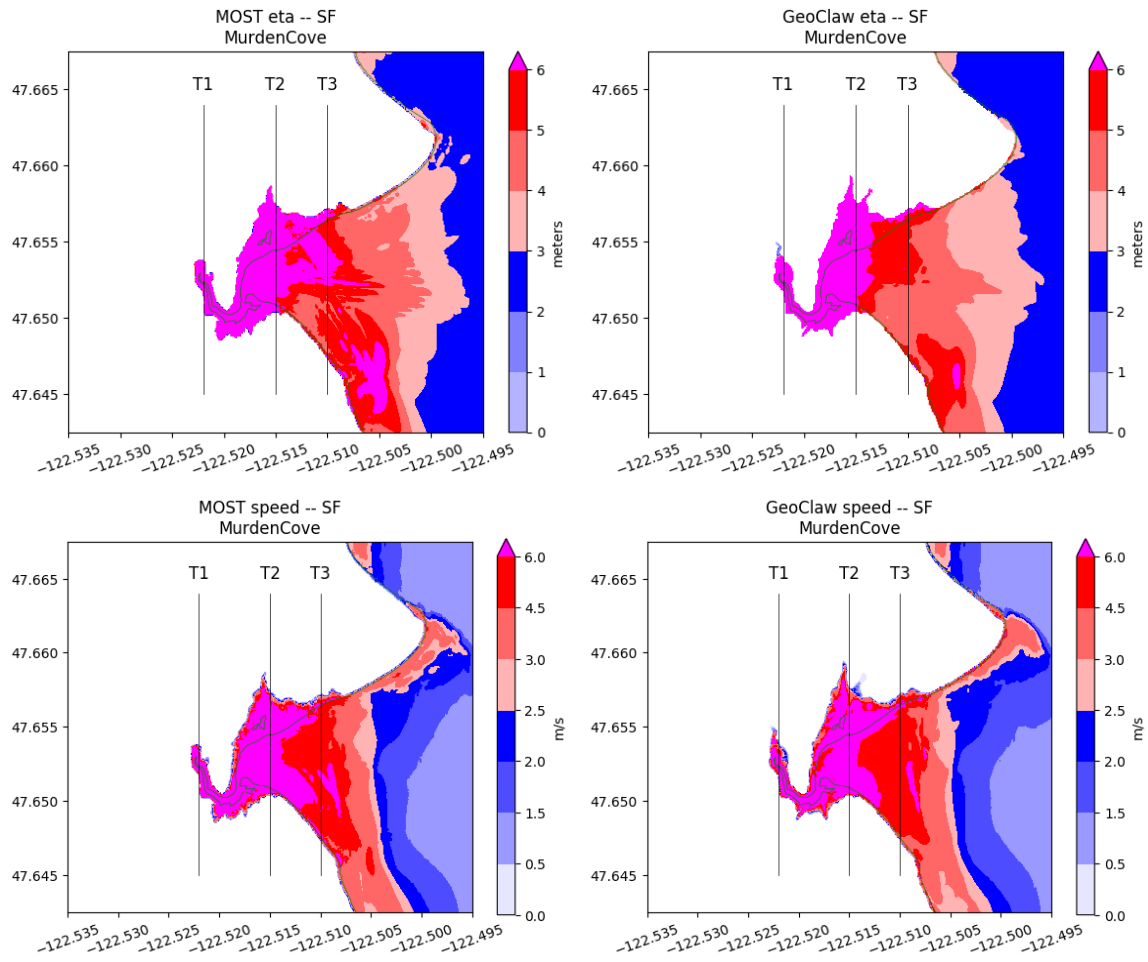


Figure 15: Comparison of MOST and GeoClaw results for the SF-L event in Murden Cove. Also shown is the location of transects. The following plots show cross sections of the maximum surface and speed along these transects.



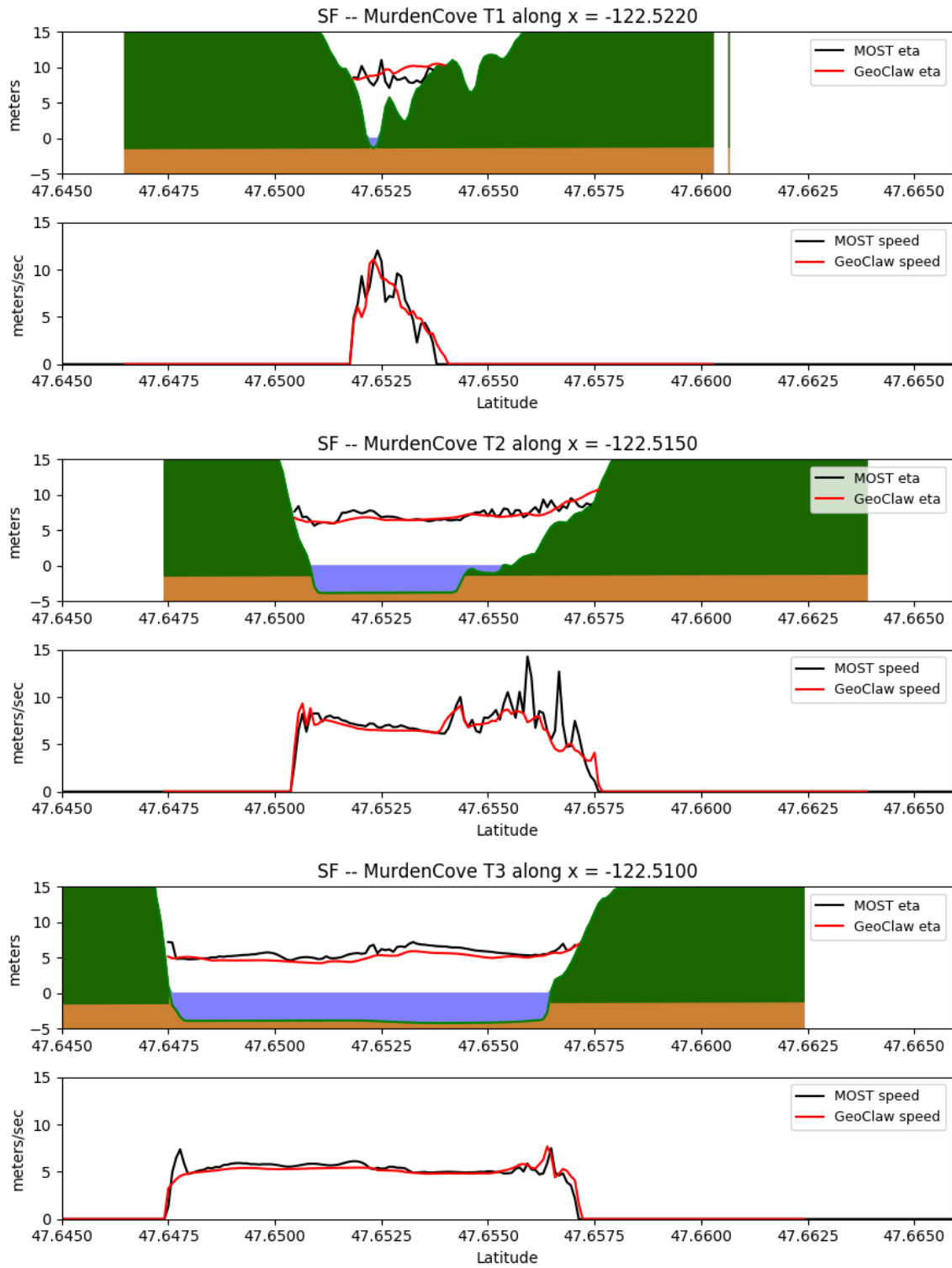


Figure 16: Comparison of MOST and GeoClaw results along Murden Cove transects.

### A.1.3 Seattle Fault SF-L, Agate Pass

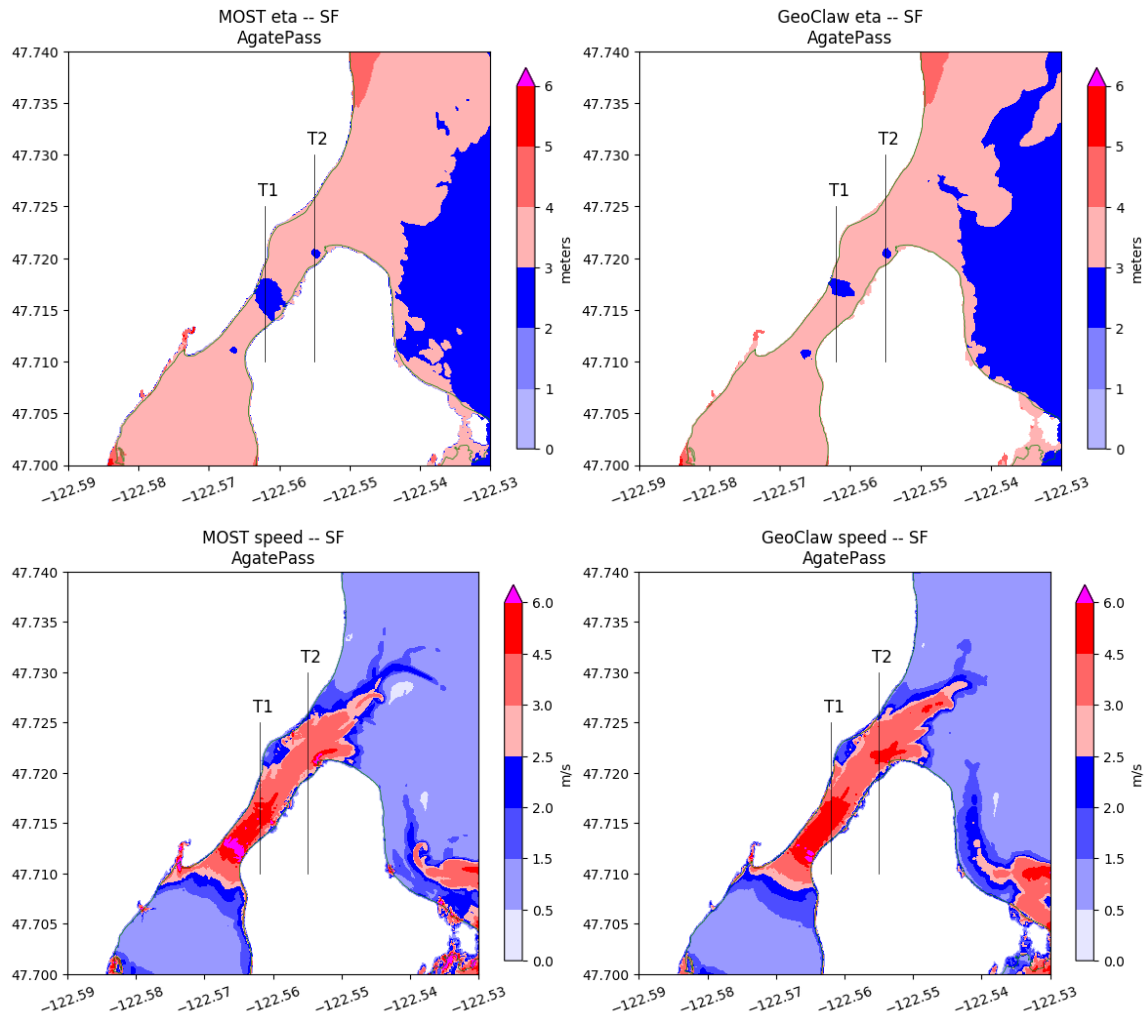


Figure 17: Comparison of MOST and GeoClaw results for the SF-L event around Agate Pass. Also shown is the location of transects. The following plots show cross sections of the maximum surface and speed along these transects.

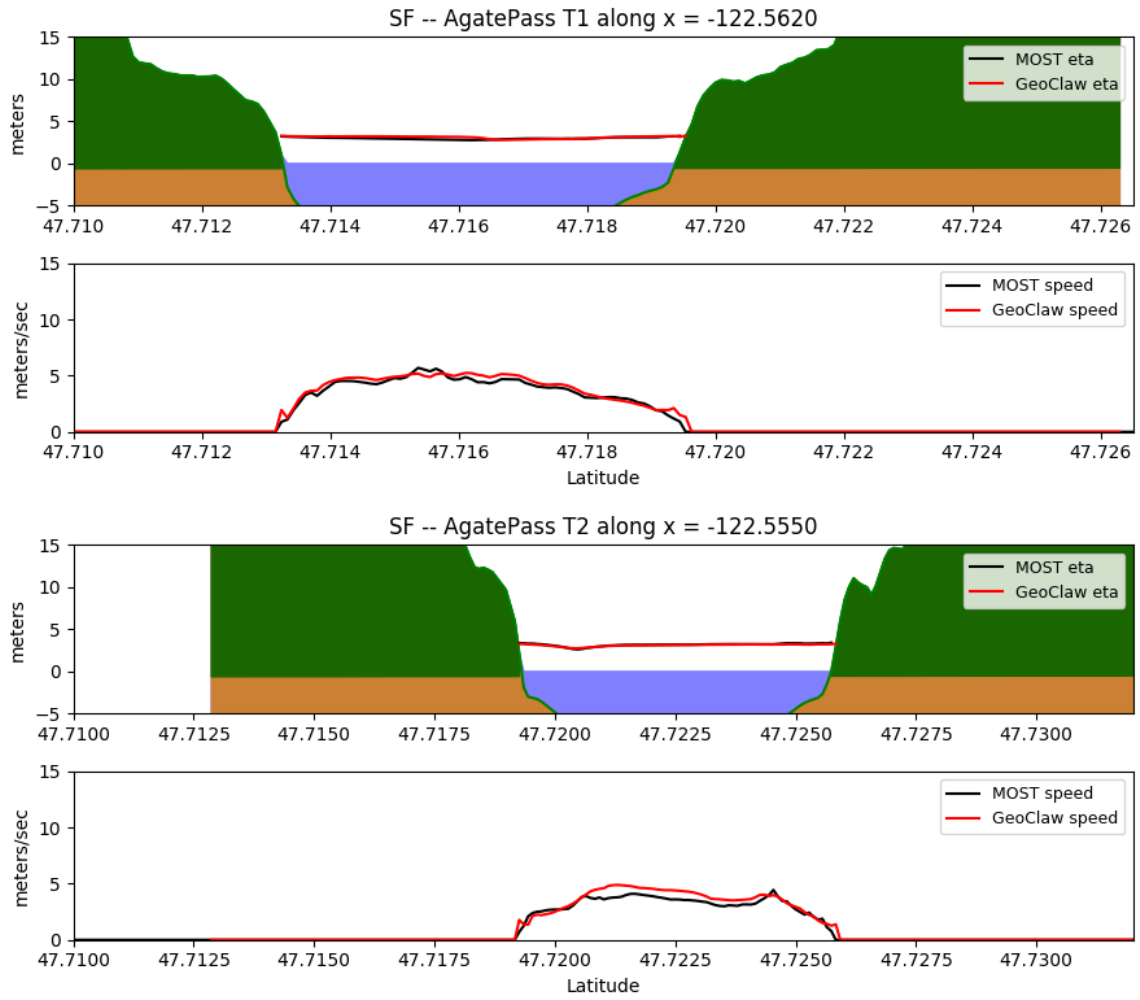


Figure 18: Comparison of MOST and GeoClaw results along Agate Pass transects.

### A.1.4 Seattle Fault SF-L, Point White

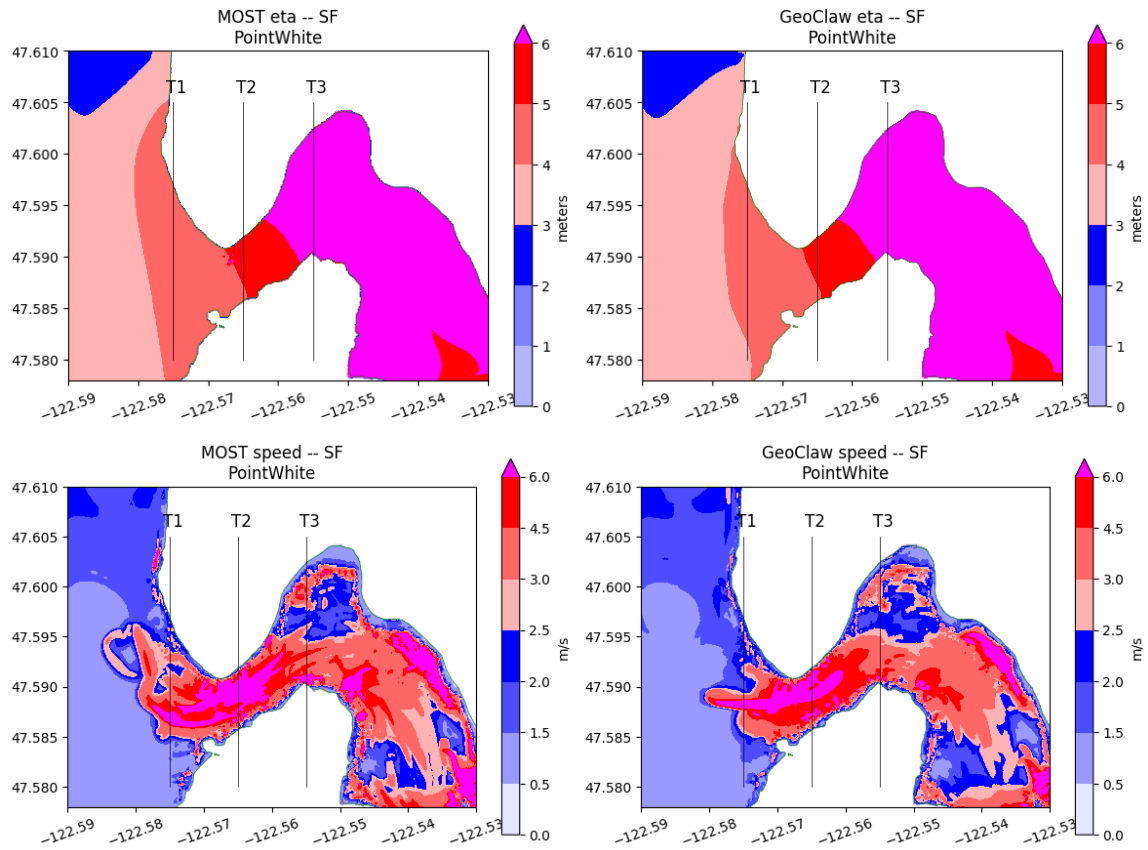


Figure 19: Comparison of MOST and GeoClaw results for the SF-L event around Point White. Also shown is the location of transects. The following plots show cross sections of the maximum surface and speed along these transects.

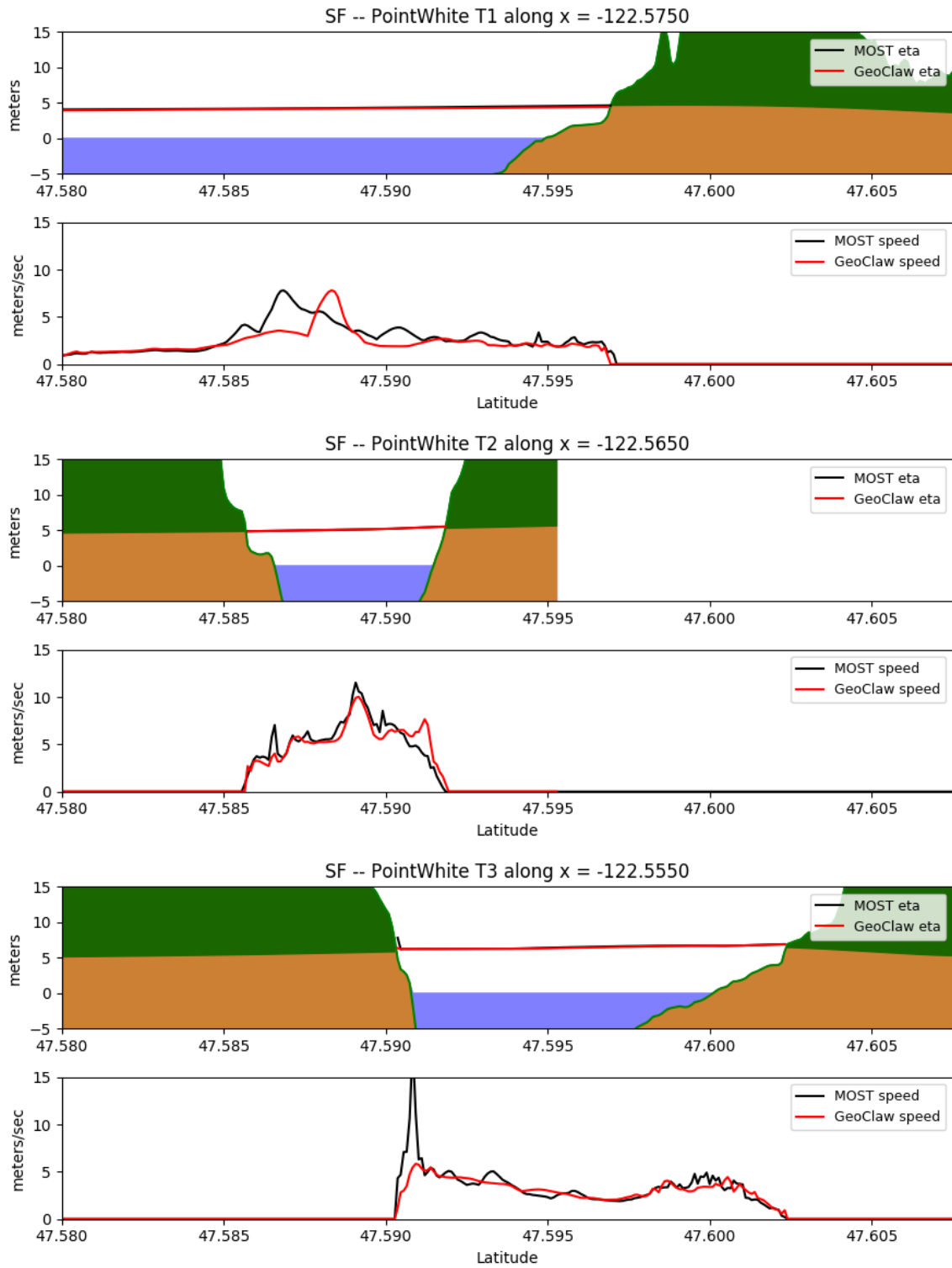


Figure 20: Comparison of MOST and GeoClaw results along Point White transects.

## B Additional comparisons of results for CSZ L1

This appendix contains additional plots comparing the results obtained with MOST and those obtained with GeoClaw, for the CSZ event L1. Section [B.1](#) shows zoomed in views of the plots from [Figure 4](#) along with cross sections of the solution on a few transects. Section [8.3](#) shows time series results at several gauges.

### B.1 Zoomed views and transect plots

The plots in the next sections first show a zoomed view of one portion of Bainbridge Island, with several transect locations indicated. Then the following plots show vertical slices along these transects. The format is the same as used for the SF-L results in [Section A.1](#); see the beginning of that section for more discussion of plots.

### B.1.1 CSZ L1, Eagle Harbor

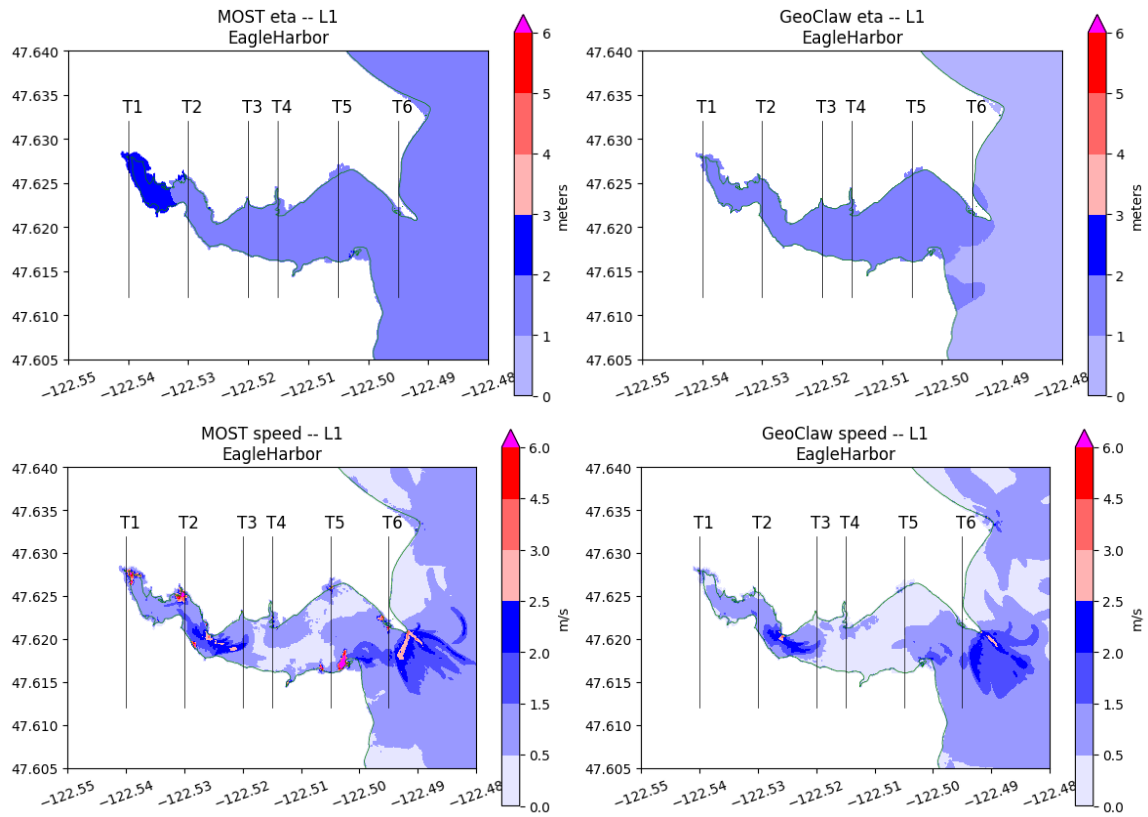


Figure 21: Comparison of MOST and GeoClaw results for the L1 event in Eagle Harbor. Also shown is the location of transects. The following plots show cross sections of the maximum surface and speed along these transects.

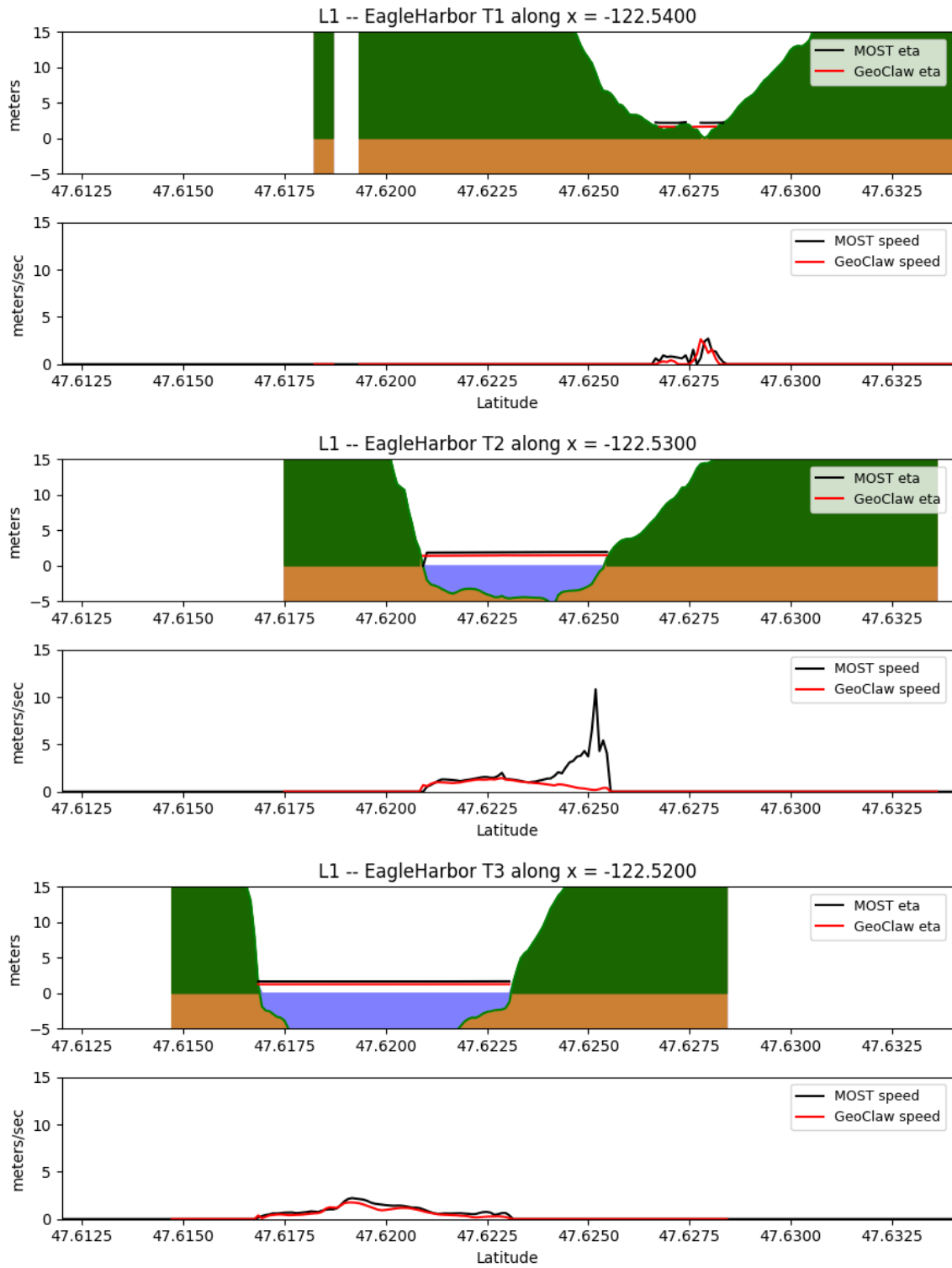


Figure 22: Comparison of MOST and GeoClaw results along Eagle Harbor transects.



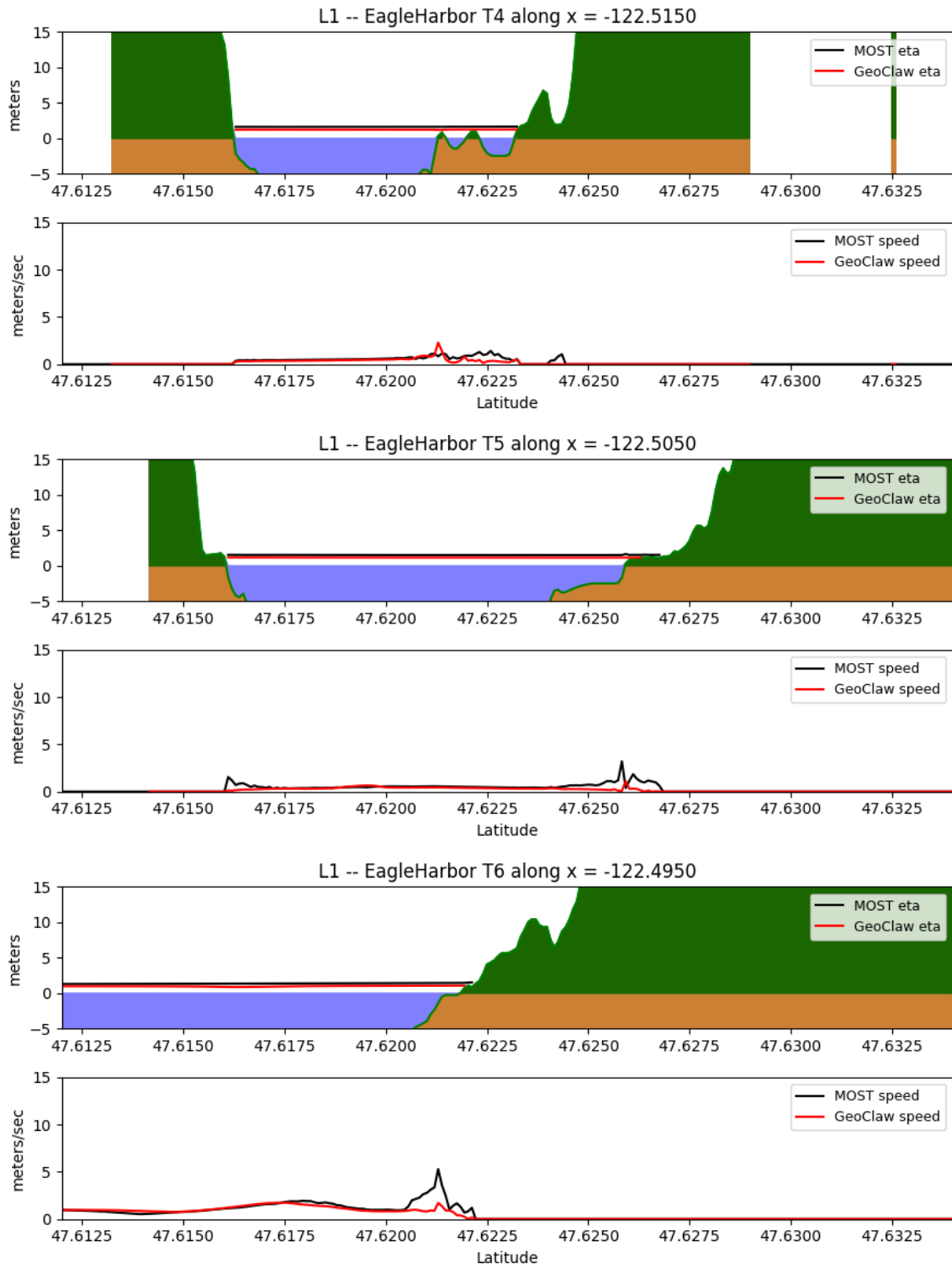


Figure 23: Comparison of MOST and GeoClaw results along Eagle Harbor transects.

### B.1.2 CSZ L1, Murden Cove

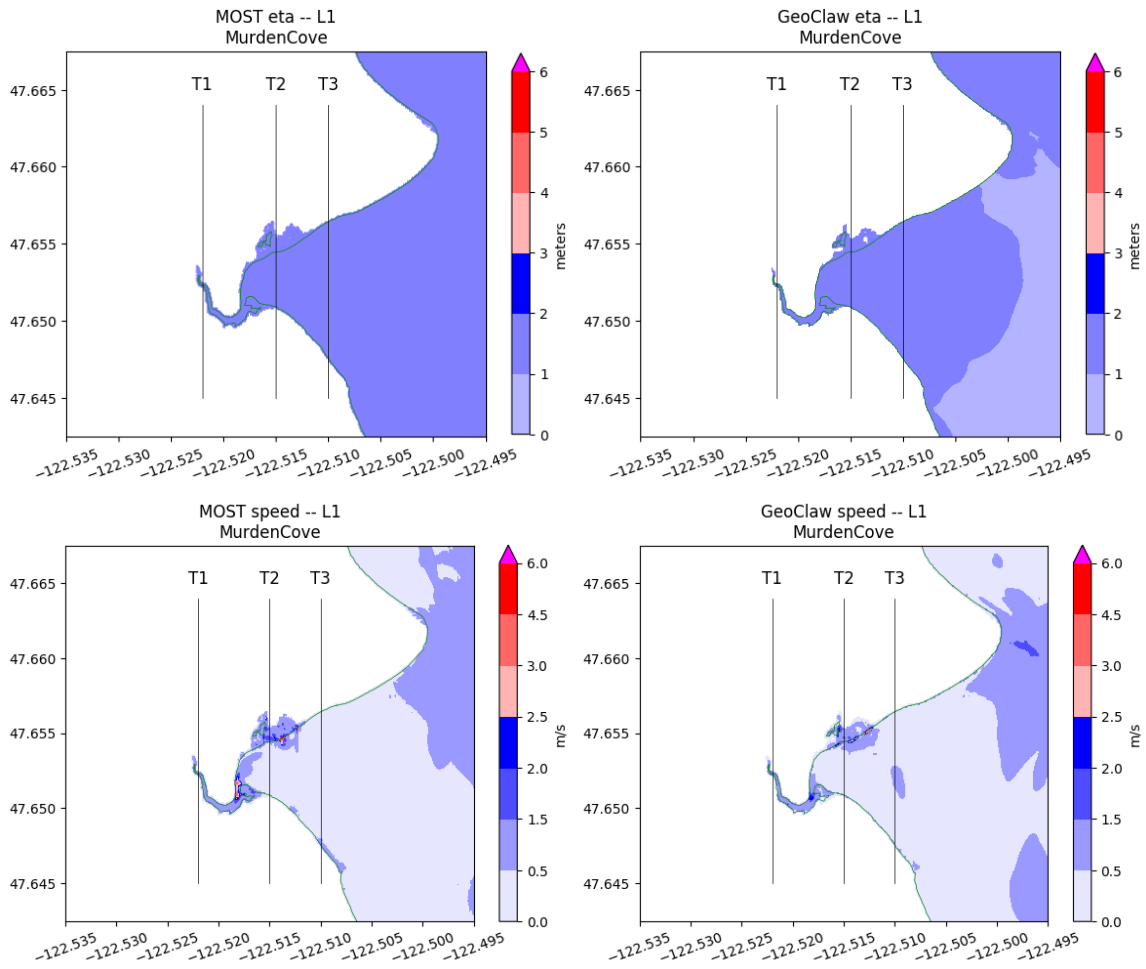


Figure 24: Comparison of MOST and GeoClaw results for the L1 event in Murden Cove. Also shown is the location of transects. The following plots show cross sections of the maximum surface and speed along these transects.

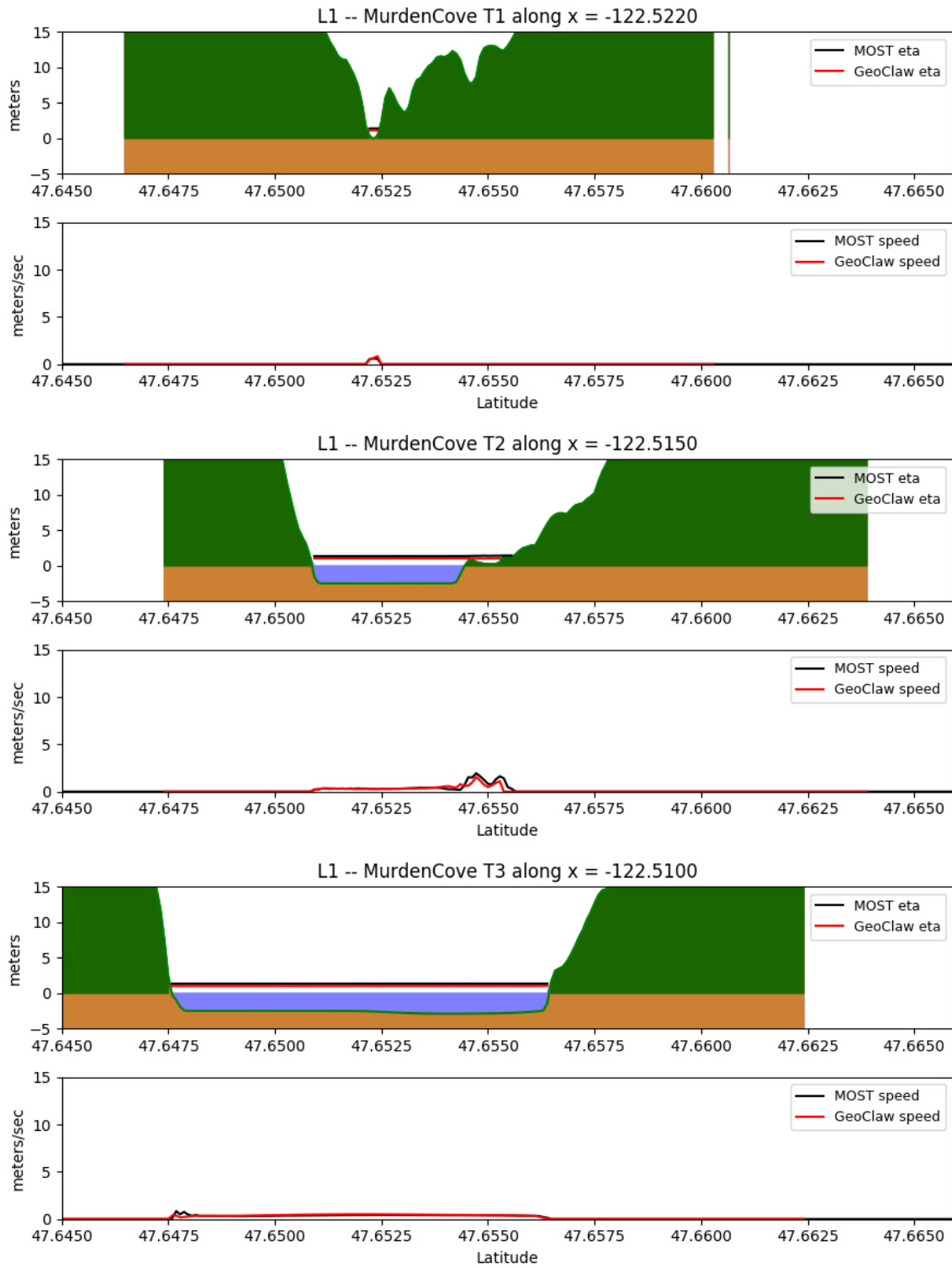


Figure 25: Comparison of MOST and GeoClaw results along Murden Cove transects.

### B.1.3 CSZ L1, Agate Pass

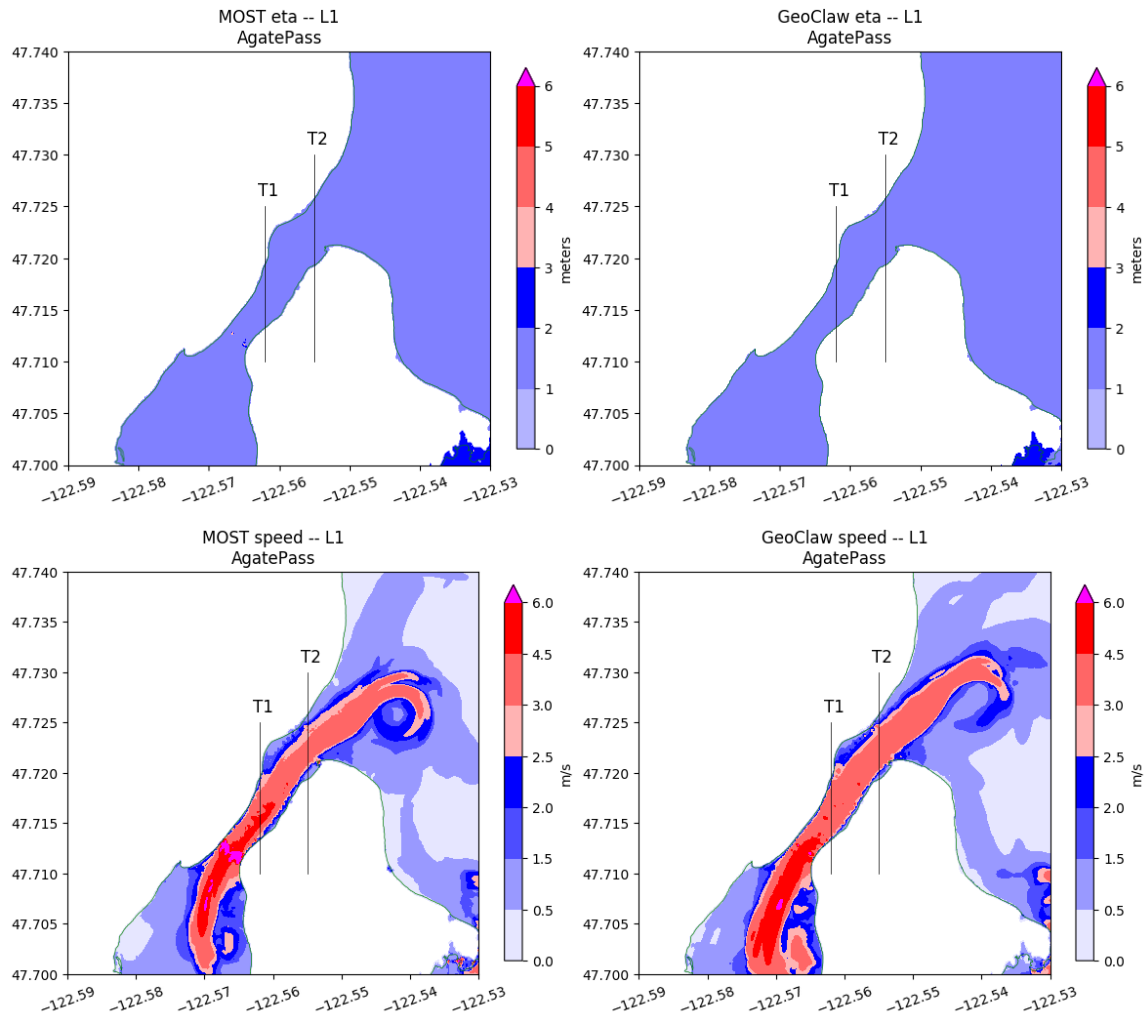


Figure 26: Comparison of MOST and GeoClaw results for the L1 event around Agate Pass. Also shown is the location of transects. The following plots show cross sections of the maximum surface and speed along these transects.

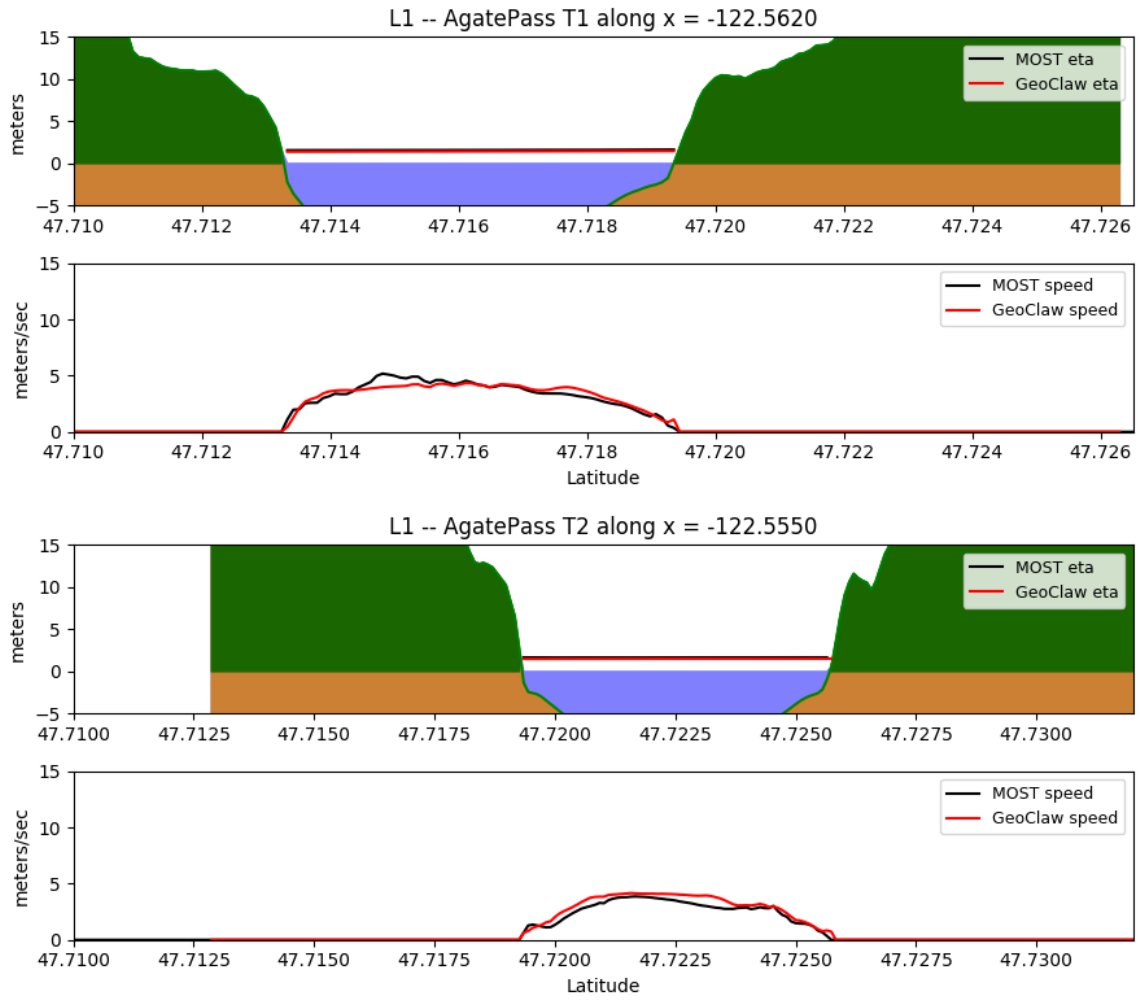


Figure 27: Comparison of MOST and GeoClaw results along Agate Pass transects.

### B.1.4 CSZ L1, Point White

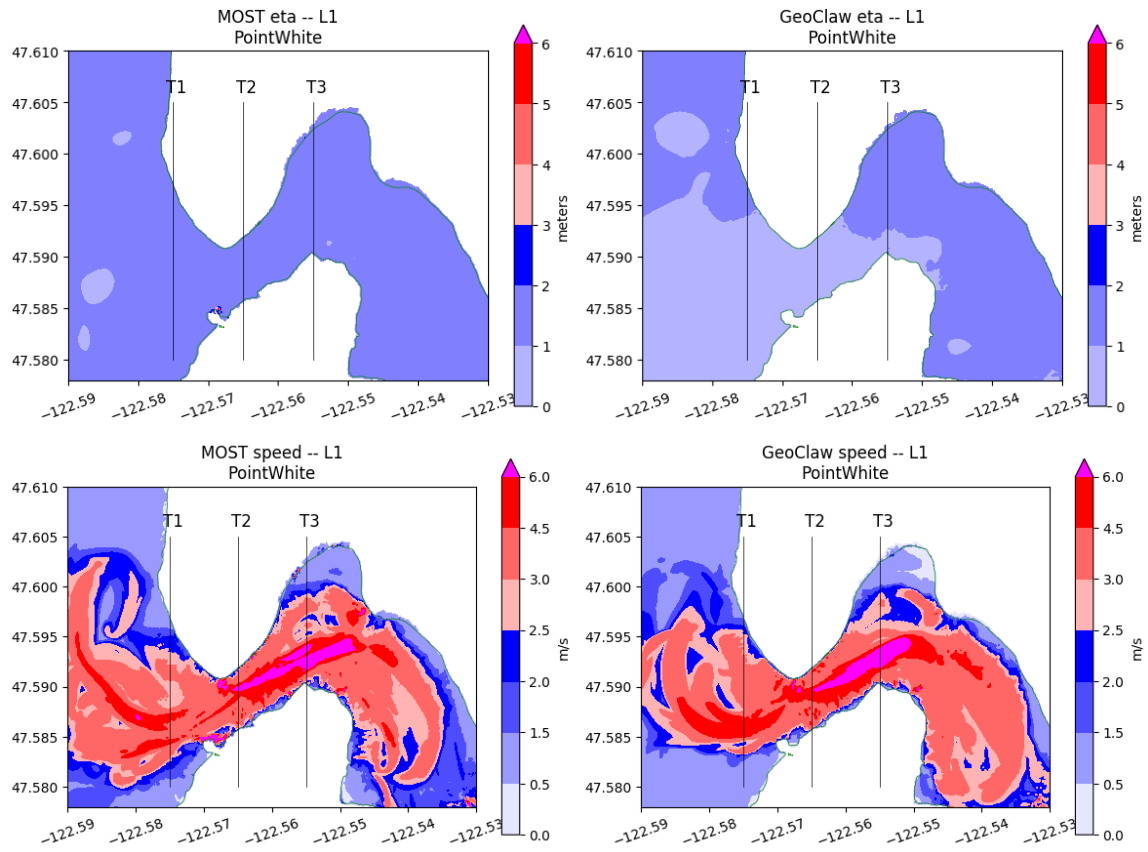


Figure 28: Comparison of MOST and GeoClaw results for the L1 event around Point White. Also shown is the location of transects. The following plots show cross sections of the maximum surface and speed along these transects.

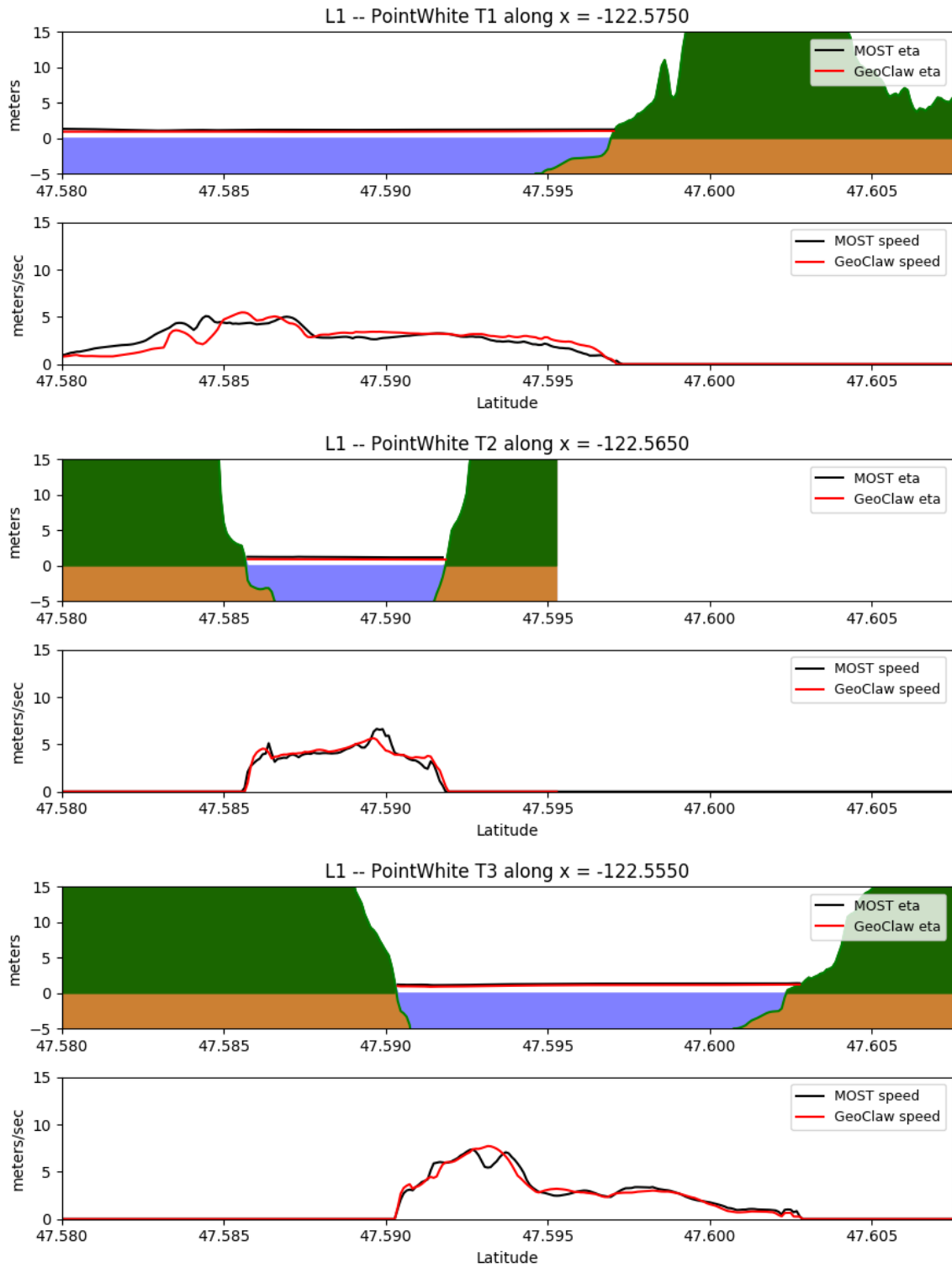


Figure 29: Comparison of MOST and GeoClaw results along Point White transects.

## C Sensitivity studies

Several sensitivity studies were performed using the GeoClaw model and the SF-L source in order to see how much the tsunami results vary due to changes in model parameters. In order to perform several simulations efficiently, for this study a restricted fine grid was used that only covered the eastern shore of Bainbridge Island from Eagle Harbor to Murden Cove. The model was also run for only 1 hour of simulated time since the maximum flow depth and speed are generally observed within this time period on this restricted domain.

[[TODO: Add plot of region, more discussion.]]

### C.1 Sensitivity to grid resolution

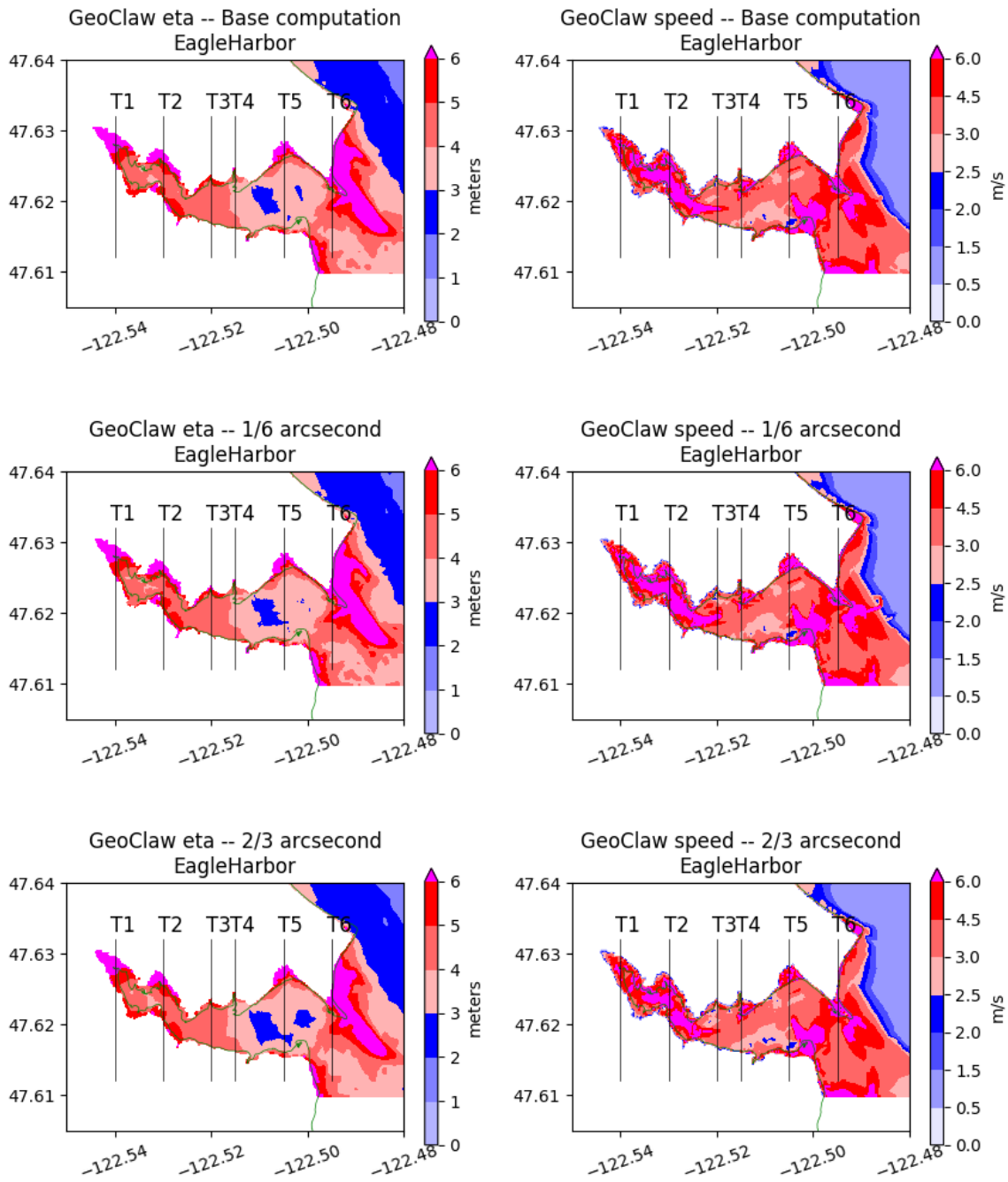
The GeoClaw simulations were run over the smaller domain with different grid resolutions on the finest level. The “base computation” uses 1/3 arcsecond grid resolution. Simulations were performed using 2/3” and 1/6”. Note that in all cases the underlying DEM defining the topography is the same 1/3” DEM.

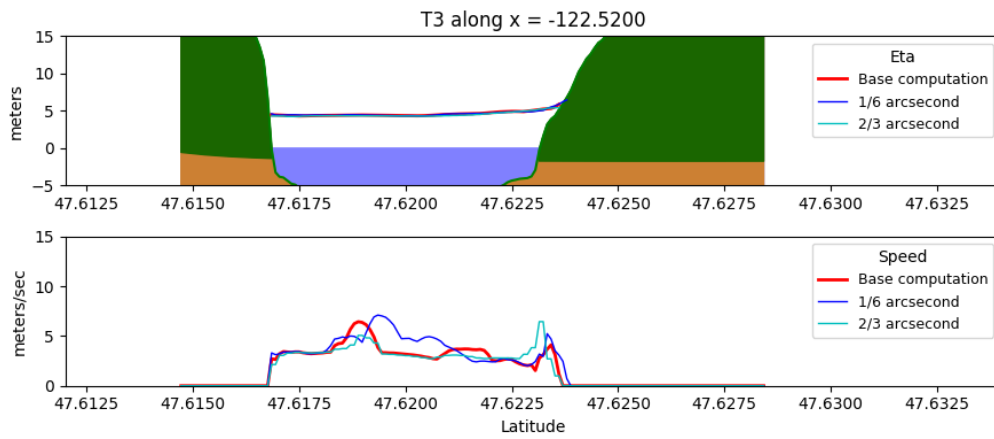
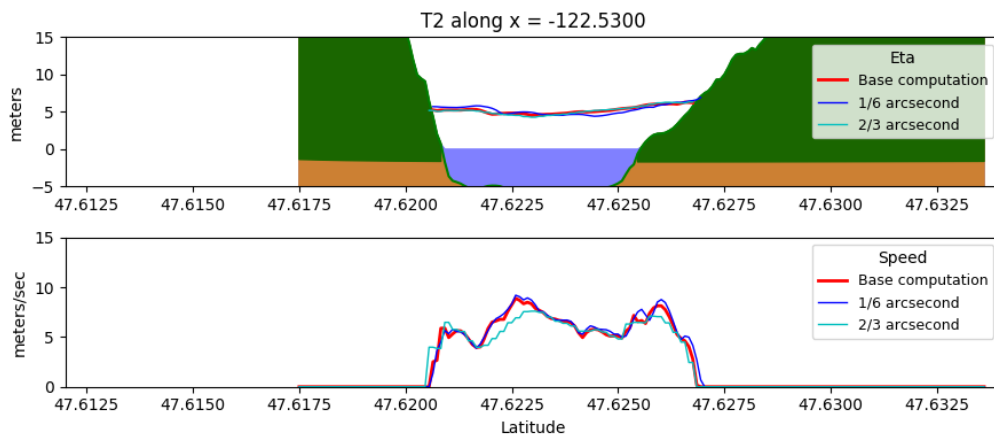
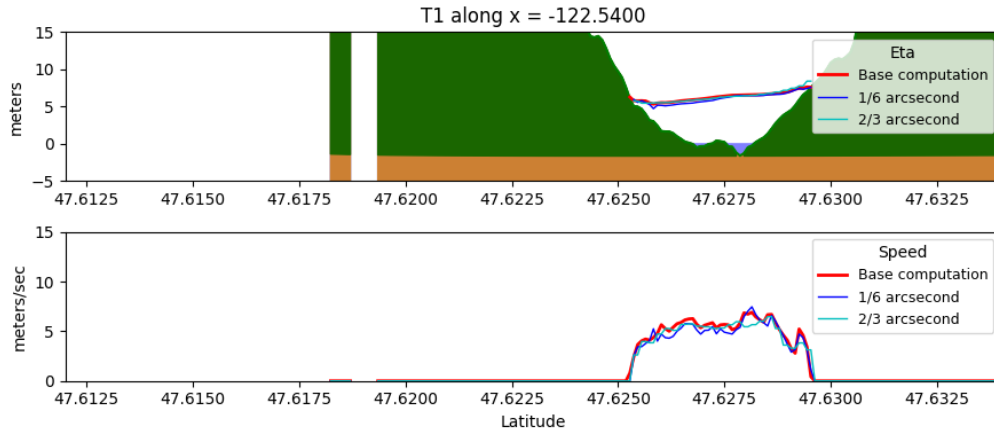


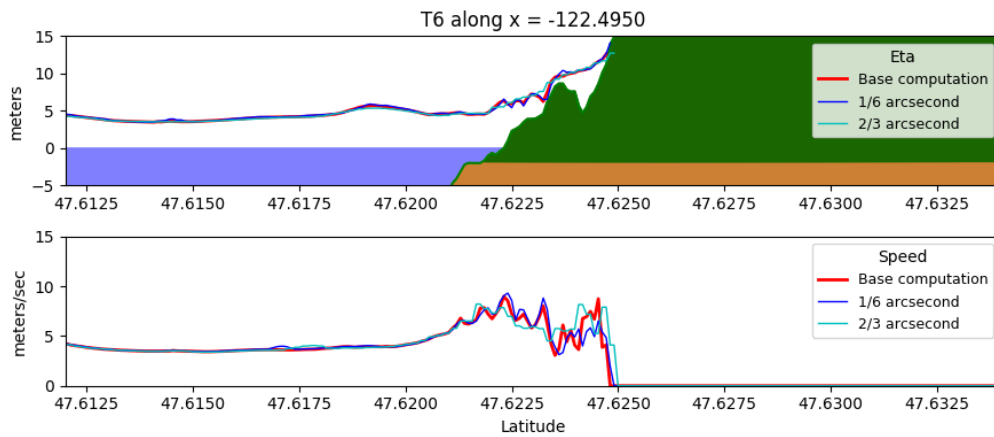
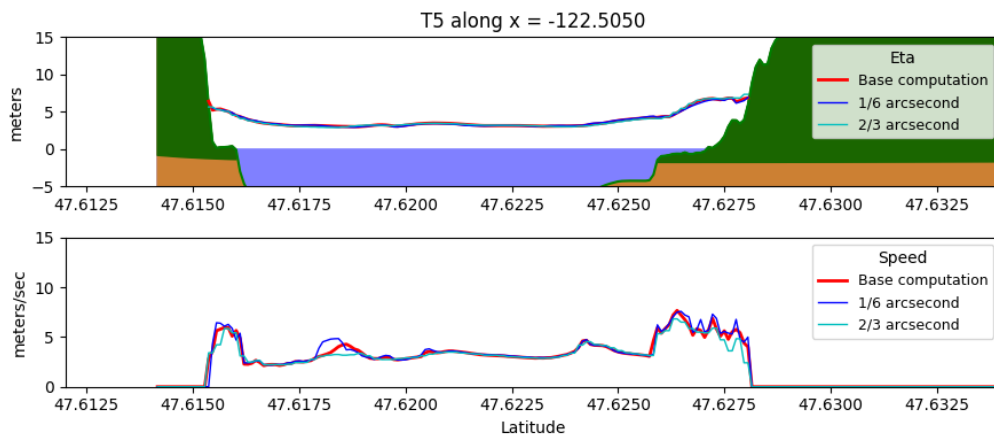
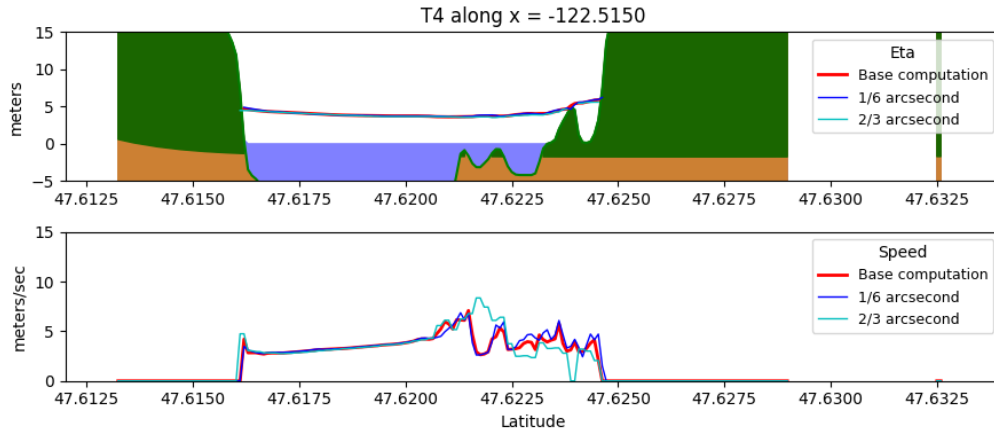
### C.1.1 Eagle Harbor

The plots below show sensitivity study results obtained with GeoClaw using the base parameters with resolution 1/3" (top) and varying the finest grid resolution to 1/6" (middle) or 2/3" (bottom).

Figures on the next two page show cross sections across each transect T1 through T6. For discussion of the topography colors in the transect plots, see Section A.1.



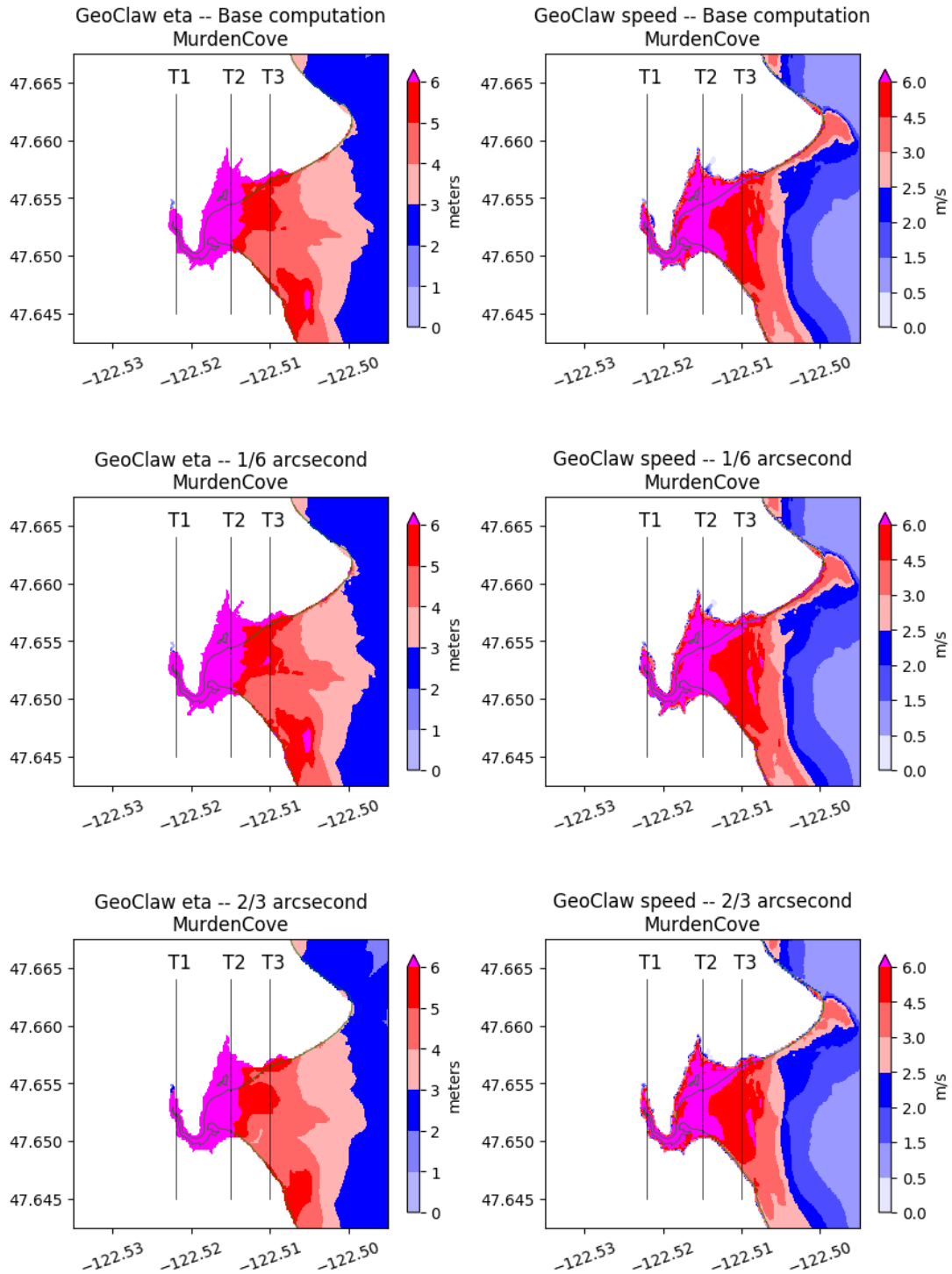


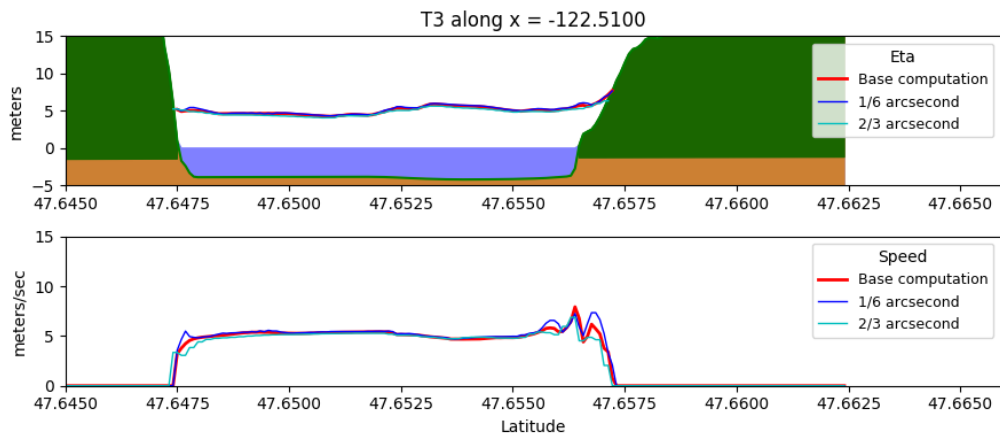
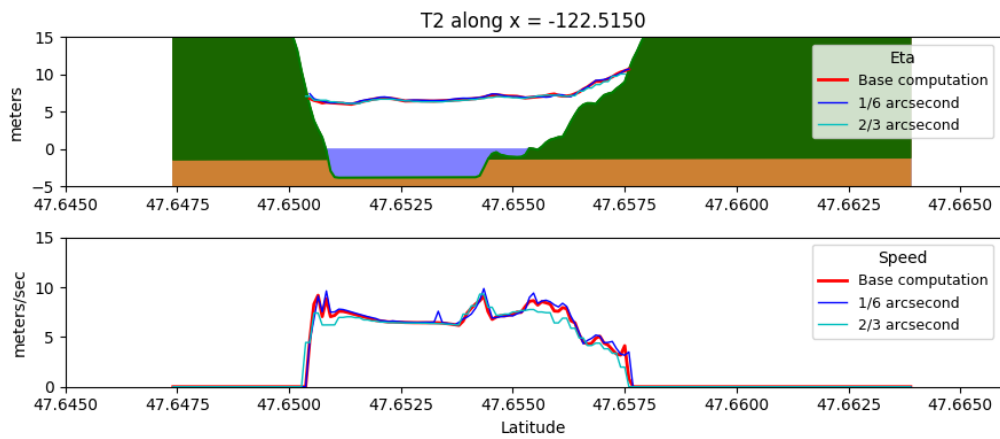
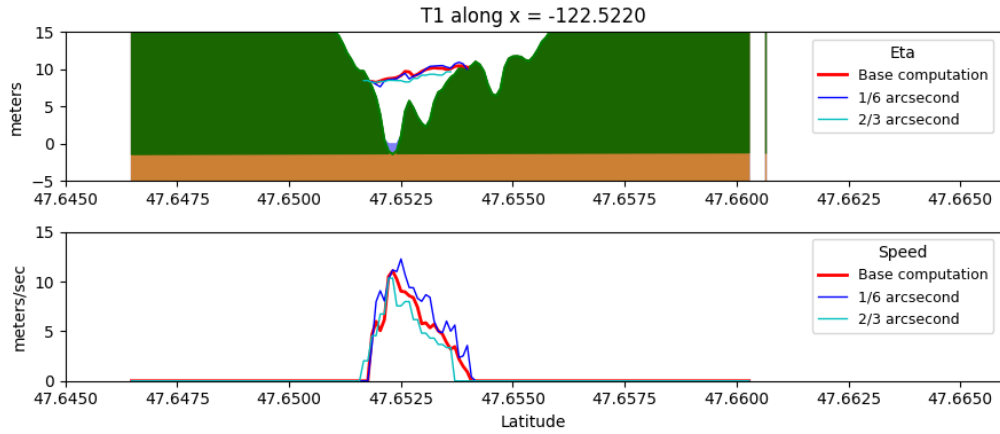


### C.1.2 Murden Cove

The plots below show sensitivity study results obtained with GeoClaw using the base parameters with resolution 1/3" (top) and varying the finest grid resolution to 1/6" (middle) or 2/3" (bottom).

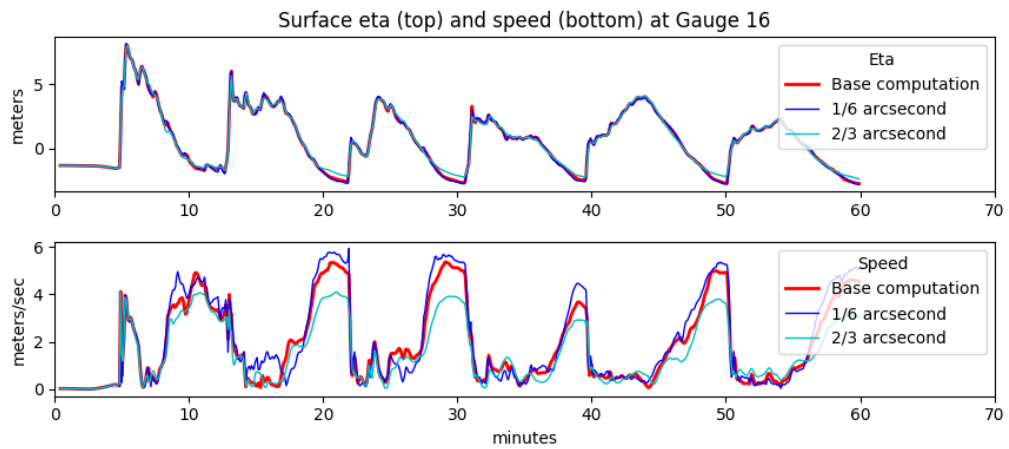
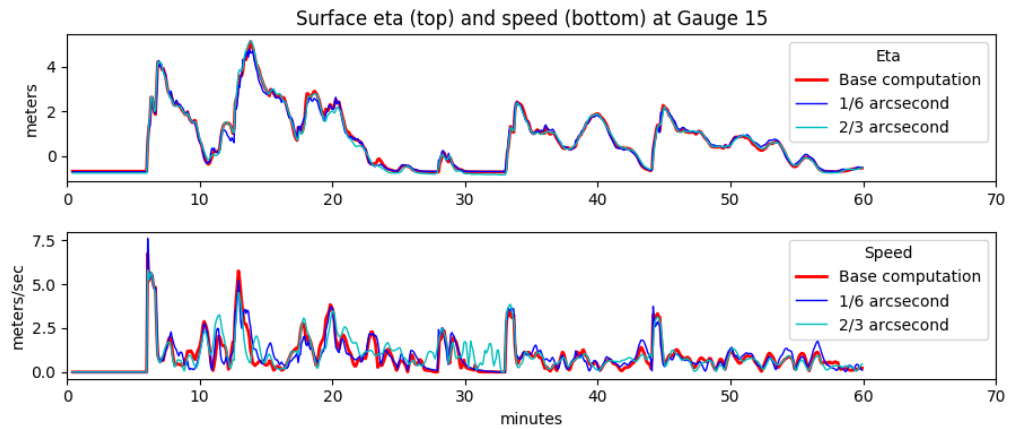
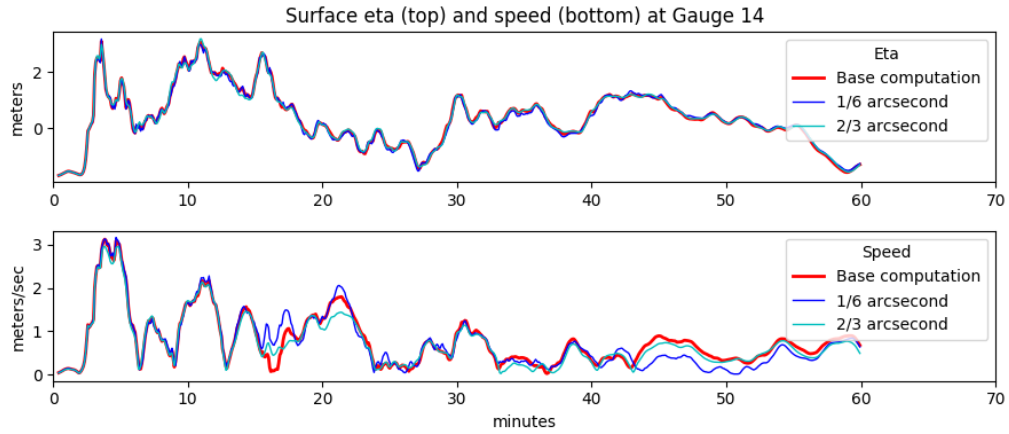
Figures on the next two page show cross sections across each transect T1 through T3. For discussion of the topography colors in the transect plots, see Section A.1.





### C.1.3 Gauge comparisons

The figures below show comparison of the synthetic tide gauge results at gauges in Eagle Harbor and Murden Cove. Comparison of GeoClaw results is shown, when the finest grid resolution is varied from the base computation resolution of  $1/3''$  to  $1/6''$  or  $2/3''$ .



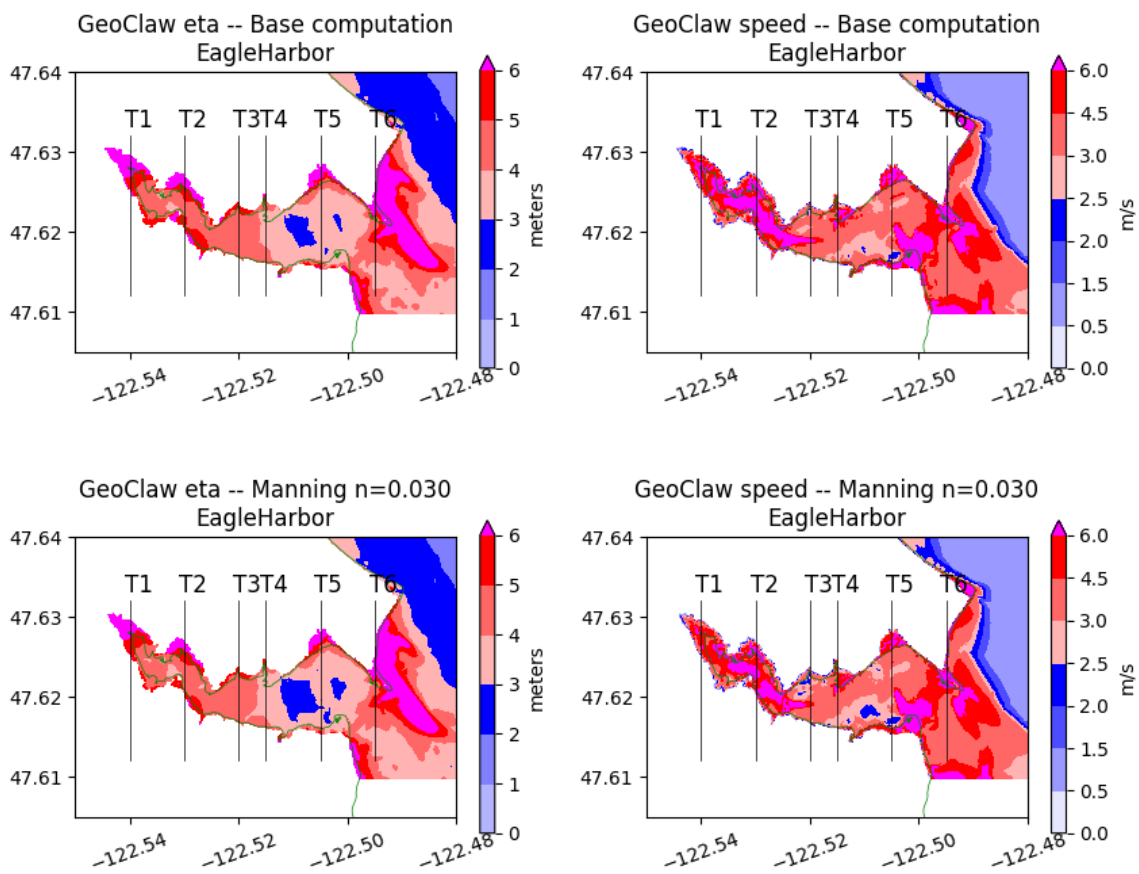
## C.2 Sensitivity to Manning coefficient

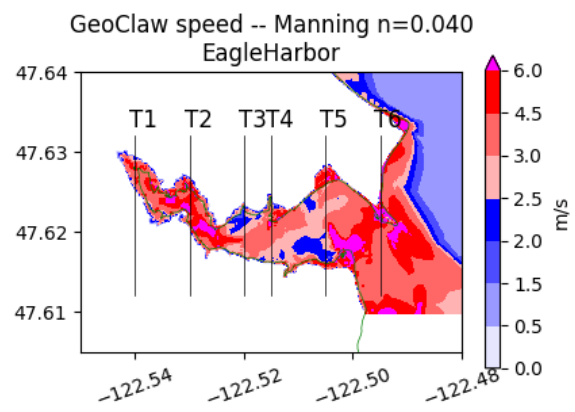
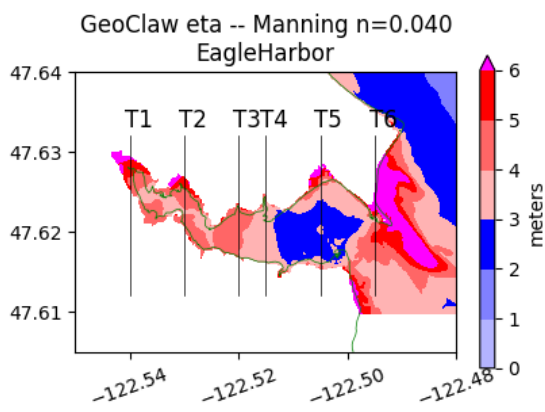
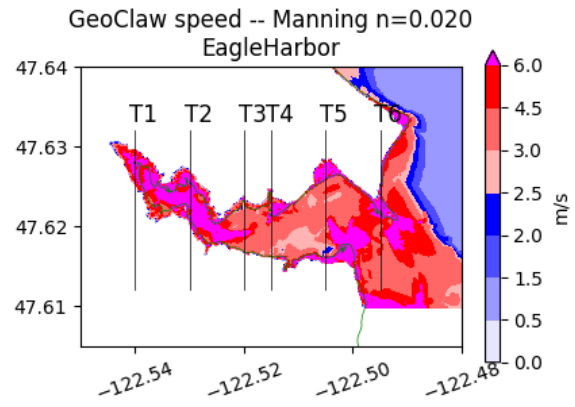
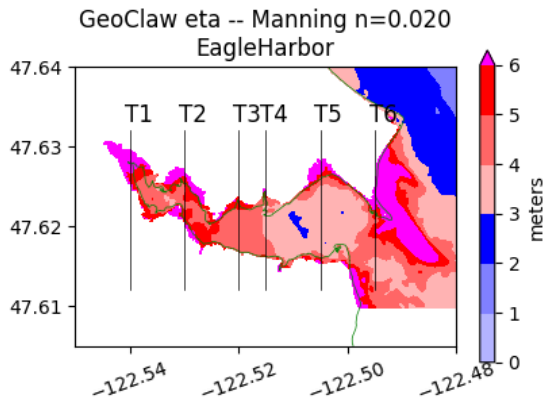
The GeoClaw simulations were run over the smaller domain with different Manning coefficients of bottom friction. The “base computation” uses  $n = 0.025$ . The value  $n = 0.03$  was used in the MOST simulations. We also ran tests using  $n = 0.02$  and  $0.04$ .

### C.2.1 Eagle Harbor

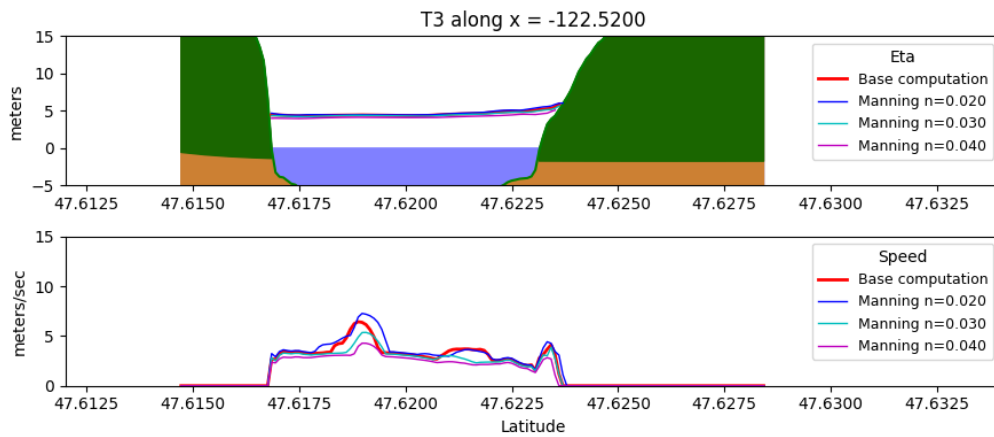
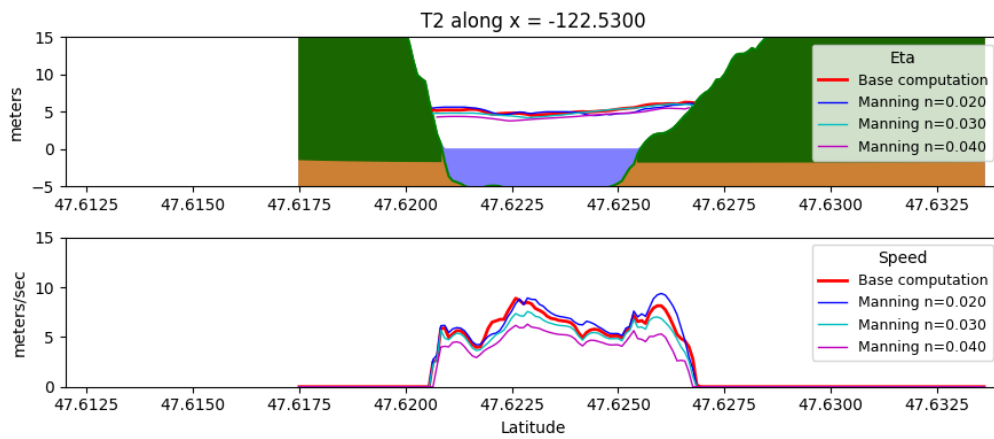
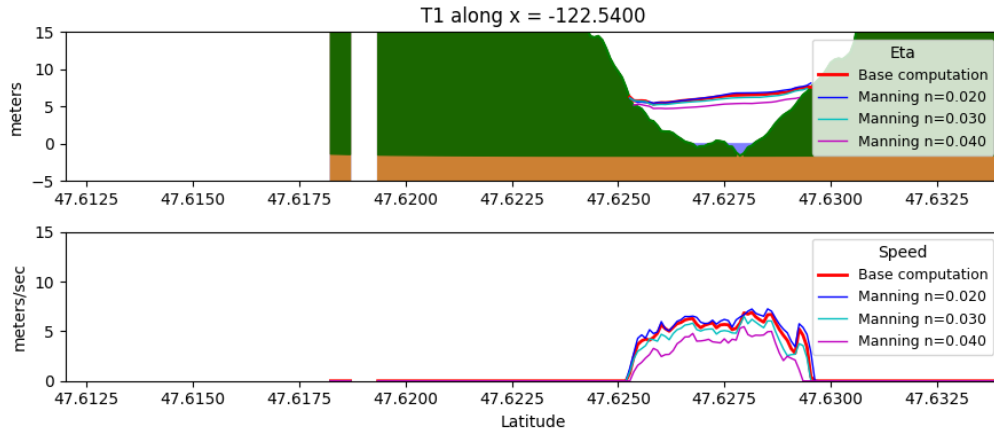
The plots below show sensitivity study results obtained with GeoClaw using the base parameters with Manning coefficient  $n = 0.025$  and varying the Manning coefficient to  $n = 0.02, 0.03, \text{ or } 0.04$ .

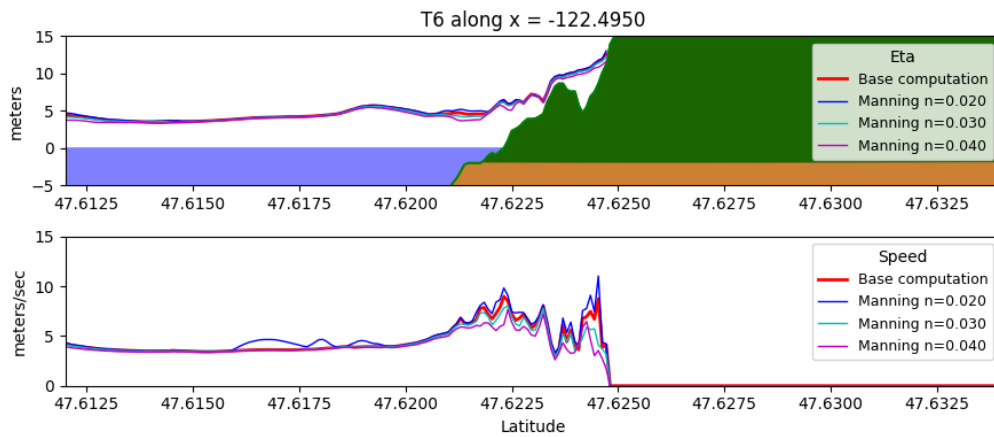
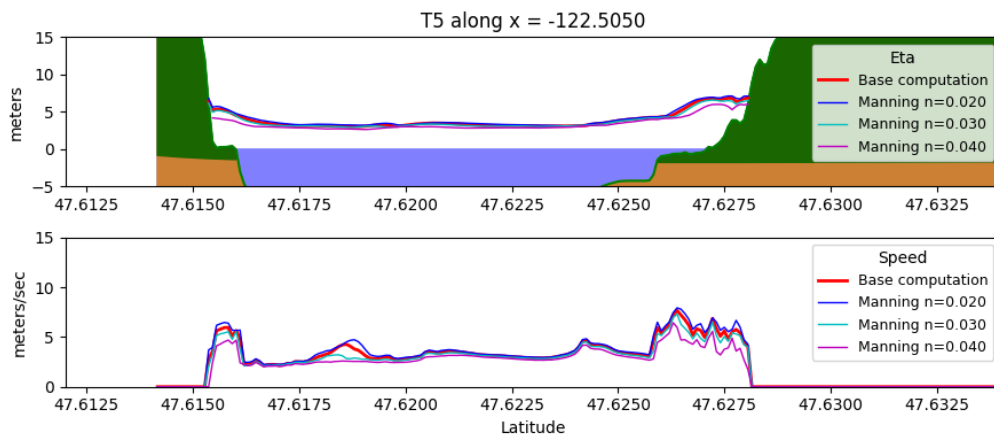
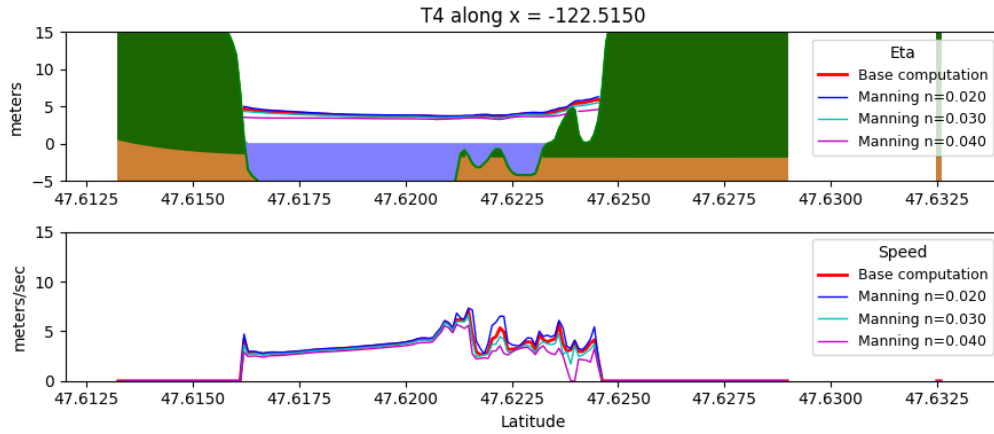
Figures on the following two page show cross sections across each transect T1 through T6. For discussion of the topography colors in the transect plots, see Section A.1.







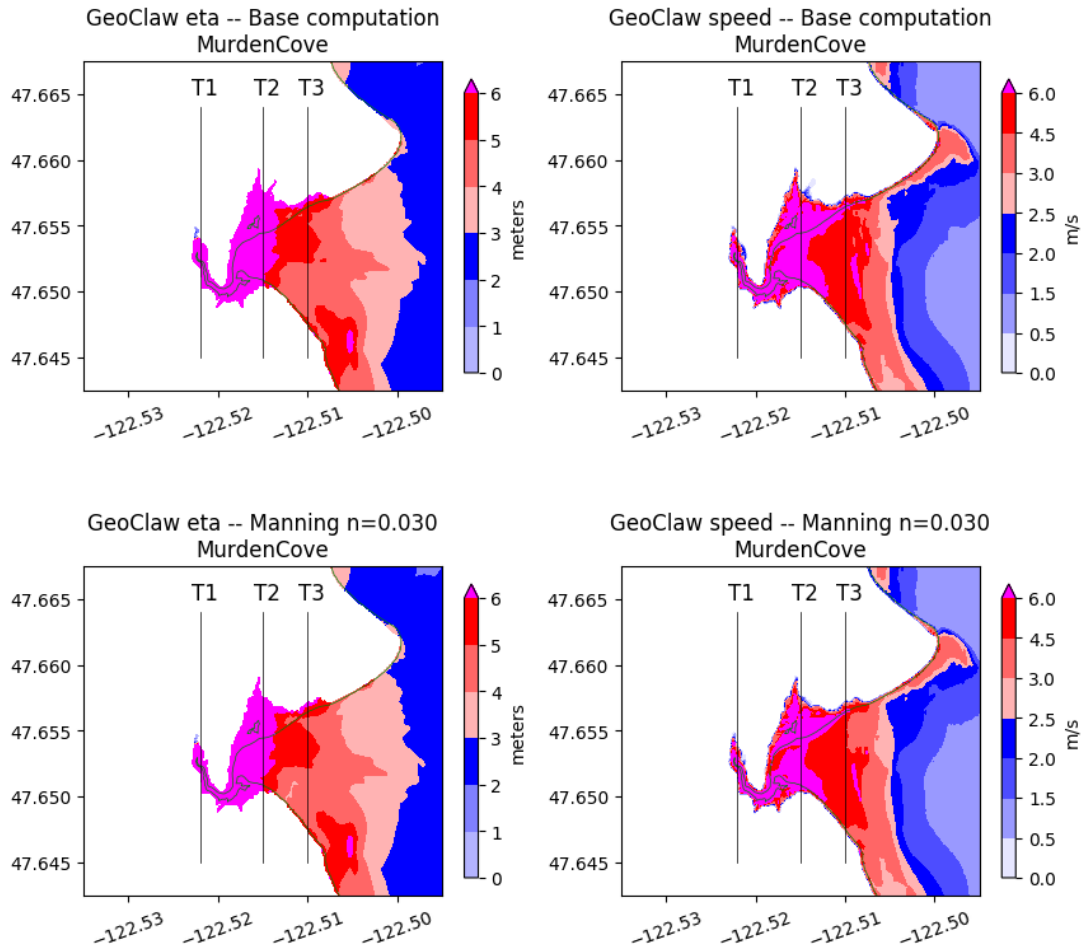


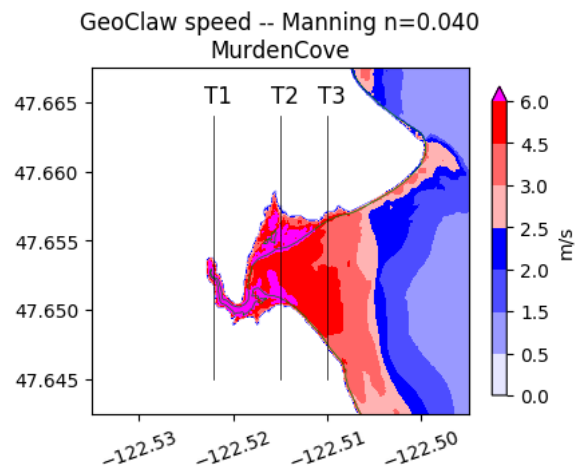
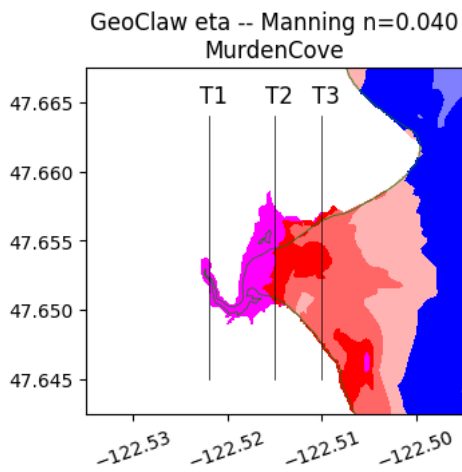
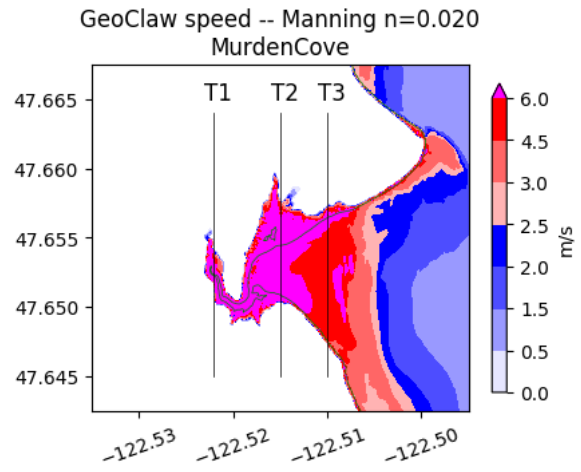
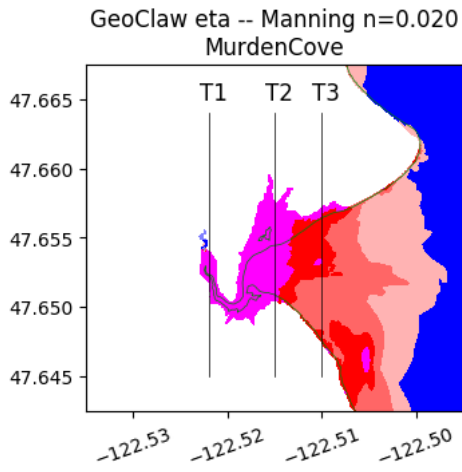


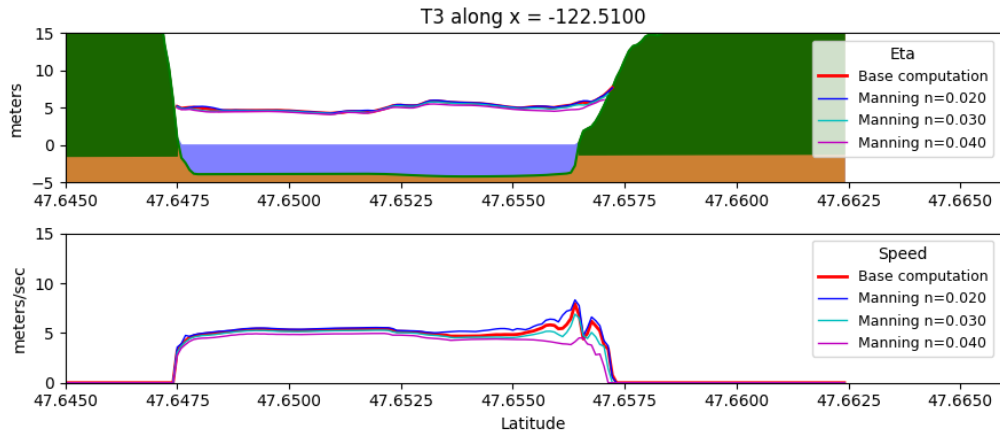
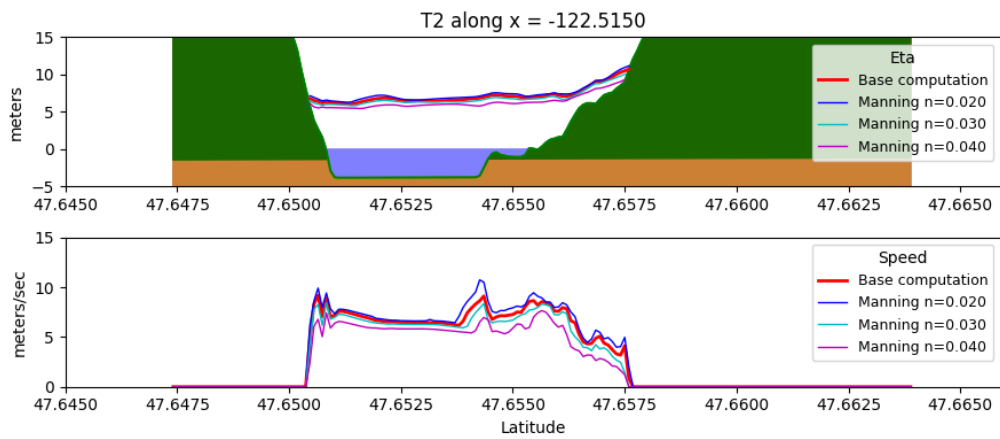
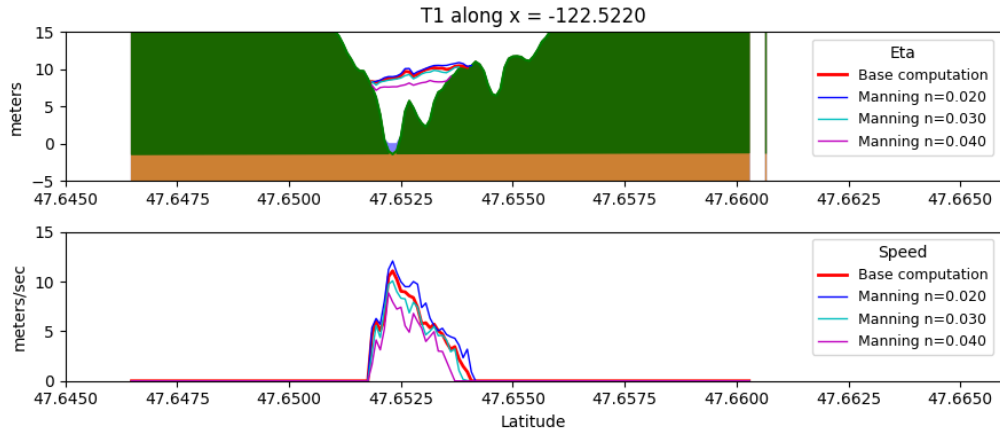
### C.2.2 Murden Cove

The plots below show sensitivity study results obtained with GeoClaw using the base parameters with Manning coefficient  $n = 0.025$  and varying the Manning coefficient to  $n = 0.02$ ,  $0.03$ , or  $0.04$ .

Figures on the following two page show cross sections across each transect T1 through T3. For discussion of the topography colors in the transect plots, see Section A.1.

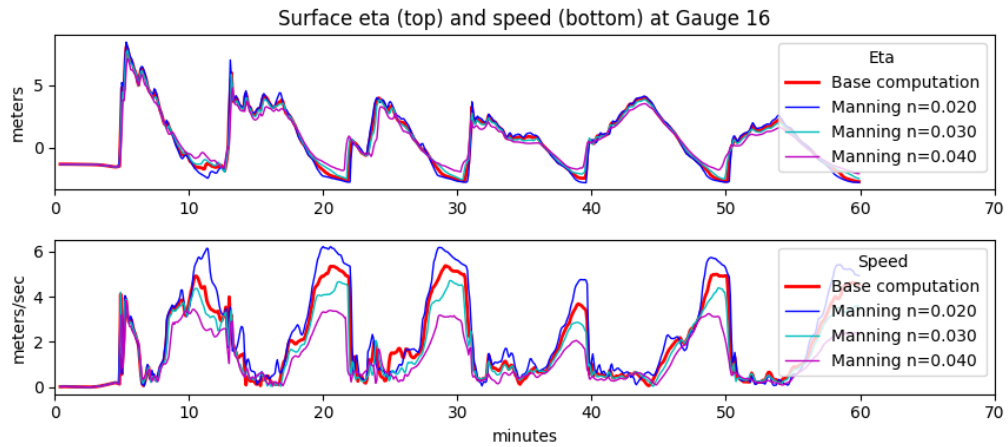
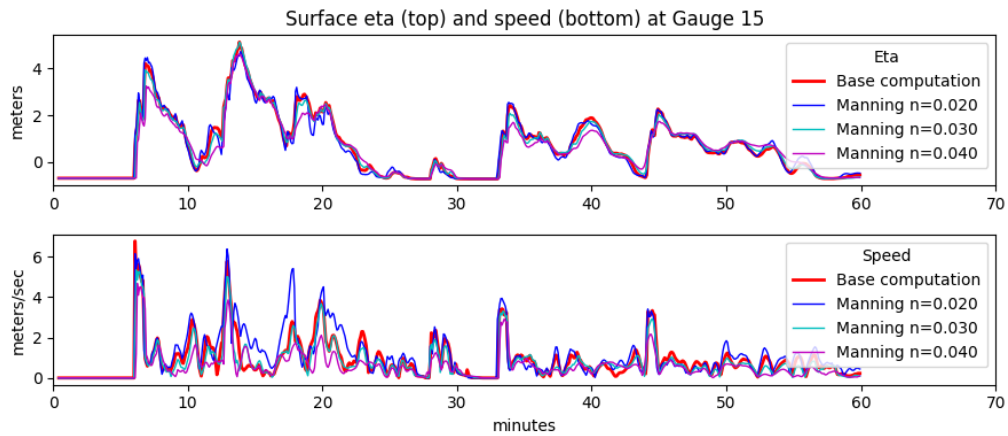
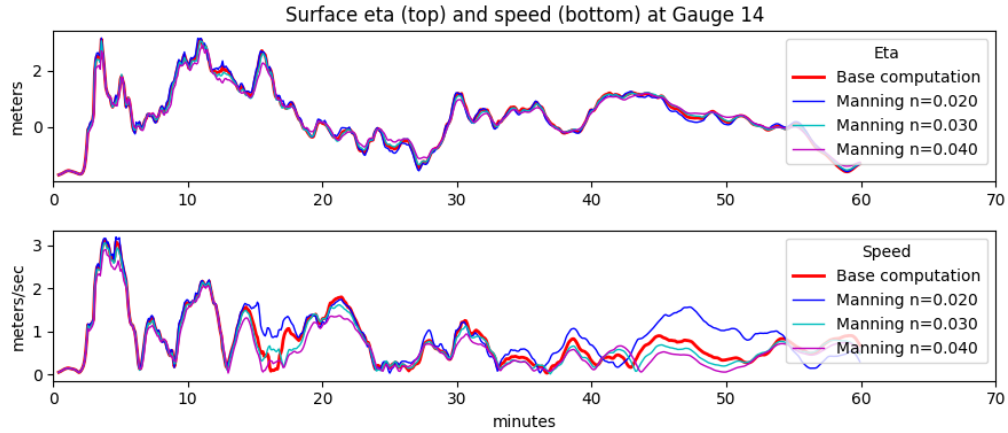






### C.2.3 Gauge comparisons

The figures below show comparison of the synthetic tide gauge results at gauges in Eagle Harbor and Murden Cove. Comparison of GeoClaw results is shown, when the Manning coefficient is varied from the base value of 0.025 to 0.02, 0.03, or 0.04.



## D GeoClaw Data format

For each earthquake source, output data is provided as csv files.

### Format of fgmax output csv files.

The maximum depth, speed, and other quantities of interest over the full duration of the simulation is recorded in the csv files:

- `L1_bainbridge_fgmax.csv` results using the CSZ-L1 source,
- `SF_bainbridge_fgmax.csv` results using the Seattle Fault event SF-L.

Each file has a one-line header followed by a line of data for each fgmax point in the region. The columns are:

1. longitude (degrees)
2. latitude (degrees)
3. topography elevation  $z$  from the DEM (meters)
4. topography value  $B$  from GeoClaw for the grid cell (m)
5. subsidence  $dz$  interpolated from deformation file (m)
6. maximum fluid depth  $h$  (m)
7. maximum fluid velocity (m/s)
8. maximum momentum flux ( $\text{m}^3/\text{s}^2$ )
9. arrival time (seconds)

The fgmax points are exactly aligned with the  $1/3''$  DEM, although sampled at  $1/3''$  in longitude. The finest level computational finite volume grid is also aligned so that cell centers are exactly at the fgmax points, and  $z$  in column 3 is the value from the DEM at this point. However, the topography value  $B$  used in a grid cell in GeoClaw is obtained by integrating a piecewise bilinear function that interpolates the  $1/3''$  DEM, and so  $B$  does not exactly equal  $z$ .

### Format of gauge output csv files.

The gauge time series is recorded in csv files with columns

1. time (seconds post-quake),
2. topography value  $B$  from GeoClaw at gauge location (m),
3. depth of water at gauge in simulation (m),
4. E/W velocity  $u$  at gauge (m/s),
5. N/S velocity  $v$  at gauge (m/s).

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