

# DQG: Dual Quaternion Guidance for the SPLICE Project

**Taylor P. Reynolds**

Presented to: Blue Origin

February 10, 2021



# Overview

The SPLICE Project

Problem Formulation

Sequential Convex Programming Implementation

Future Additions and Improvements

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Problem Formulation

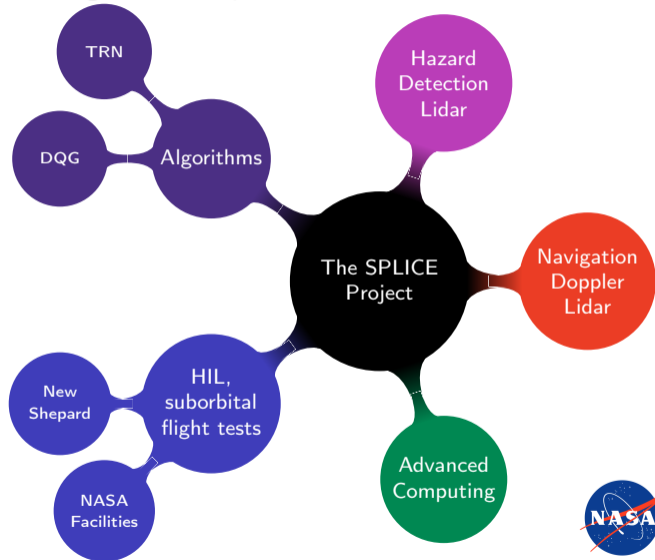
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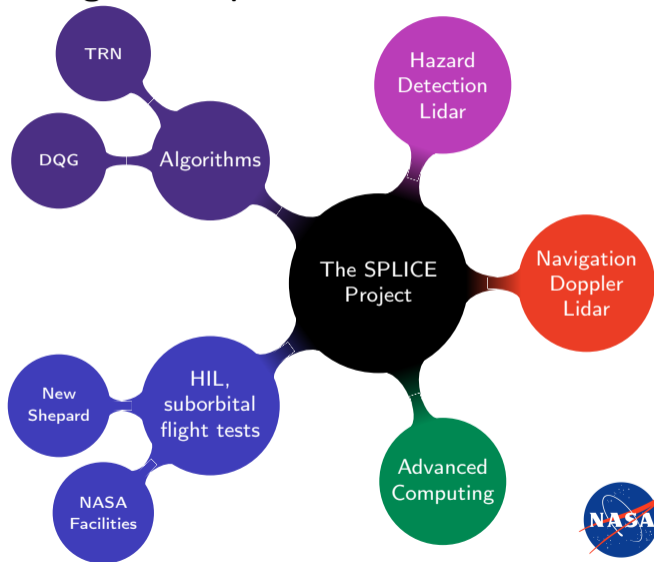
# Safe & Precise Landing - Integrated Capabilities Evolution

## Objectives

- Modernize precision landing technology
- Create target-agnostic solutions
- Achieve landing accuracy of  $\mathcal{O}(10)$  m



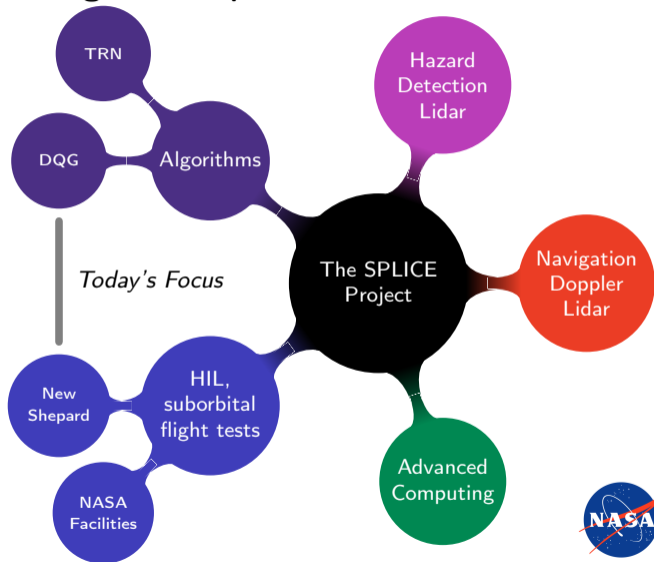
# Safe & Precise Landing - Integrated Capabilities Evolution



# Safe & Precise Landing - Integrated Capabilities Evolution

## Collaborators

- JSC<sup>1</sup>, LaRC, GSFC, JPL, AFRC, MSFC
- Draper, Blue Origin, Coherent Applications, Masten Space Systems, ...
- UW, Texas A&M, ...



<sup>1</sup>All funding through NASA's STMD



# DQG Algorithm Development

## University of Washington:

- Basic research on:
  - solution of nonconvex OCPs
  - problem formulations for lunar descent
- Develop Matlab-based toolbox to test and compare formulations and solution methods
- Develop flight code prototype in C/C++

### Team:

TPR, M. Szmuk, D. Malyuta  
M. Mesbahi, B. Açıkmeşe



## Draper Laboratory:

- Develop cFS application for DQG
- Implement DQG prototype on SPLICE compute hardware

### Team:

Javier Doll  
Matt Fritz, Tim Barrows



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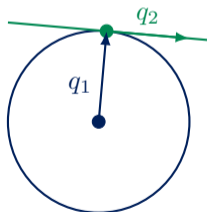


# Dual Quaternions

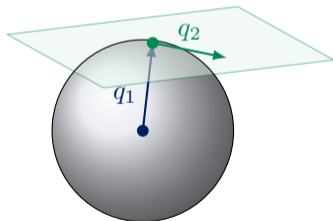
- A unit dual quaternion,  $\tilde{q}$ , satisfies two properties:

$$\tilde{q} = \begin{bmatrix} q_1 \\ q_2 \end{bmatrix}_{8 \times 1} \quad \text{where } q_1^\top q_1 = 1, \quad \text{and } q_1^\top q_2 = 0.$$

- DQG uses a right-handed, Hamiltonian, scalar-last convention
- The geometry of unit dual quaternions in lower dimensions:



dimension: 2



dimension: 3

?

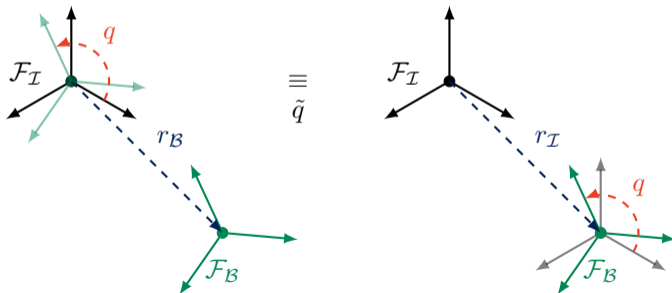
dimension: 4

## Dual Quaternions & Rigid Body Motion

- The unit dual quaternion  $\tilde{q}$  represents the pose of  $\mathcal{F}_B$  with respect to  $\mathcal{F}_I$ :

$$\tilde{q} = \begin{bmatrix} q \\ \frac{1}{2}q \otimes r_B \end{bmatrix} \equiv \begin{bmatrix} q \\ \frac{1}{2}r_I \otimes q \end{bmatrix} \quad \text{and} \quad \tilde{\omega} = \begin{bmatrix} \omega_B \\ v_B \end{bmatrix}$$

- The dual velocity  $\tilde{\omega}$  is composed of angular velocity and  $v_B = \dot{r}_B + \omega_B^\times r_B$



# Optimal Control Problem

Cost Function

$$\max m(t_f)$$

[C]

Dual Quaternion Dynamics

$$\dot{m} = -\alpha \|u_{\mathcal{B}}\|_2 \quad [\text{NC}]$$

$$\dot{\tilde{q}} = \frac{1}{2} \tilde{q} \otimes \tilde{\omega} \quad [\text{NC}]$$

$$J\dot{\tilde{\omega}} = \Phi u_{\mathcal{B}} - \tilde{\omega} \otimes J\tilde{\omega} + m\tilde{g}_{\mathcal{B}} \quad [\text{NC}]$$

- 15-dimensional state vector (1+8+6)
- $u_{\mathcal{B}}$  is thrust vector,  $g_{\mathcal{B}}$  is gravity
- matrix  $\Phi$  maps thrust to a force & torque

# Optimal Control Problem

## Cost Function

$$\max m(t_f)$$

[C]

## Dual Quaternion Dynamics

$$\dot{m} = -\alpha \|u_{\mathcal{B}}\|_2 \quad \text{[NC]}$$

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## Control Constraints

$$u_{\min} \leq \|u_{\mathcal{B}}\|_2 \leq u_{\max} \quad \text{[NC]}$$

$$\|u_{\mathcal{B}}\|_2 \leq \sec \delta_{\max} z_{\mathcal{B}}^{\top} u_{\mathcal{B}} \quad \text{[C]}$$

$$-\dot{u}_{z,\max} \leq z_{\mathcal{B}}^{\top} u_{\mathcal{B}} \leq \dot{u}_{z,\max} \quad \text{[C]}$$

$$\|E_{xy} u_{\mathcal{B}}\|_2 \leq \dot{\delta}_{\max} z_{\mathcal{B}}^{\top} u_{\mathcal{B}} \quad \text{[C]}$$

- upper/lower throttle constraint
- gimbal angle constraint,  $z_{\mathcal{B}}$  is vertical direction
- approx. throttle rate constraint
- approx. gimbal angle constraint

# Optimal Control Problem

## Cost Function

$$\max \quad m(t_f) \quad [C]$$

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$$\dot{m} = -\alpha \|u_{\mathcal{B}}\|_2 \quad [NC]$$

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## State Constraints

$$-\tilde{q}^{\top} M_{\gamma} \tilde{q} + \|2E_d \tilde{q}\|_2 \cos \gamma_{\max} \leq 0 \quad [C]$$

$$\tilde{q}^{\top} M_{\theta} \tilde{q} + \cos \theta_{\max} \leq 0 \quad [C]$$

$$m_{dry} \leq m \quad [C]$$

$$\|E_v \tilde{\omega}\|_2 \leq v_{\max} \quad [C]$$

$$\|E_w \tilde{\omega}\|_{\infty} \leq \omega_{\max} \quad [C]$$

- approach angle (glide slope) and tilt angle expressed as quadratic functions of  $\tilde{q}$
- mass, speed, and angular rate constraints

# Optimal Control Problem

## Cost Function

$$\max \quad m(t_f) \quad [\text{C}]$$

## Dual Quaternion Dynamics

$$\dot{m} = -\alpha \|u_{\mathcal{B}}\|_2 \quad [\text{NC}]$$

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$$\|E_v \tilde{\omega}\|_2 \leq v_{\max} \quad [\text{C}]$$

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## Boundary Conditions

$$m(t_0) = m_{ic} \quad [\text{C}]$$

$$\tilde{q}(t_0) = b_{\tilde{q}}(q(t_0)), \quad b_f(\tilde{q}(t_f)) \leq 0 \quad [\text{C}]$$

$$\tilde{\omega}(t_0) = b_{\tilde{\omega}}(q(t_0)), \quad \tilde{\omega}(t_f) = \tilde{\omega}_f \quad [\text{NC}]$$

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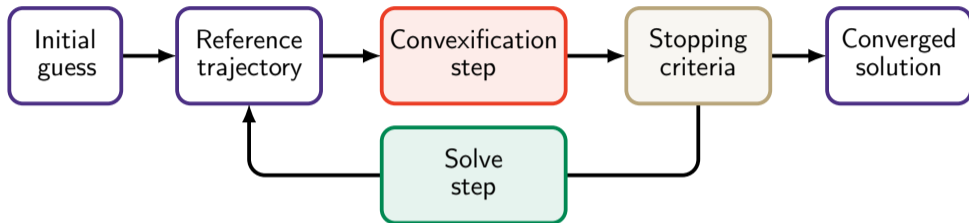
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# Sequential Convex Programming



- Solve nonconvex OCP by solving a sequence of convex approximations
- Initial guess obtained by simply interpolating between current and desired final states
- Converged solution satisfies dynamics to pre-determined precision

M. Szmuk et al. *JGCD*, 2020 | TPR et al. *JGCD*, 2020.



## Solve Step

- Each iteration solves a **second-order cone program** using custom solver **BSOCP**<sup>1</sup>
- BSOCP is written in C++, but can generate C code tailored to the specific problem

### OCP

- convex cost function
- nonlinear, differential eq. constraints
- general ineq. and eq. constraints

$$\begin{aligned} \min_{u,p} \quad & J(x, u, p) \\ \text{s.t.} \quad & \dot{x} = f(x, u, p) \\ & 0 \geq g(x, u, p) \\ & 0 = h(x, u, p) \end{aligned}$$

### SOCP

- linear cost function
- affine, algebraic eq. constraints
- affine or second-order cone ineq. constraints

$$\begin{aligned} \min_z \quad & c^\top z \\ \text{s.t.} \quad & Az = b \\ & z \in \mathcal{C}_L \times \mathcal{C}_{Q_1} \times \cdots \times \mathcal{C}_{Q_m} \end{aligned}$$

<sup>1</sup>D. Dueri, 2018

## Solve Step

Solve  
step

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### Convexification

<sup>1</sup>D. Dueri, 2018

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### SOCP

- linear cost function
- affine, algebraic eq. constraints
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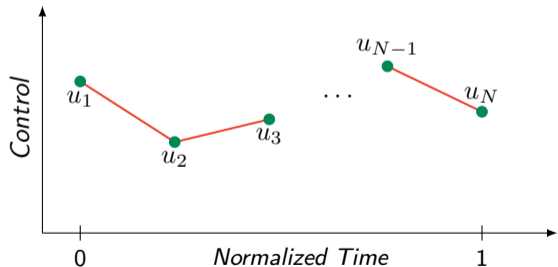
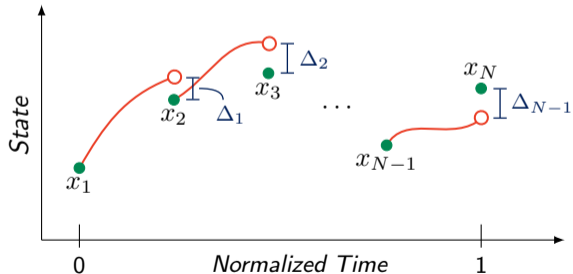
$$\begin{aligned} \min_z \quad & c^\top z \\ \text{s.t.} \quad & Az = b \\ & z \in \mathcal{C}_L \times \mathcal{C}_{Q_1} \times \cdots \times \mathcal{C}_{Q_m} \end{aligned}$$

Parsing

<sup>1</sup>D. Dueri, 2018

## Convexification: Propagation

- Assume the control can be affinely interpolated between a set of  $N$  time nodes
- Use an exact discretization; solution of linearized ODE via numerical integration
- Defects  $\Delta$  serve as an indicator of dynamic feasibility
- Properly implemented, this should take roughly  $\mathcal{O}(1)\%$  of the DQG's runtime



## Convexification: Constraint Approximation

## Control Constraints

$$u_{\min} \leq \|u_{\mathcal{B}}\|_2 \leq u_{\max} \quad \text{[NC]} \quad (\text{linearized} + \text{SOC})$$

$$\|u_{\mathcal{B}}\|_2 \leq \sec \delta_{\max} z_{\mathcal{B}}^{\top} u_{\mathcal{B}} \quad \text{[C]} \quad (\text{SOC})$$

$$-\dot{u}_{z,\max} \leq z_{\mathcal{B}}^{\top} u_{\mathcal{B}} \leq \dot{u}_{z,\max} \quad \text{[C]} \quad (\text{affine})$$

$$\|E_{xy} u_{\mathcal{B}}\|_2 \leq \dot{\delta}_{\max} z_{\mathcal{B}}^{\top} u_{\mathcal{B}} \quad \text{[C]} \quad (\text{SOC})$$

- Approach cone constraint is not an SOC, must linearize
- Max. violations of approx'd constraints tracked using parameter:  $\delta$

## State Constraints

$$-\tilde{q}^{\top} M_{\gamma} \tilde{q} + \|2E_d \tilde{q}\|_2 \cos \gamma_{\max} \leq 0 \quad \text{[C]} \quad (\text{linearized})$$

$$\tilde{q}^{\top} M_{\theta} \tilde{q} + \cos \theta_{\max} \leq 0 \quad \text{[C]} \quad (\text{SOC})$$

$$m_{dry} \leq m \quad \text{[C]} \quad (\text{affine})$$

$$\|E_v \tilde{\omega}\|_2 \leq v_{\max} \quad \text{[C]} \quad (\text{SOC})$$

$$\|E_w \tilde{\omega}\|_{\infty} \leq \omega_{\max} \quad \text{[C]} \quad (\text{affine})$$

- Each constraint enforced at  $N$  nodes
- To parse SOCP: can quantify the min. number of variables and rows of  $A$ ,  $b$

## Convexification: Constraint Approximation

## Boundary Conditions

At  $t_0$  :

$$m(t_0) = m_{ic} \quad [\text{C}] \quad (\text{affine})$$

$$\tilde{q}(t_0) = b_{\tilde{q}}(q(t_0)) \quad [\text{C}] \quad (\text{affine})$$

$$\tilde{\omega}(t_0) = b_{\tilde{\omega}}(q(t_0)) \quad [\text{NC}] \quad (\text{linearized})$$

At  $t_f$  :

$$b_f(\tilde{q}(t_f)) \leq 0 \quad [\text{C}] \quad (\text{SOC})$$

$$\tilde{\omega}(t_f) = \tilde{\omega}_f \quad [\text{C}] \quad (\text{affine})$$

- Specified:

- initial mass, (inertial) position and velocity, angular rates
- final attitude, (inertial) velocity, angular rates

$$b_{\tilde{q}}(q(t_0)) = \begin{bmatrix} q(t_0) \\ \frac{1}{2} r_{\mathcal{I}} \otimes q(t_0) \end{bmatrix}$$

$$b_{\tilde{\omega}}(q(t_0)) = \begin{bmatrix} \omega_{\mathcal{B}}(t_0) \\ q(t_0)^* \otimes v_{\mathcal{I}}(t_0) \otimes q(t_0) \end{bmatrix}$$

$$b_f(\tilde{q}(t_f)) = \|2E_d \tilde{q}(t_f) - c'\|_2 - \varepsilon_{\text{miss}}$$

where  $E_d = \mathbf{diag} \{0_{4 \times 4}, I_4\}$

## Trust Regions and Virtual Control

- Algorithmic modifications to ensure:
  - Each SOCP is feasible and bounded
  - Iterates kept “close” to the reference used for approximation
- **Virtual control** added to all approximated constraints:

$$\text{[NC]} : h(x) = 0 \quad \implies \quad \text{[C]} : h(\bar{x}) + \nabla h(\bar{x})^\top (x - \bar{x}) + \nu = 0$$

where  $\nu$  is *unconstrained* but highly *penalized* in the cost.

- **Trust region** added as additional constraints:

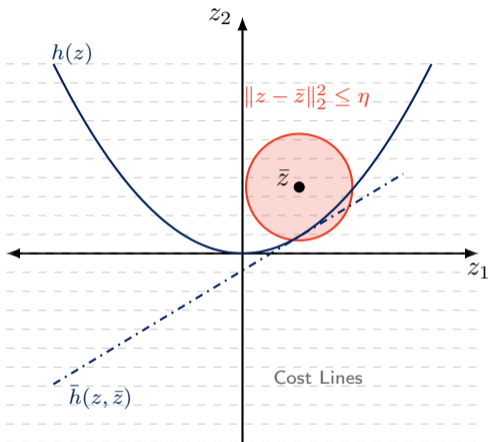
$$\|x - \bar{x}\|_2^2 + \|u - \bar{u}\|_2^2 \leq \eta \quad \text{and} \quad \|p - \bar{p}\|_2^2 \leq \eta_p$$

where  $\eta, \eta_p$  are chosen by the solver and modestly penalized in the cost.

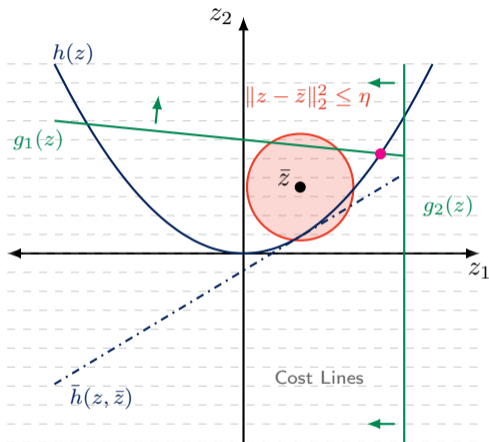
### Cost Function

$$\max \quad m(t_f) - w_{tr}^\top \eta - w_{tr,p} \eta_p - w_{vc} \sum_k \|\nu_k\|_1$$

## Trust Regions and Virtual Control



**Artificial Unboundedness:** cost function is unbounded without a trust region



**Artificial Infeasibility:** no feasible solution with approximated constraint  $\bar{h}$



# Stopping Criteria

## Criteria:

- ① small defects & constraint violation  $\max \{ \max_k \Delta_k, \delta \} \leq \varepsilon_\Delta$
- ② small state change  $\max_k \|x_k - \bar{x}_k\|_2 \leq \varepsilon_x$
- ③ small final mass change  $|m_N - \bar{m}_N| \leq \varepsilon_m$

## Logic:

$$\text{① AND ( ② OR ③ )}$$

- ➔  $\varepsilon_\Delta$  measures “feasibility”, both dynamic and approx’d constraints
- ➔  $\varepsilon_m$  used to stop if optimality not sufficiently improving
- ➔ Control changes ignored: large thrust change can have small impact on state trajectory

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## Mission-Specific Initial Guess

- Currently, DQG uses a very simple initialization:

$$x_k = \left( \frac{N-k}{N-1} \right) x_{ic} + \left( \frac{k-1}{N-1} \right) x_{fc} \quad \text{and} \quad u_k = m_k g_{\mathcal{B}}, \quad k = 1, \dots, N$$

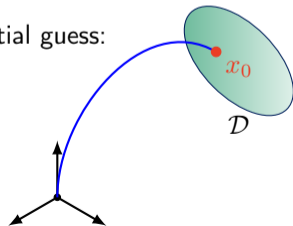
where  $x_{ic}$  and  $x_{fc}$  are boundary conditions,  $g_{\mathcal{B}}$  is gravity in body frame  $\mathcal{F}_{\mathcal{B}}$

- This trajectory is **not feasible** but works well enough and is easy to compute

Better initial guess  $\Rightarrow$  fewer DQG iterations  $\Rightarrow$  lower runtime

- **Idea:** For a given mission, create a map from initial condition to initial guess:

$$\Psi : \mathcal{D} \rightarrow \mathcal{X} \times \mathcal{U} \times \mathbb{R}_{++}$$
$$x_0 \mapsto \{x_k, u_k, t_f\}_{k=1}^N$$



# Custom Conversion to Standard Form

- BSOCP solves a problem in *standard form*:

$$\begin{aligned} \min \quad & c^\top z \\ \text{s.t.} \quad & Az = b \\ & z \in \mathcal{C}_L \times \mathcal{C}_{Q_1} \times \cdots \times \mathcal{C}_{Q_m} \end{aligned}$$

- Two possible methods to define data  $A$ ,  $b$ ,  $c$  and the cone dimensions:

## Generic Parser (Current)

- ✓ Ideal for prototyping
- ✗ Can add variables/constraints
- ✗ Opaque problem construction
- ✗ Uses dynamic memory allocation

## Handparsing

- ✗ Least flexible
- ✓ Guarantees smallest problem
- ✓ Most control over coding
- ✓ Uses static memory allocation

# Handparsing to Standard Form

$$z = \begin{bmatrix} \star z_1 \\ \star z_2 \\ \star z_3 \end{bmatrix} \left\{ \begin{array}{l} \text{block } v_1 \\ \text{block } v_2 \\ \text{block } v_3 \end{array} \right.$$

$$A = \begin{bmatrix} \star^A_P & 0 & 0 \\ \star^A_C & \star^A_s & \star^A_\chi \end{bmatrix} \begin{array}{l} \text{block } c_1 \\ \text{block } c_2 \end{array} \begin{bmatrix} \star^b_P \\ \star^b_C \end{bmatrix} = b$$

$$c = \begin{bmatrix} \star^c_\phi & \star^c_s & \star^c_\chi \end{bmatrix}$$

- Variables:

$v_1$ : used to write dynamics

$v_2$ : linear slack variables

$v_3$ : trust region and SOC slack variables

- Constraints:

$c_1$ : dynamics

$c_2$ : all other constraints

# Handparsing to Standard Form

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$$c = \begin{bmatrix} \star c_\phi & \star c_s & \star c_\chi \end{bmatrix}$$

- ➡ blocks  $\star$ : can be pre-parsed
- ➡ blocks  $\star$ : are updated each iteration

- Variables:

$v_1$ : used to write dynamics

$v_2$ : linear slack variables

$v_3$ : trust region and SOC slack variables

- Constraints:

$c_1$ : dynamics

$c_2$ : all other constraints

## State-Triggered Constraints (STC)

- STCs are constraints enforced conditionally based on the value of a *trigger function*

$$\underbrace{g(z) < 0}_{\text{trigger condition}} \Rightarrow \underbrace{h(z) \leq 0}_{\text{constraint condition}}$$

- Equivalently, we can enforce the nonconvex constraint

$$-\min(g(z), 0) h(z) \leq 0$$

- Models binary decisions using continuous variables
- Can combine trigger/constraint conditions using Boolean *AND* and *OR* operations

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M. Szmuk et al. *JGCD*, 2020

# State-Triggered Constraints (STC)

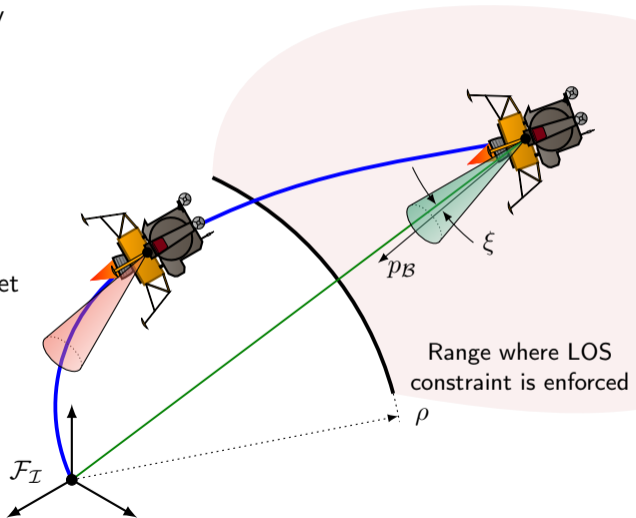
- Reconciles vehicle configuration with feasibility of optimal control problem

- Trigger: slant range larger than  $\rho$

$$g(\tilde{q}) = \rho - \|2E_d\tilde{q}\|_2$$

- Constraint: line of sight angle to landing target

$$h(\tilde{q}) = \tilde{q}^\top M_\xi \tilde{q} + \|2E_d\tilde{q}\|_2 \cos \xi_{\max} - \varepsilon$$





# State-Triggered Constraints (STC)

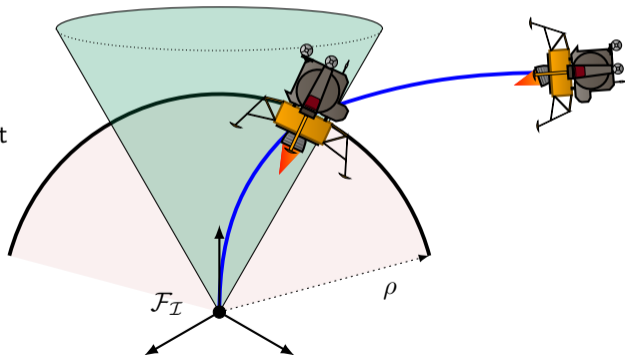
- Lunar descent orbits characteristically low altitude at large downrange distances

- Trigger: slant range small than  $\rho$

$$g(\tilde{q}) = \|2E_d\tilde{q}\|_2 - \rho$$

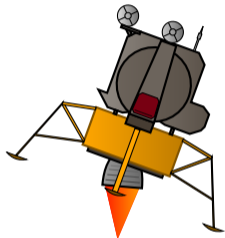
- Constraint: approach angle to landing target

$$h(\tilde{q}) = -\tilde{q}^\top M_\gamma \tilde{q} + \|2E_d\tilde{q}\|_2 \cos \gamma_{\max}$$



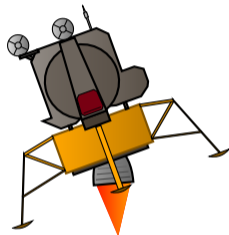
# Summary

- ➔ DQG solves a nonconvex optimal control problem in real-time
  - parameterizes pose with dual quaternions
  - includes several 6-DOF constraints
  - uses sequential convex programming
- ➔ Part of NASA's SPLICE project to modernize autonomous precision landing
  - algorithm dev: UW, Draper, JSC
  - HIL/flight demo: Blue Origin, Draper, JSC
- ➔ Plenty of room for improvement, both research-based and on the DQG implementation



Thank you!

email: [tpreynolds6@gmail.com](mailto:tpreynolds6@gmail.com)



**UW**

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R. Sostaric  
D. Matz  
E. Braden

**Draper**

J. Doll  
M. Fritz  
T. Barrows  
R. Loffi

# A Few Relevant Publications

## Algorithm Development

- TPR, M. Szmuk, D. Malyuta, M. Mesbahi, B. Açıkmeşe and J. M. Carson III, "Dual Quaternion Based Powered Descent Guidance with State-Triggered Constraints," *J. of Guidance, Control and Dynamics*, vol. 43, no. 9, pp. 1584-1599, 2020
- M. Szmuk, TPR, and B. Açıkmeşe, "Successive Convexification for Real-Time 6-DoF Powered Descent Guidance with State-Triggered Constraints," *J. of Guidance, Control, and Dynamics*, vol. 43, no. 8, pp. 1399-1413, 2020
- TPR, D. Malyuta, M. Mesbahi, B. Açıkmeşe and J. M. Carson III, "A Real-Time Algorithm for Non-Convex Powered Descent Guidance," *AIAA SciTech Forum*, Orlando, FL. 2020
- D. Malyuta, TPR, M. Szmuk, M. Mesbahi, B. Açıkmeşe, and J. M. Carson III, "Discretization Performance and Accuracy Analysis for the Powered Descent Guidance Problem," *AIAA SciTech Forum*, Orlando, FL. 2019

## SPLICE

- R. Sostaric, S. Pedrotty, J. M. Carson III, et al., "The SPLICE Project: Safe and Precise Landing Technology Development and Testing," *AIAA SciTech Forum*, Virtual, 2021
- J. M. Carson III, M. M. Munk, R. Sostaric, et al., "The SPLICE Project: Continuing NASA Development of GN&C Technologies for Safe and Precise Landing," *AIAA SciTech Forum*, Orlando, FL. 2020