

# **NOTCH SENSITIVITY OF COMPOSITE SANDWICH STRUCTURES**

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A part of the FAA Joint Advanced Materials & Structures Center of Excellence



# FAA Sponsored Project Information

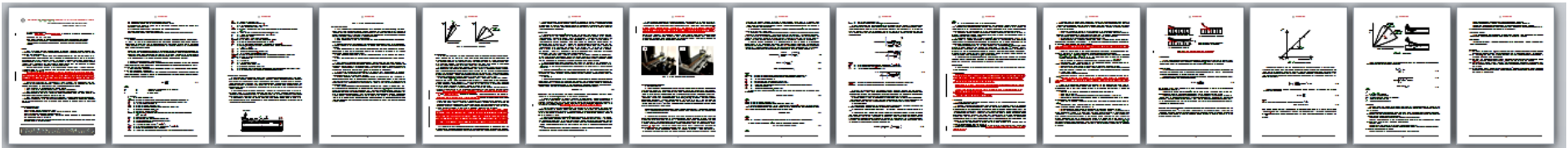
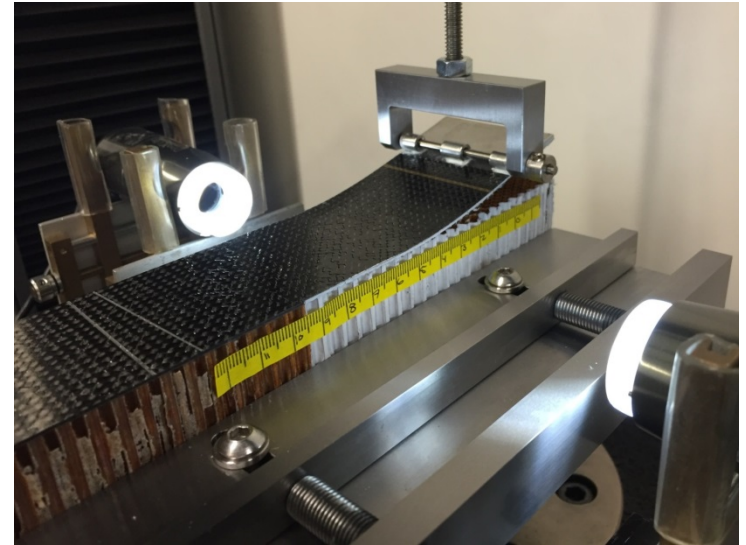
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- Graduate Student Researchers:  
**Marcus Stanfield**  
**Brad Kuramoto**  
**Martin Raming**
- FAA Technical Monitor: **Zhi-Ming Chen**
- Collaborators:  
**Materials Sciences Corporation**  
**Boeing (Charles Park)**  
**ASTM D30 (Composites)**

# *Status Update:*

## **Mode I Sandwich Fracture Mechanics Test Method**

- **Recently completed second round of ASTM balloting (September 2018) at D30.09 (sandwich) and D30 (main) levels**
- **Ballot negatives and comments currently being addressed**
- **Will reballot in January 2019 prior to next ASTM D30 meeting in March 2019 (SLC, UT)**



# *Status Update:*

## **Additional Sandwich Disbond Related Activities**

- **Mode I Single Cantilever Beam Fatigue Test**
  - New initiative for 2019
  - Focus on development of ASTM standard practice
- **Mode II Separated End Notched Flexure Test**
  - Evaluation by working group members
- **Sandwich Mixed Mode Bend (MMB) Test**
  - Evaluation by working group members
- **Sandwich Disbond Building Block Approach and Numerical Analysis Round Robin**
  - Working group focus for 2019

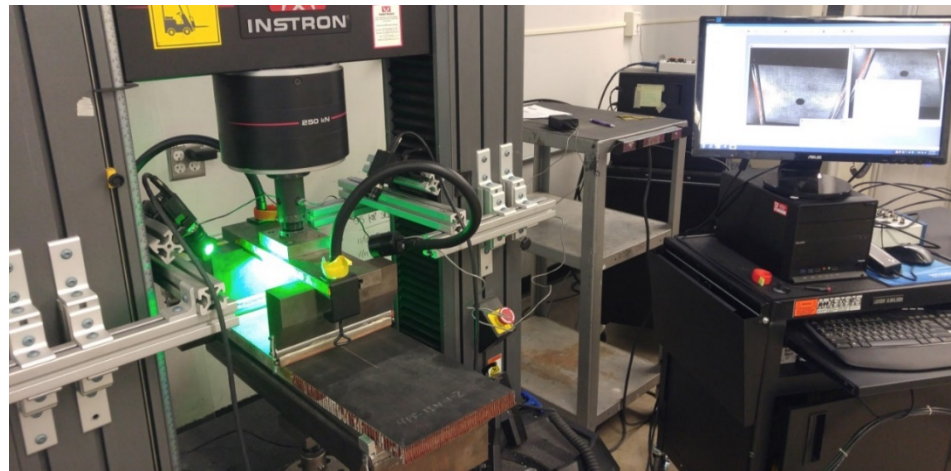




# *Status Update:*

## Sandwich Damage Tolerance

- **Draft standard of Sandwich composite Compression After Impact (SCAI) competed**
  - Balloted Spring 2018 ASTM D30 meeting
  - Updates to address negative votes in work
- **Draft practice of 4-Point Flexure After Impact (4-FAI) in progress**



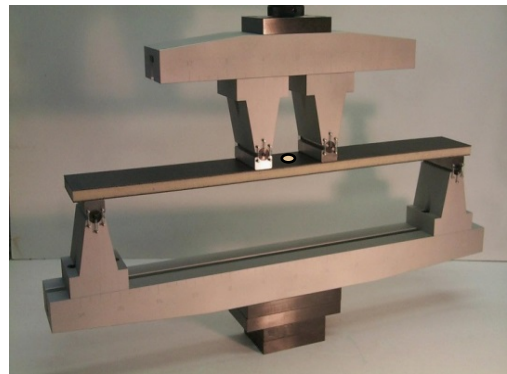
# Research Objectives:

## Notch Sensitivity of Sandwich Composites

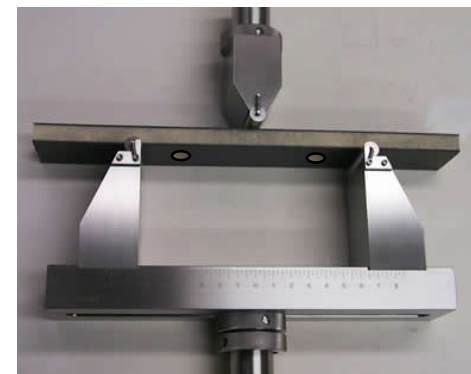
- Initial development of notched test methods and associated analysis methodologies for composite sandwich panels
- Documentation notched testing and analysis protocols in Composites Materials Handbook (CMH-17)
- Explore development of new ASTM standards for notch sensitivity of sandwich composites



**Sandwich Open Hole  
Compression**



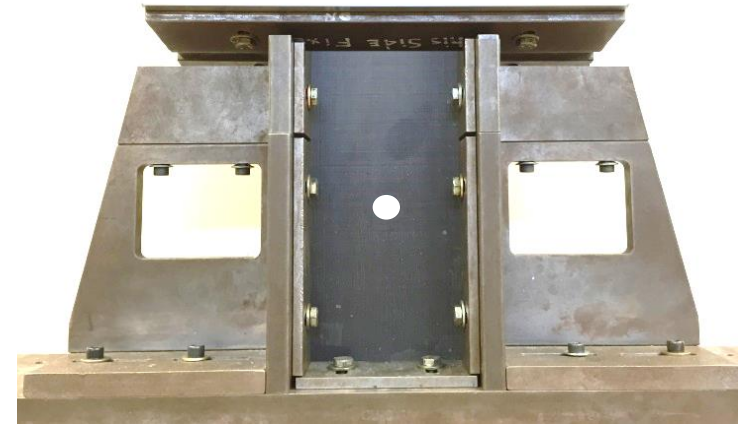
**Sandwich Open Hole  
Flexure**



**Sandwich Open Hole  
Shear**

# Testing Considerations: Sandwich Open Hole Compression

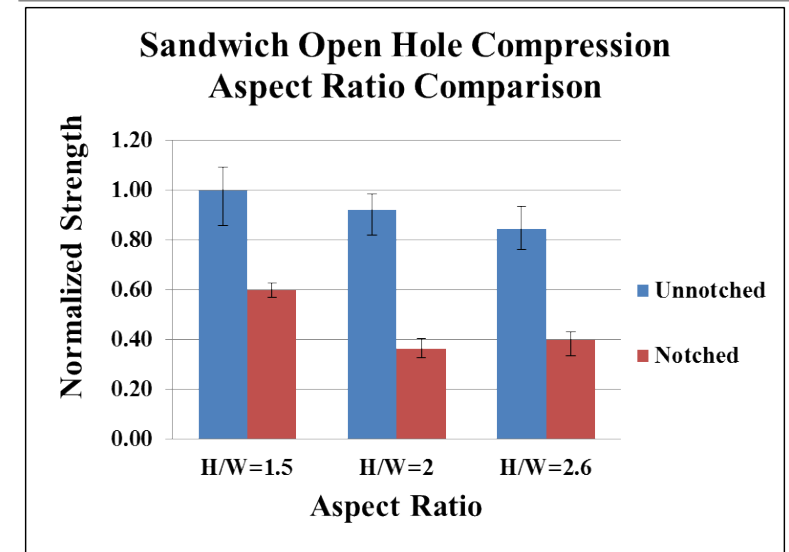
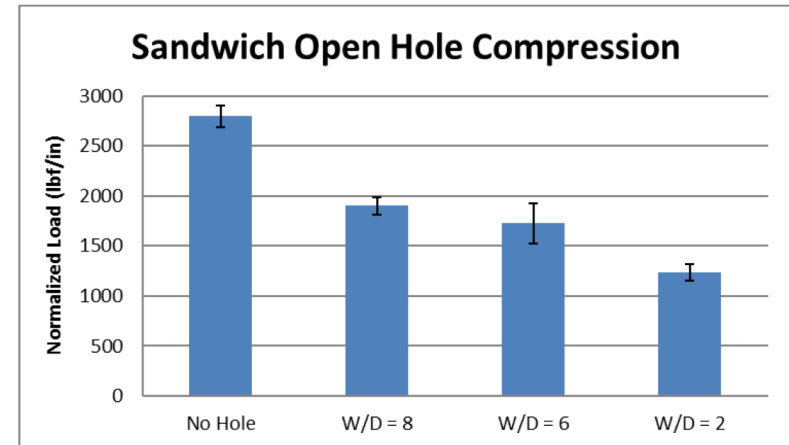
- **Test fixture/Specimen support**
  - **End supports**
    - Clamping top and bottom
    - Potting
  - **Side supports**
    - Knife edge
- **Specimen size**
  - Separation of central hole and boundary effects
  - Production of acceptable strength reductions
- **Strain measurement**
- **Specimen alignment**



Open hole compression fixture  
for monolithic composites

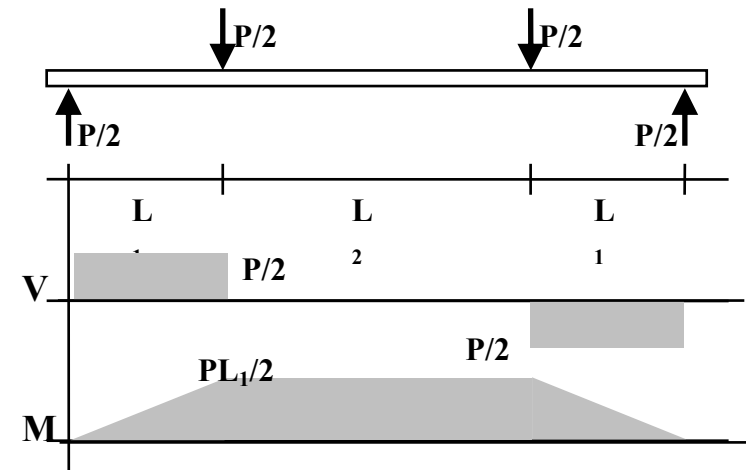
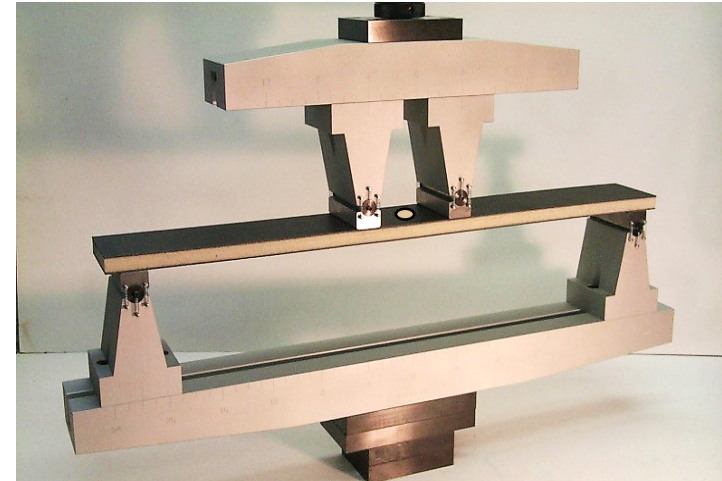
# Previous Work: Specimen Size

- **Hole Diameter (W/D)**
  - Legacy:  $W/D = 6$
  - Acceptable strength reduction
  - Minimal finite width effects
- **Aspect Ratio (H/W)**
  - $H/W = 2$
  - Acceptable strength reduction
- **Standard Configuration**
  - Width: 4 in.
  - Height: 8 in.
  - Hole Diameter: 0.67 in.



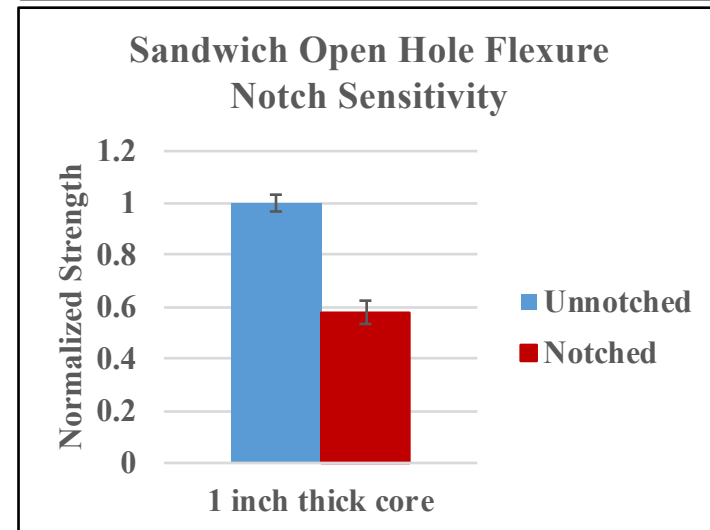
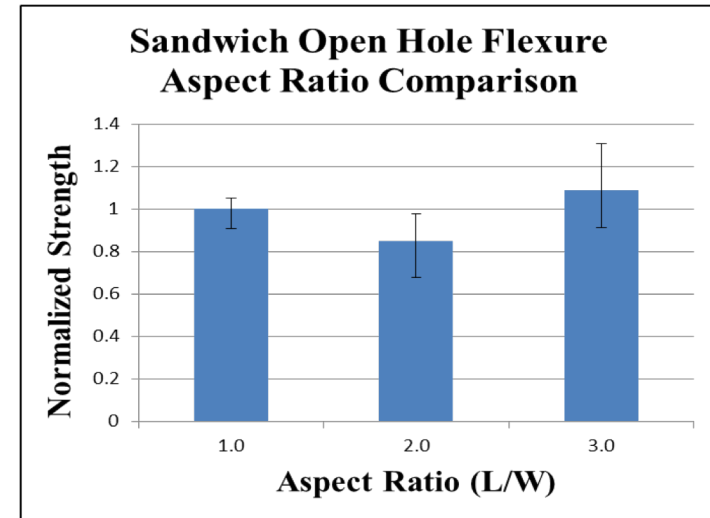
# Testing Considerations: Sandwich Open Hole Flexure

- Test fixture/specimen support
  - Inner span
    - Separation of notch and loading boundary effects
  - Outer span
    - Develop sufficient bending moment
    - Ensure failure in inner span
- Required specimen width
  - Separation of central hole and specimen edges
  - Production of acceptable strength reduction



# Previous Work: Specimen Size

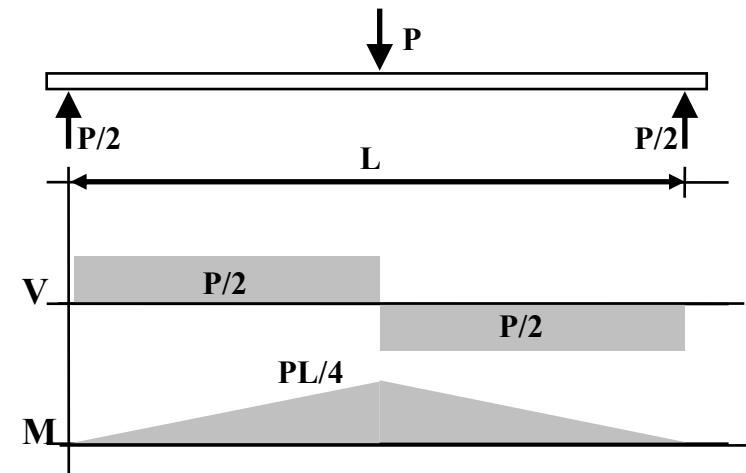
- **Standard configuration**
  - Specimen width  $W = 3$  in.
  - Hole diameter  $D = 0.5$  in.
  - Inner span  $L = 4$  in.
  - Outer span sized to ensure inner span failure
- **No inner span aspect ratio sensitivity ( $L/W$ )**
  - Inner span can be increased for measurement purposes





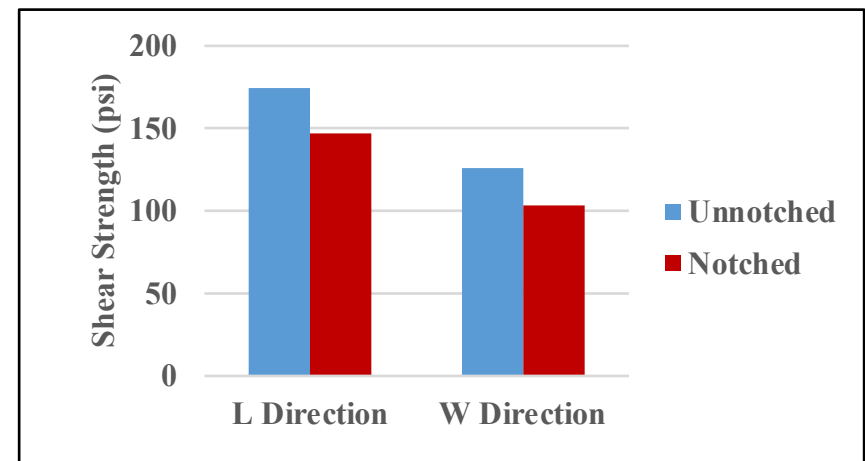
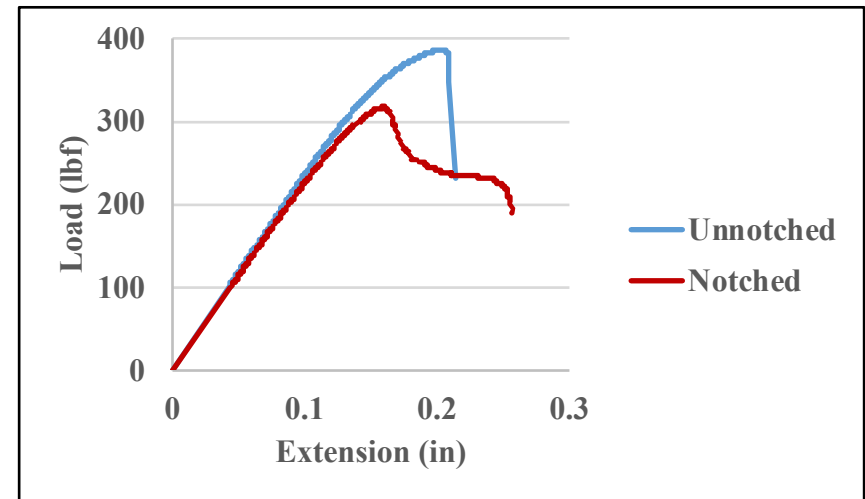
# Testing Considerations: Sandwich Open Hole Shear

- **Test fixture/specimen support**
  - **Span**
    - Locate notch to ensure shear failure in core at notch
- **Required specimen width**
  - Separation of central hole and specimen edges
  - Production of acceptable strength reduction



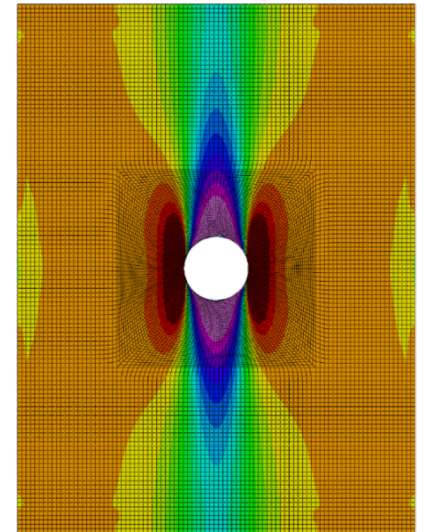
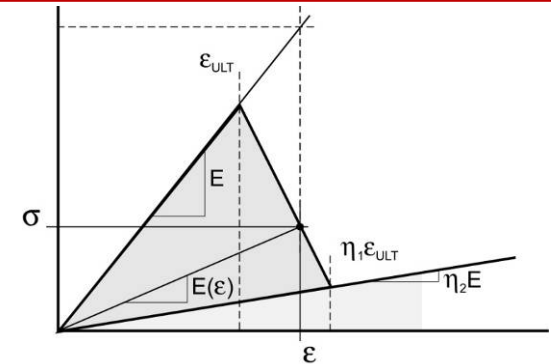
# Previous Work: Specimen Size

- **Standard configuration**
  - Specimen width  $W = 3$  in.
  - Hole diameter  $D = 0.5$  in.
  - Span  $L = 6$  in.
  - Notch located at quarter points
- **No significant notch effect**
- **Net section failure**
- **Similar behavior between ribbon and transverse directions**



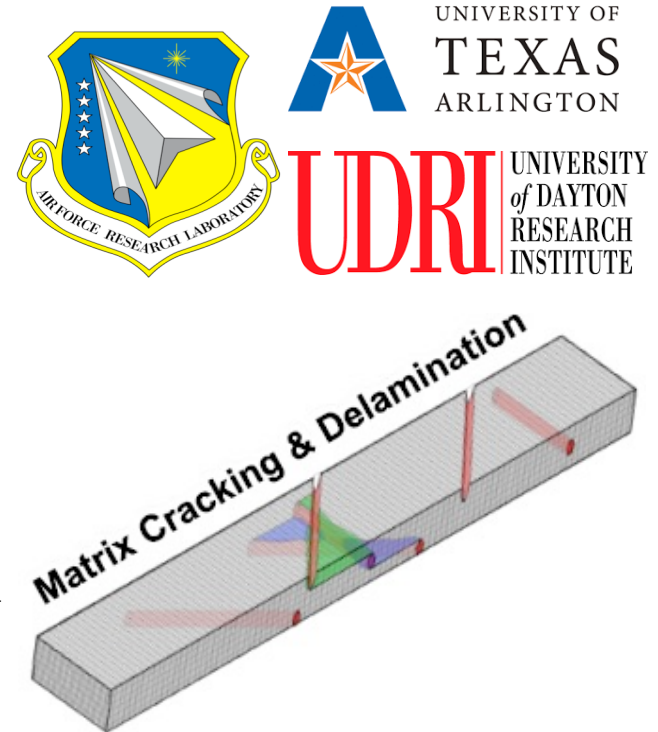
# Analysis of Notched Sandwich Specimens ABAQUS with NDBILIN:

- User-defined nonlinear material model (UMAT) for ABAQUS
- Developed by Materials Sciences Corp.
- Stiffness degradation based progressive damage model
  - Bilinear stiffness response used to model material damaged state
  - “Built in” laminated plate theory for elements
  - Lamina level stiffness degradation
  - Max. stress, max. strain or Hashin failure criteria for damage onset



# Analysis of Notched Sandwich Specimens B-Spline Method (BSAM):

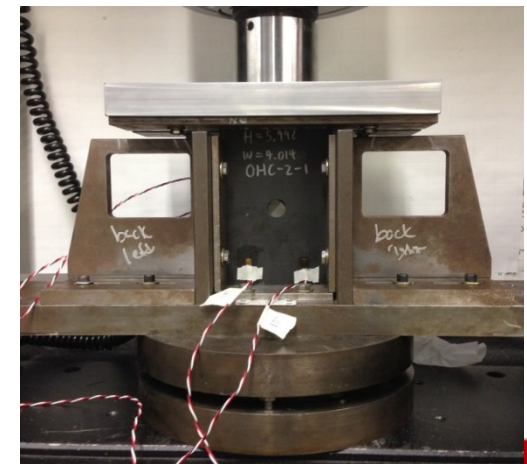
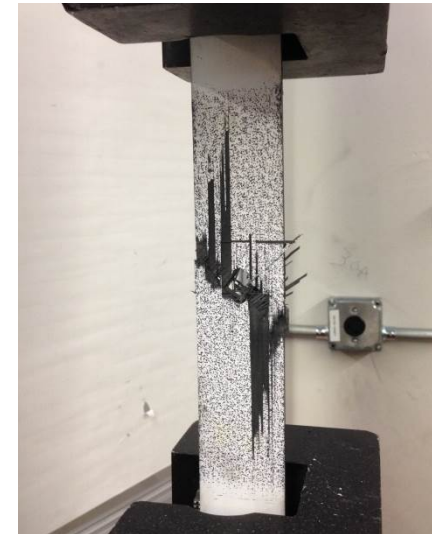
- Stand-alone software
- Developed by AFRL, UDRI, UTA
- Discrete damage modeled using Regularized Extended Finite Element Method (Rx-FEM)
  - Matrix Cracking
    - Multiple failure criteria for damage onset
    - Damage propagation using cohesive zone method
  - Delamination using cohesive zone method
  - Fiber failure using Critical Failure Volume or CDM



# Failure Analysis of Notched Sandwich Specimens

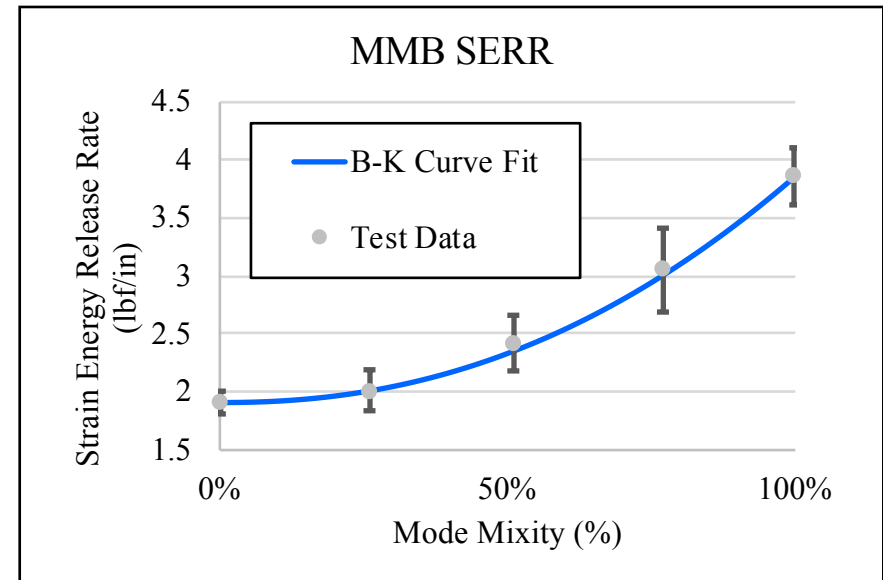
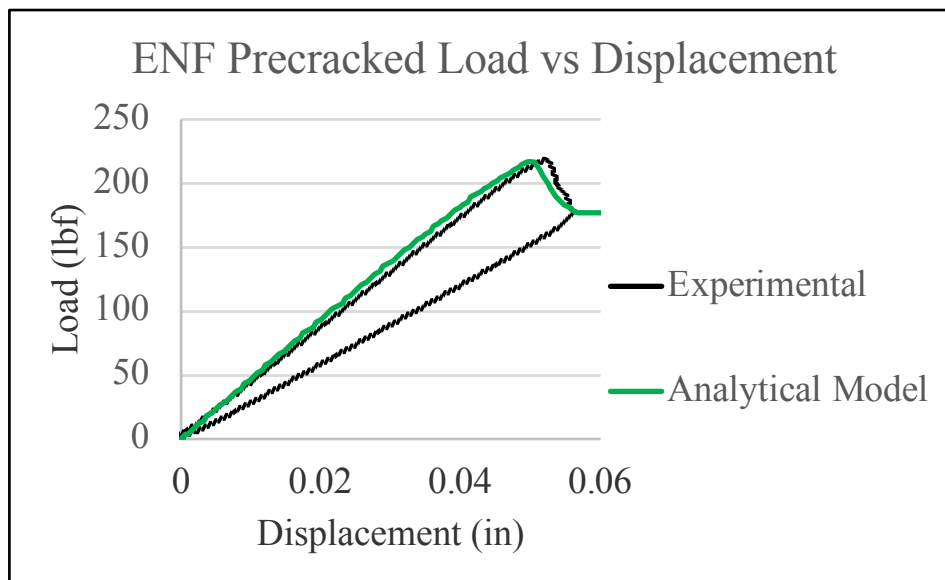
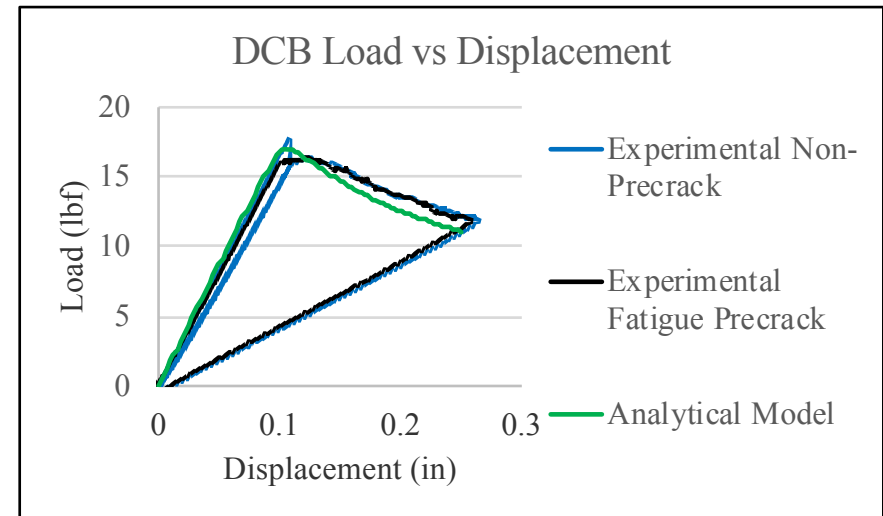
## Development of Modeling Approach

- **Modeling of damage progression in facesheets**
  - Interlaminar disbond (Mode I and II)
  - Laminate tension (+/-45 layup)
  - Open-hole tension
  - Open-hole compression
- **Modeling of damage progression in core**
  - Flatwise compression
  - Flatwise shear
- **Modeling of damage progression in sandwich composites**
  - Sandwich interface disbond (Mode I and II)
  - Sandwich open-hole shear
  - Sandwich open-hole flexure
  - Sandwich open-hole compression



# Damage Progression in Facesheets: Analysis of Delamination

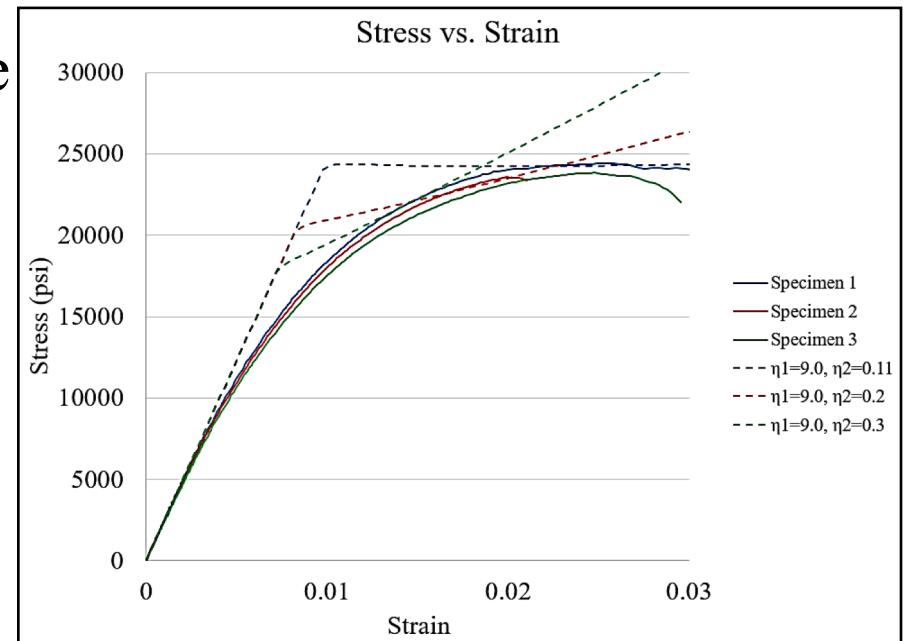
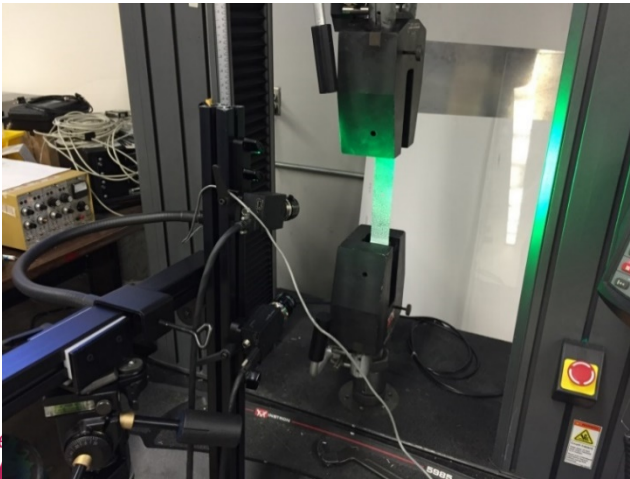
- **Calibration of cohesive zone**
  - Mode I DCB using ASTM D5528
  - Mode II ENF using ASTM D7905
  - MMB using ASTM D6671
- **Both modeling approaches use the same damage formulations**





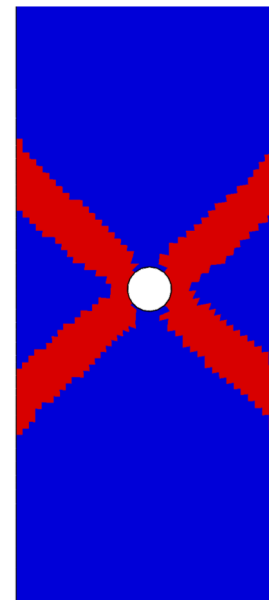
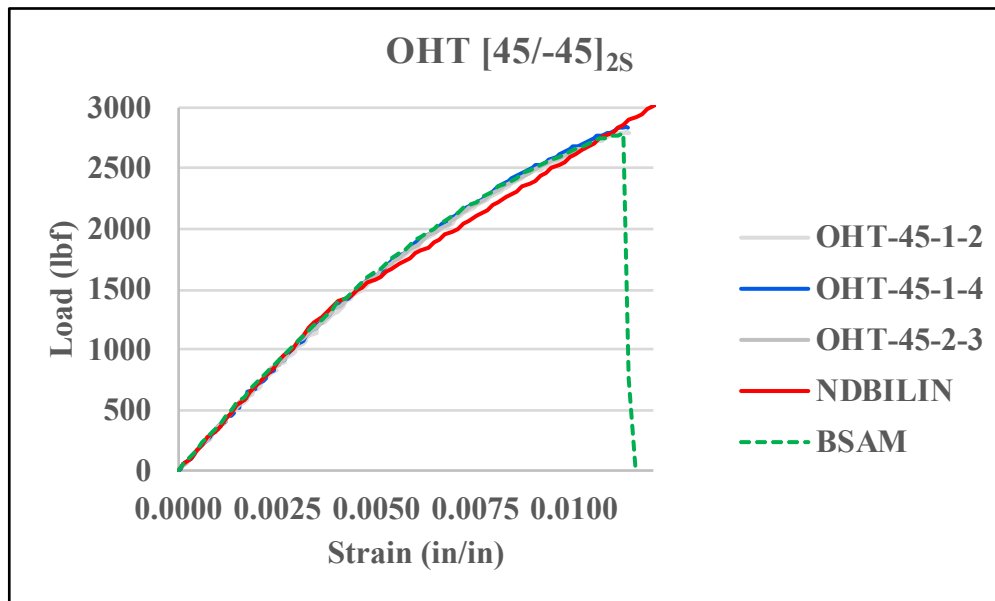
# Damage Progression in Facesheets: Analysis of +/-45 Laminates

- Simulation of un-notched and open-hole tension testing
- IM7/8552 carbon/epoxy,  $[45/-45]_{2S}$  laminates
- Matrix shear modulus, strength and damage parameters calibrated using measured stress-strain behavior
  - NDBILIN: bilinear response
  - BSAM: non-linear response

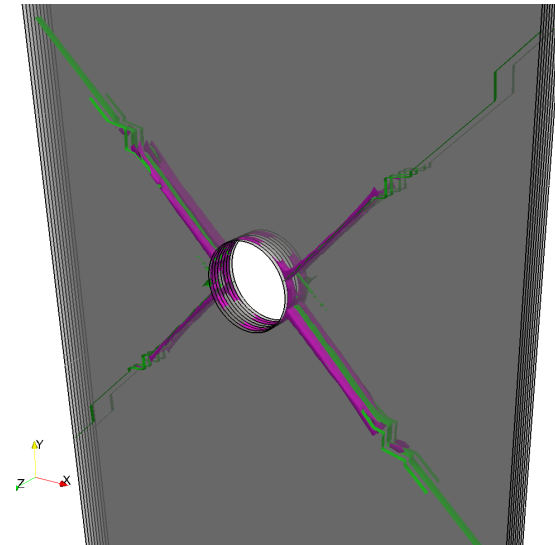


# Damage Progression in Facesheets: Laminate +/-45 layup Open-Hole Tension

- NDBILIN does not predict when failure occurs
- BSAM failure strain is sensitive to intralaminar shear strain energy release rate (GIIC)

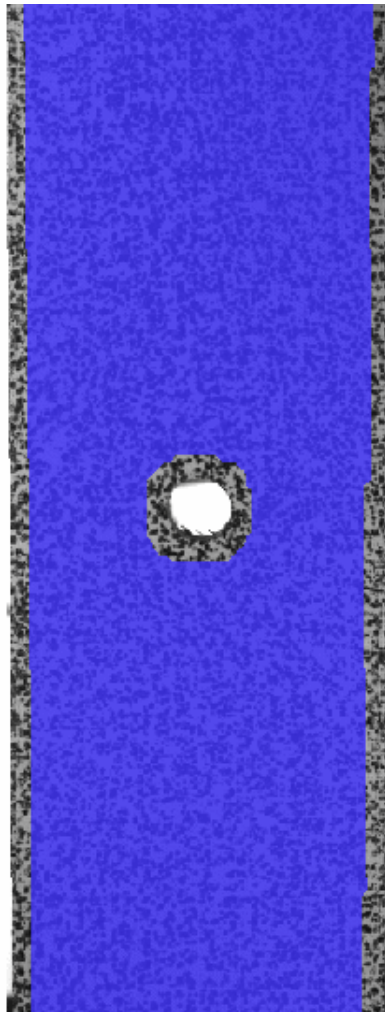


NDBILIN  
Red = Failed Elements

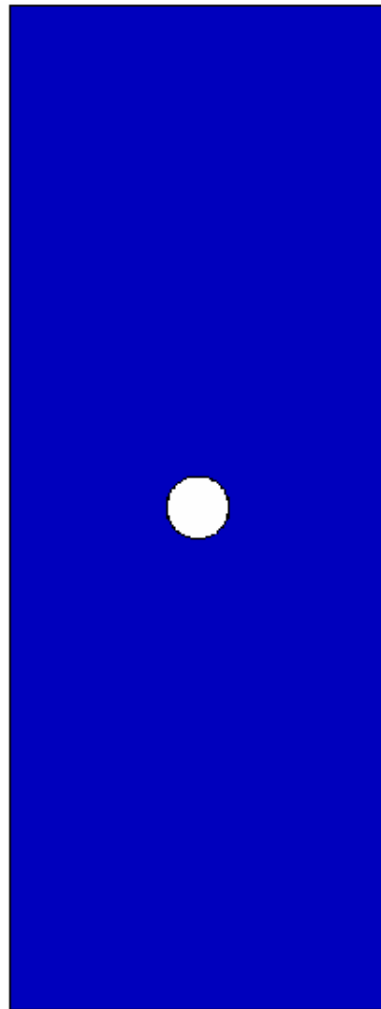


BSAM  
Green = Matrix Cracks  
Purple = Delamination

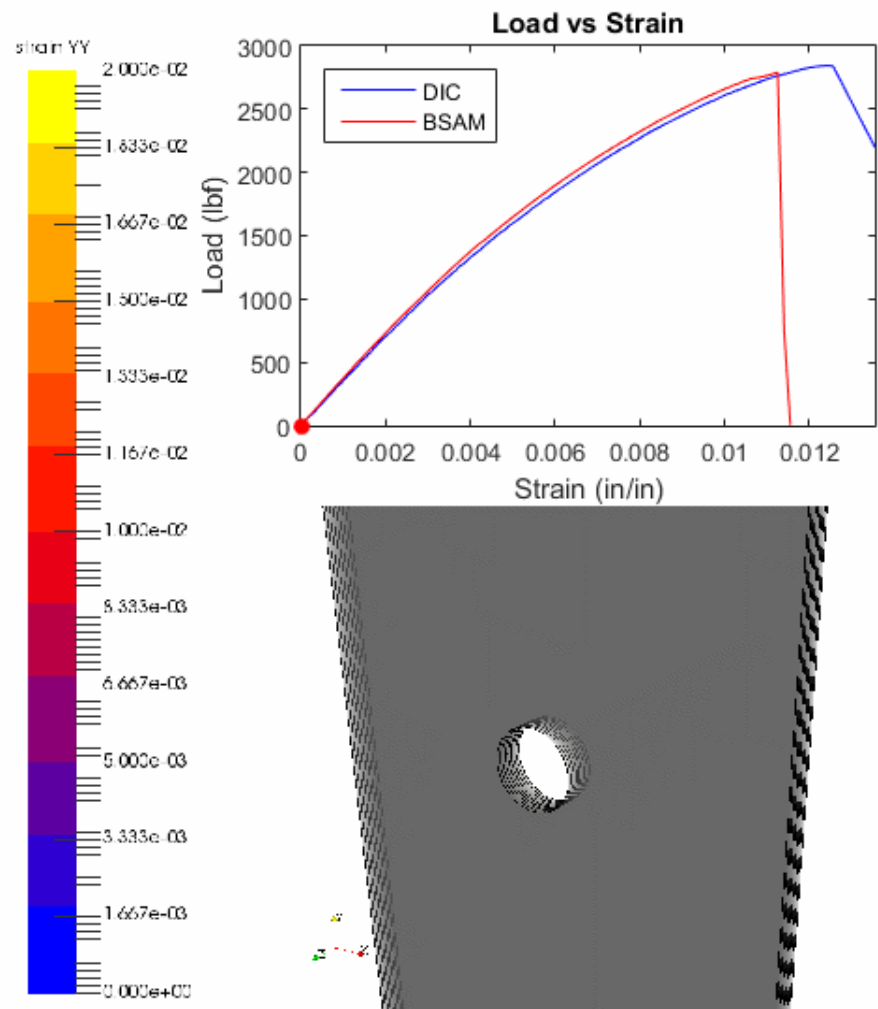
# Damage Progression in Facesheets: BSAM +/-45 Open-Hole Tension



DIC



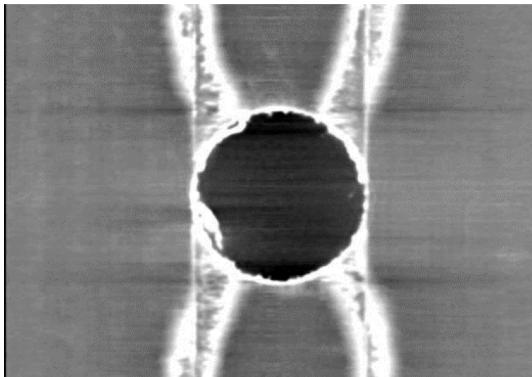
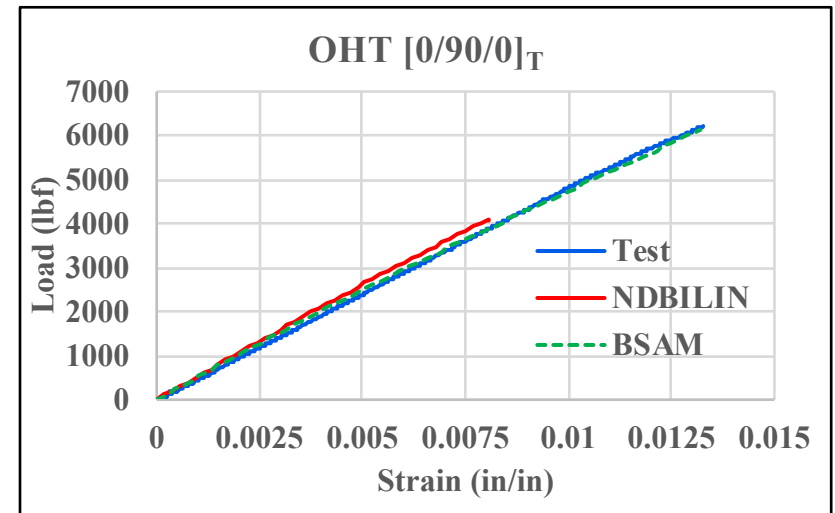
FEM



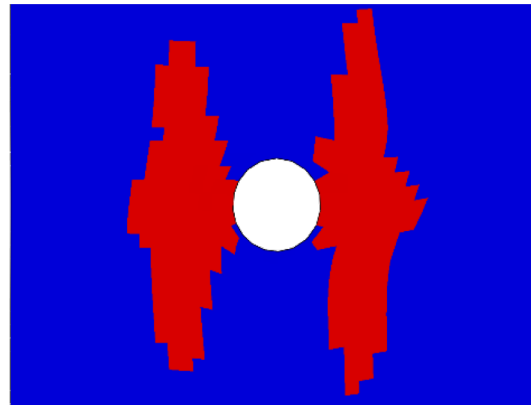
Damage Progression

# Damage Progression in Facesheets: Cross ply Open-Hole Tension

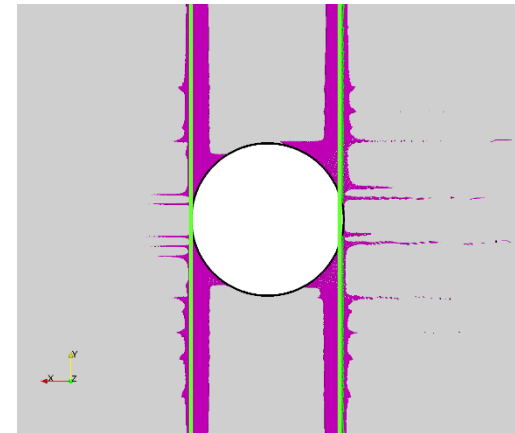
- Facesheet layup orientation
  - $[0/90/0]_T$
- NDBILIN predicts notch sensitivity
- BSAM predicts notch insensitive (<4% difference)
- BSAM requires fine mesh for a close to converged solution



X-Ray CT



NDBILIN

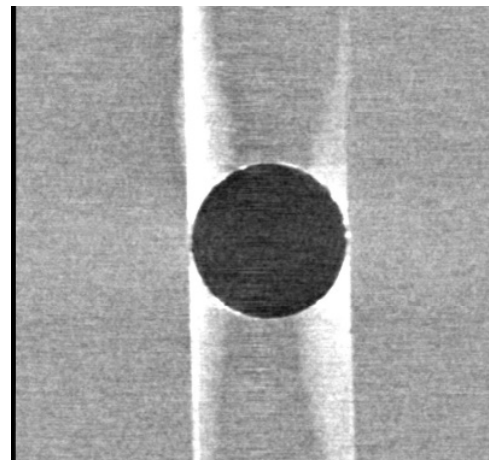


BSAM

# Damage Progression in Facesheets: Open-Hole Compression

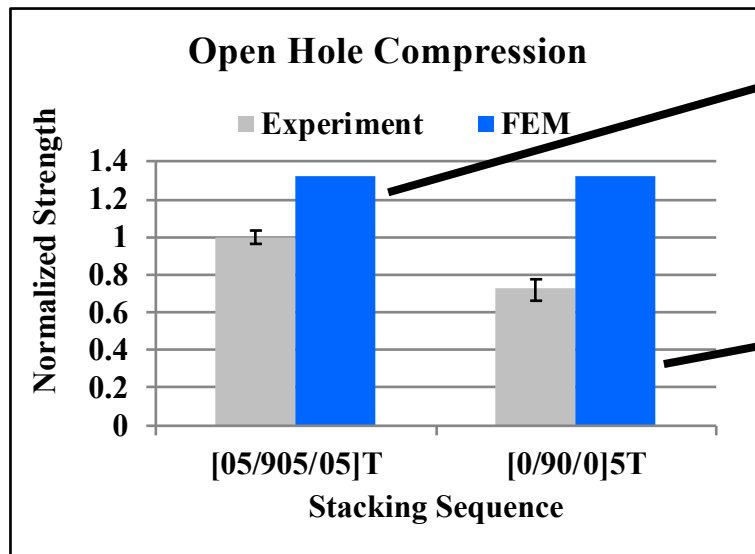
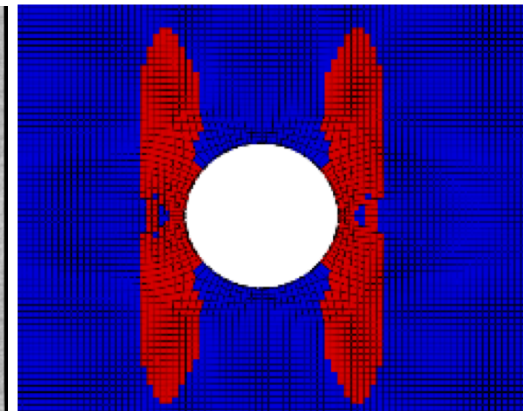
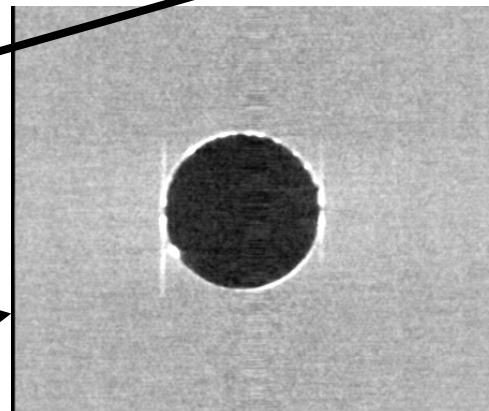
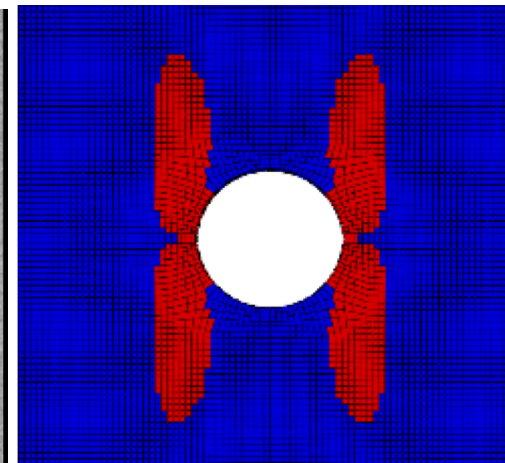
- Scaled facesheet layup orientation
  - $[0_5/90_5/0_5]_T$
  - $[0/90/0]_{5T}$
- NDBILIN predicts similar damage progression and failure loads

X-Ray CT



NDBILIN

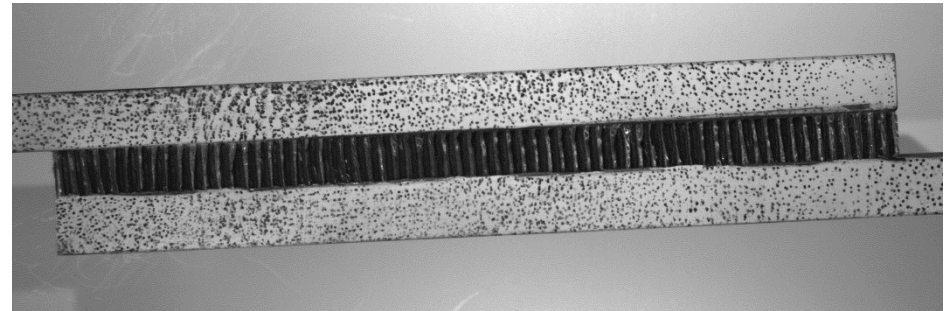
Red = Failed Elements





# Damage Progression in Core: Flatwise Compression/Shear

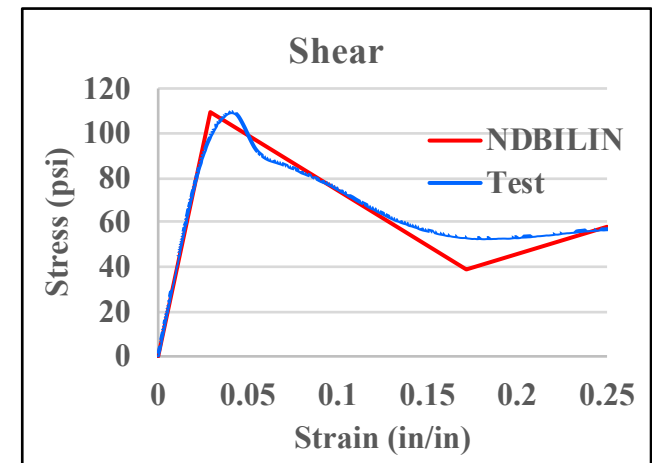
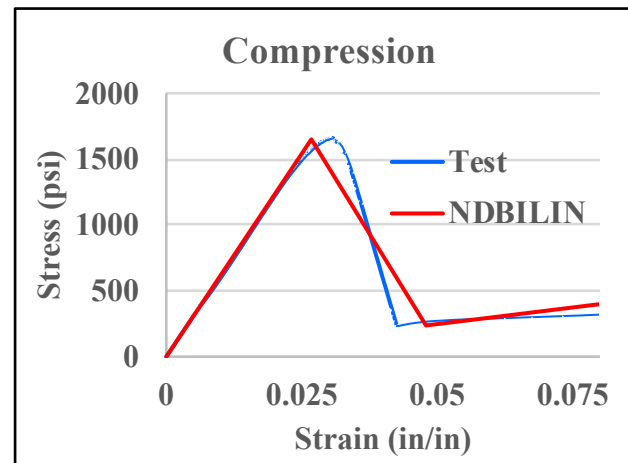
- Honeycomb core loaded until total core collapse in both compression and shear
- NDBILIN parameters fit to material curves



Flatwise Shear Test



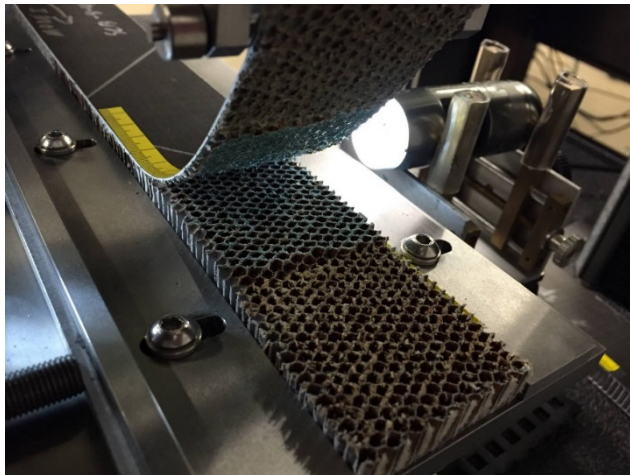
Compression Test



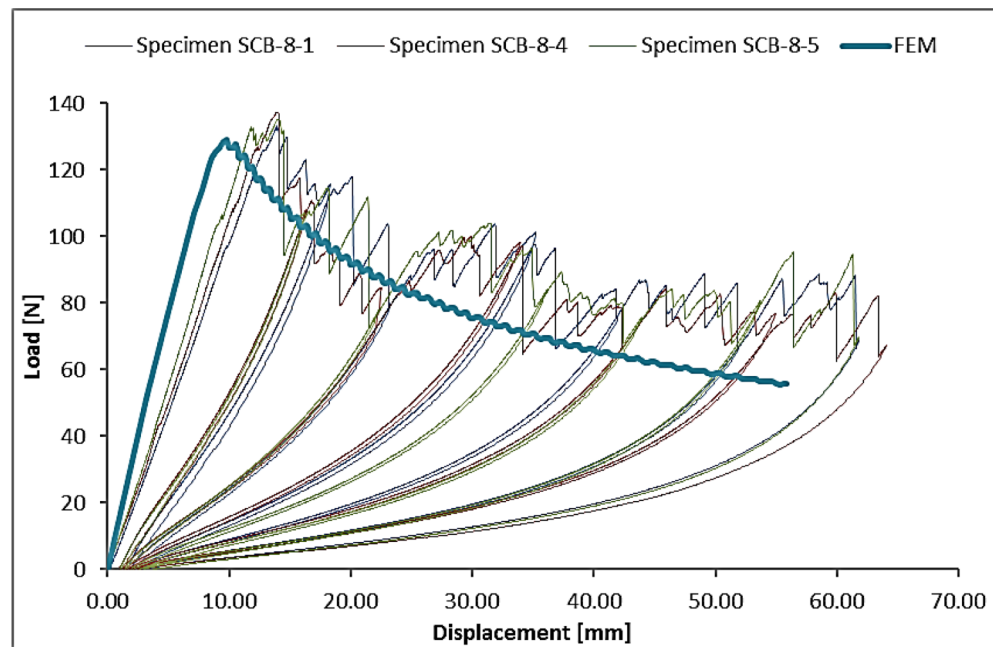


# Damage Progression in Sandwich Composites: Analysis of Interfacial Disbond

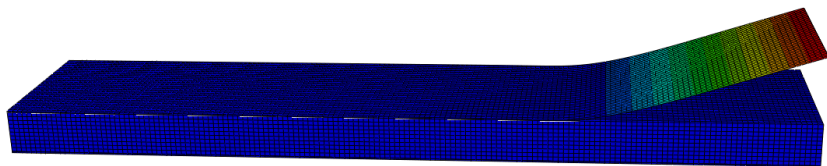
- Calibration of interfacial cohesive zone
  - Mode I Sandwich SCB



Single Cantilever Beam Test



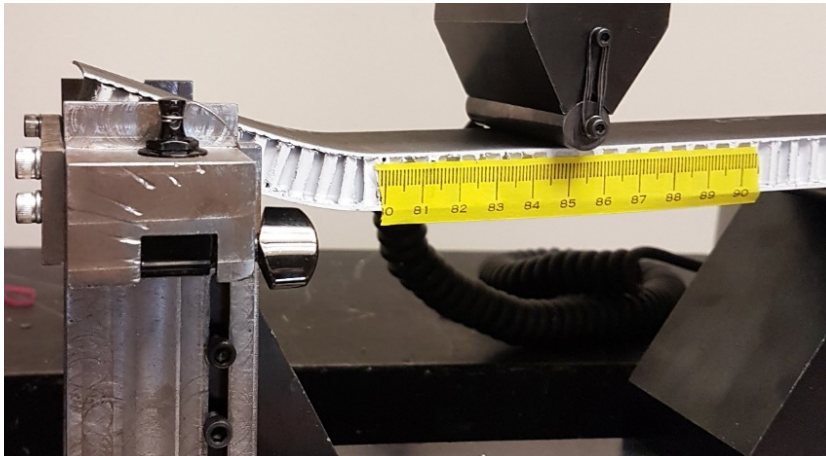
Load vs Displacement Data



Single Cantilever Model Displacements

# Damage Progression in Sandwich Composites: Mode II and Mixed-Mode

- **Calibration of interfacial cohesive elements**
  - **New failure mode: core cell walls buckle at crack tip, no crack growth**
  - **Analytical and numerical models do not account for constraint effect on honeycomb core**



**Mode II Sandwich ENF Test**

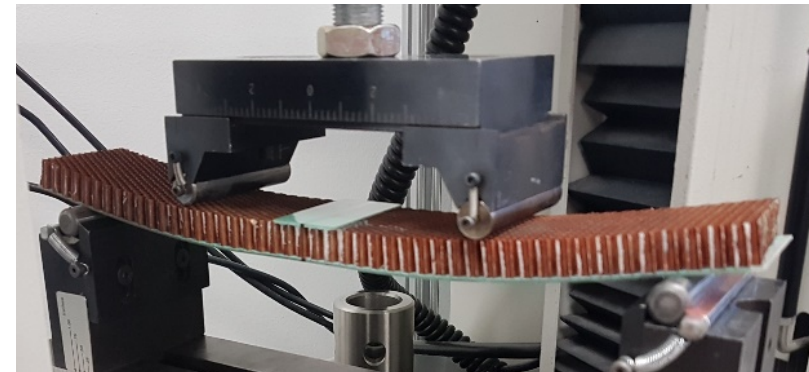
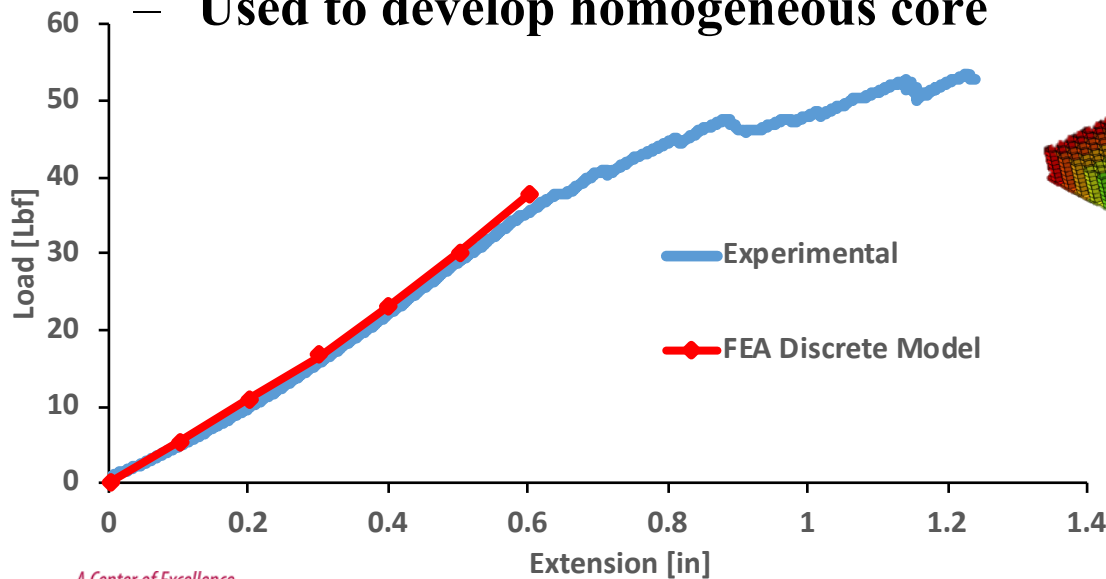


**Sandwich Mixed Mode Bend Test**

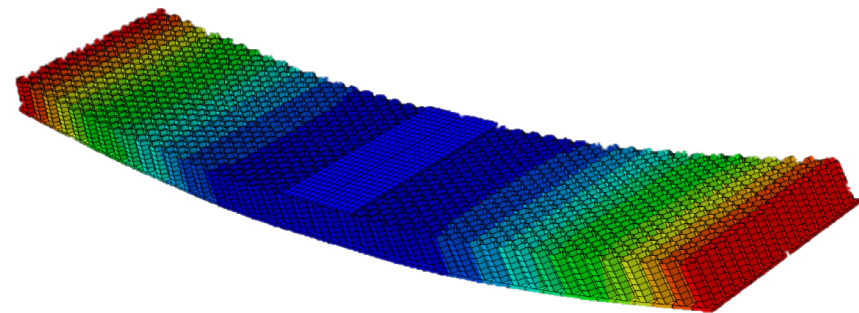
# Core Constraint Effect: Discrete Core Model in Flexure

- **Open-Face Flexure**

- Constraint effects at crack front
- Ribbon properties calibrated with flatwise compression and shear tests
- Captures elastic curve
- Used to develop homogeneous core



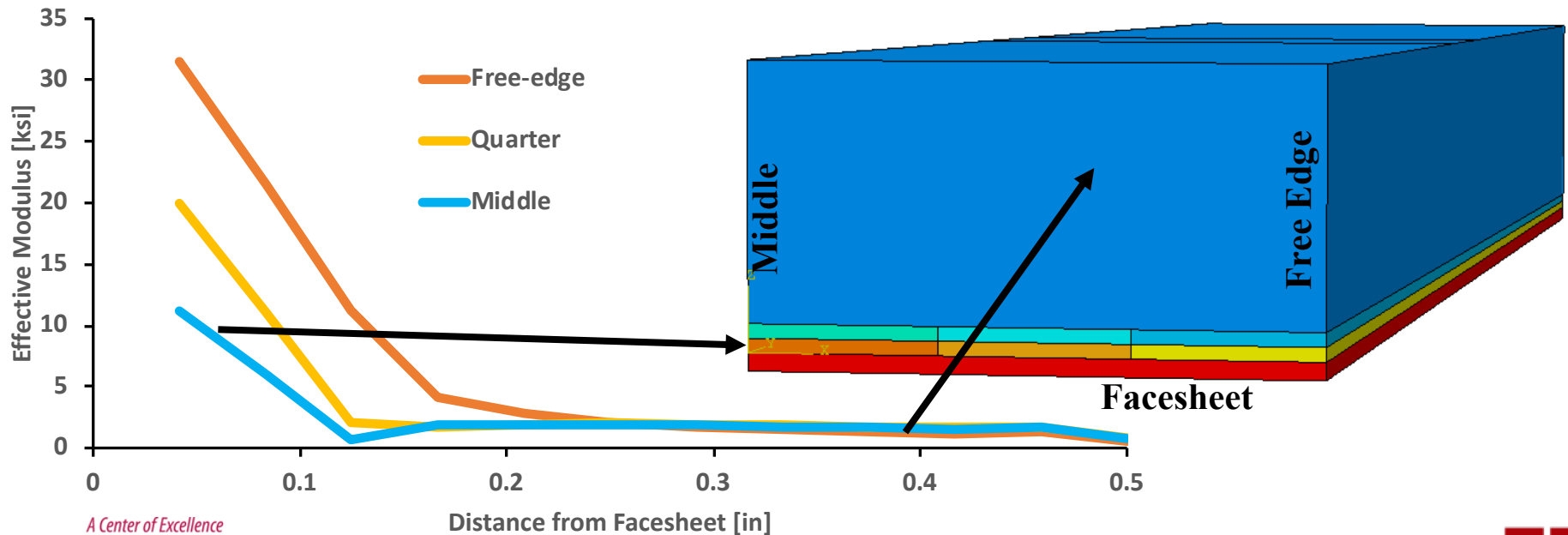
Test



FEM

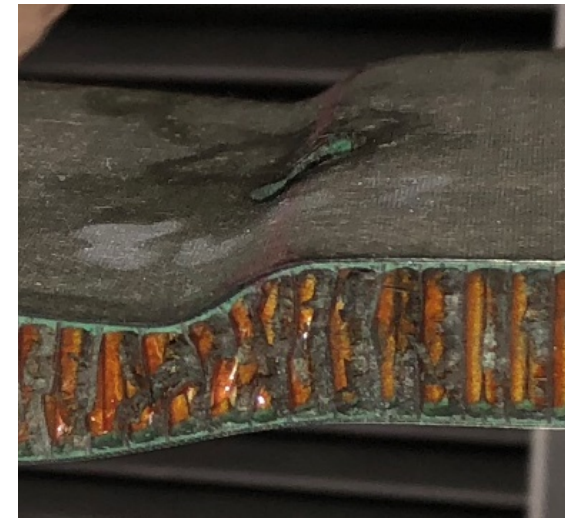
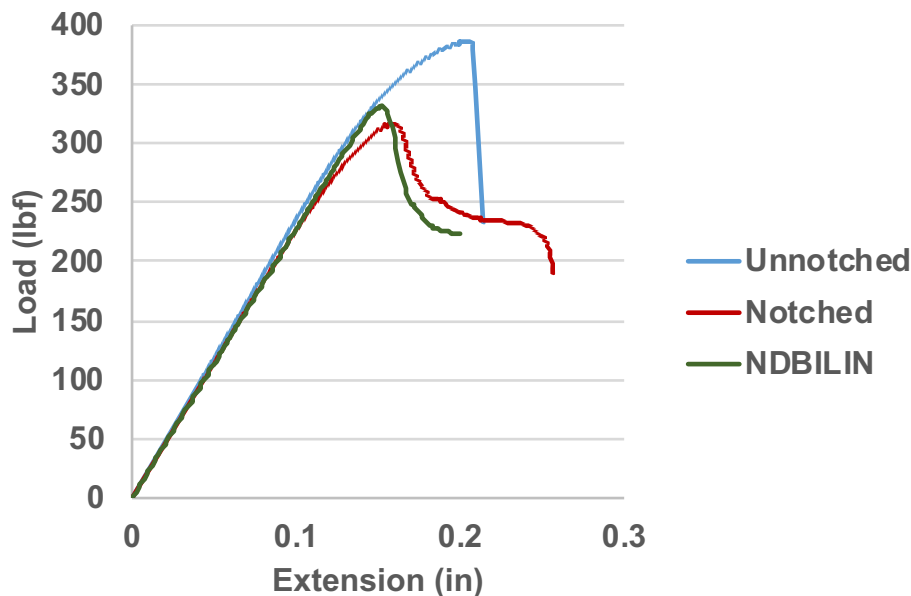
# Homogeneous Core: Current Focus

- **Discretized Homogeneous Core**
  - Thickness and free-edge effects
  - Discretize and apply unique material properties and failure parameters
  - Incorporate into sandwich disbond models

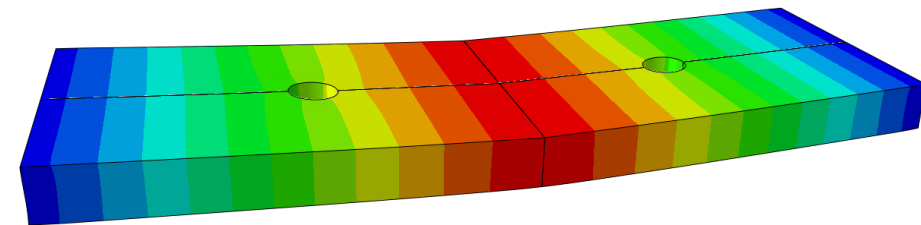


# Damage Progression in Sandwich Composites: Analysis of Sandwich Open-Hole Shear Tests

- Core modeled with NDBILIN
- Slight over prediction of max load
- Reload Captured



Sandwich Open-Hole Shear Failure

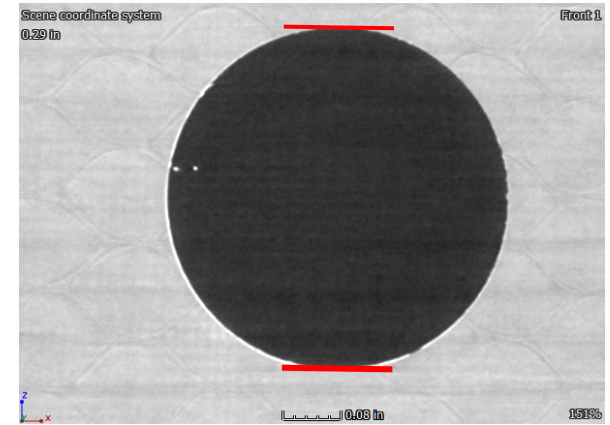


Model Displacements



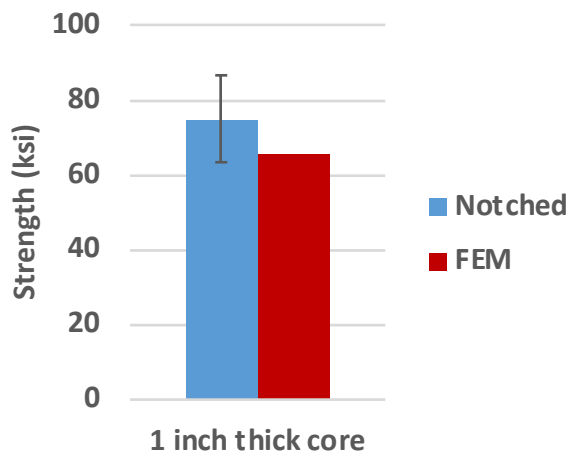
# Damage Progression in Sandwich Composites: Analysis of Sandwich Open-Hole Flexure Tests

- 90% load X-ray CT shows minimal damage progression
- Model over predicting damage and under predicting failure load

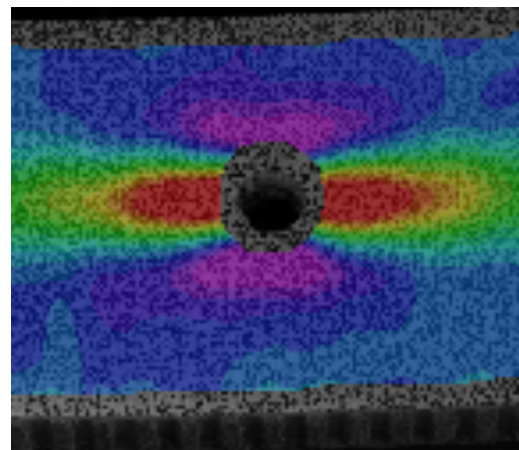


X-Ray CT

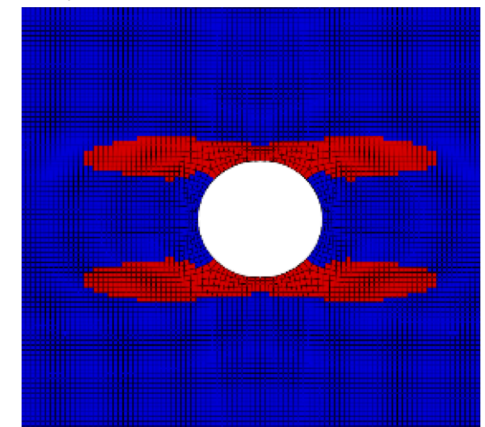
(Courtesy of Southwest Research Institute)



Compression Strength Comparison



DIC Strain

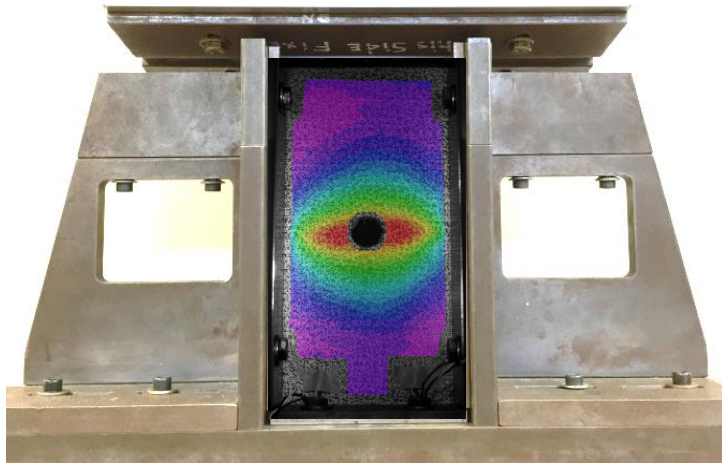


NDBILIN Damage Prediction

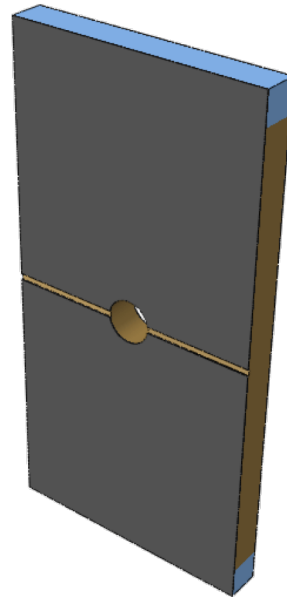


# Damage Progression in Sandwich Composites: Analysis of Sandwich Open-Hole Compression Tests

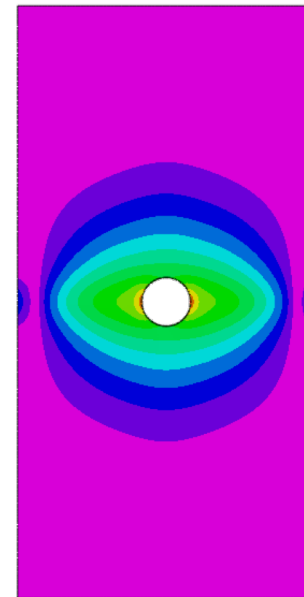
- Out-of-plane displacements observed in DIC measurements
- First mode facesheet buckling observed
- Global buckling due to failure on Non-DIC facesheet
- Deformation caused by post failure eccentric loading



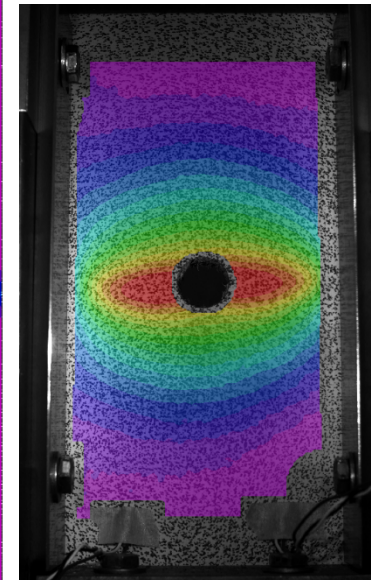
SOHC out-of-plane deformation



Idealized Failure



Out-of-plane deformations  
FEM



DIC  
THE UNIVERSITY OF UTAH

# Upcoming Work:

## Notch Sensitivity of Composite Sandwich Structures

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- **Develop sizing guidelines for proposed notch sensitivity testing methods**
- **Assess discrete damage models for remainder of calibration/validation building block approach**
- **Continue working toward homogeneous core for incorporation into Sandwich Mode II & MMB**
- **Incorporate initial damage from hole drill process on Sandwich Open-hole Compression**

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# Thank you for your attention!

## Questions?