

JOINT ADVANCED MATERIALS & STRUCTURES
CENTER OF EXCELLENCE

“Delamination/Disbond Arrest Features in Aircraft Composite Structures”

JAMS Technical Review

Luke Richard and Kuen Y. Lin

University of Washington

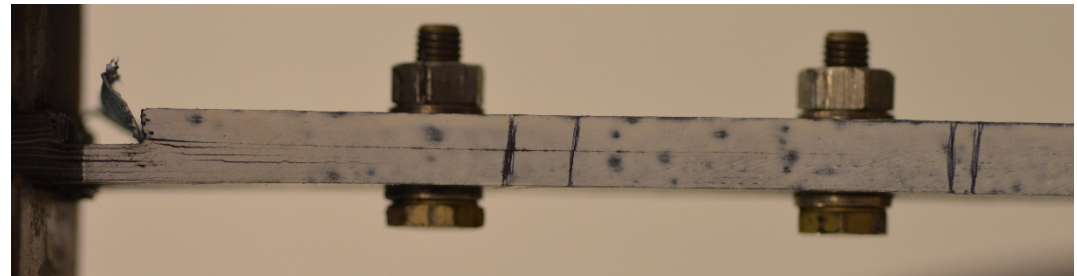
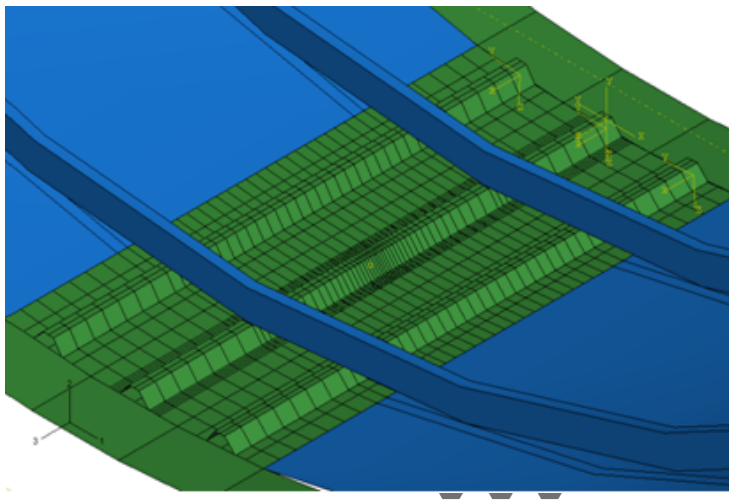
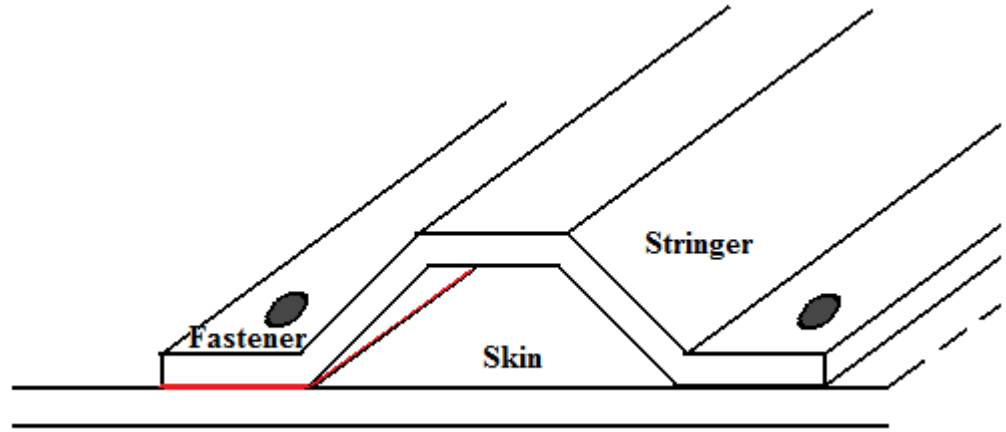
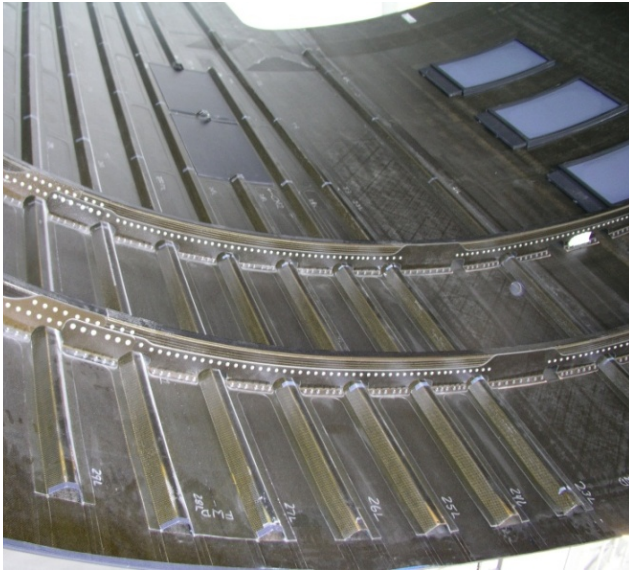
March 23, 2016



Sponsored Project Information

- **Principal Investigator:**
 - Dr. Kuen Y. Lin, Aeronautics and Astronautics, UW
- **Research Assistant:** Luke Richard, UW (lrich1@uw.edu)
- **FAA Technical Monitor:** Lynn Pham
- **Other FAA Personnel:** Curtis Davies, Larry Ilcewicz
- **Industry Participants:**
 - **Boeing:** Eric Sager, Matthew Dilligan, Lyle Deobald, Gerald Mabson, Eric Cregger, Marc Piehl, Bill Avery
 - **Toray:** Kenichi Yoshioka, Dongyeon Lee, Masahiro Hashimoto, Felix Nguyen
- **Industry Sponsors:** Toray and Boeing

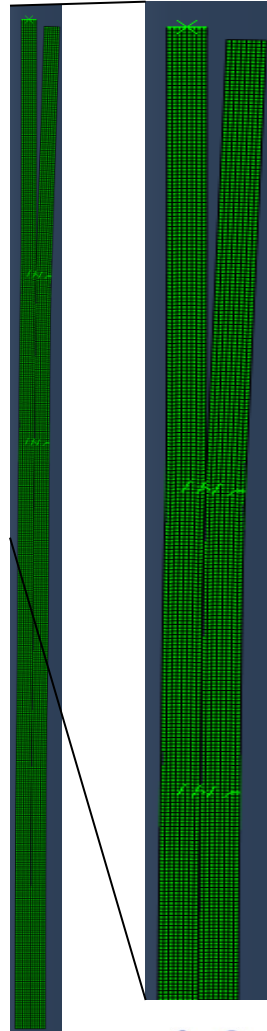
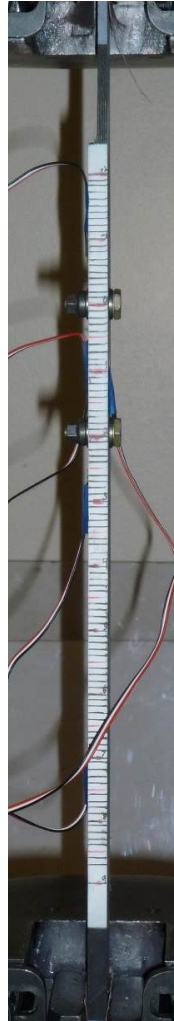
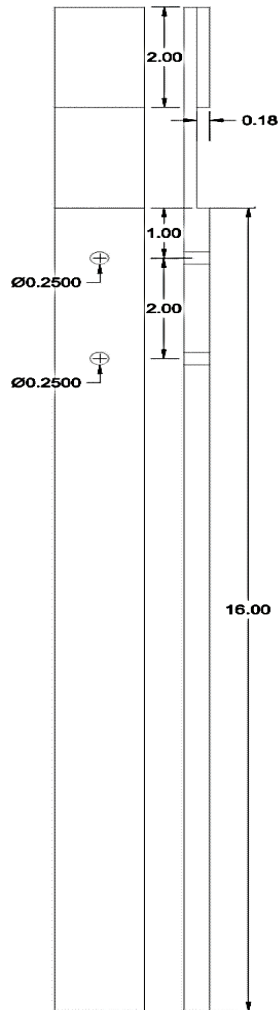
Crack Arrest Mechanism by Fastener



Research Objectives

- Accurately predict crack arrest capability for varying laminate and fastener configurations
 - Understand driving parameters of crack propagation and arrest by multiple fasteners under static and fatigue loading
 - Develop modeling techniques which can be employed for design, certification and optimization

Two Fastener Experimental Work



- T800S/3900-2B unidirectional pre-preg tape
- 0.25 inch fasteners (Titanium and Stainless)
- $(0/45/90/-45)_{3S}$ and 50% 0
- Load rate 0.1 mm/min (Static)
- 10 Hz or less (Fatigue)
- Crack tip tracked visually

2-Plate Two-Fastener Finite Element Model

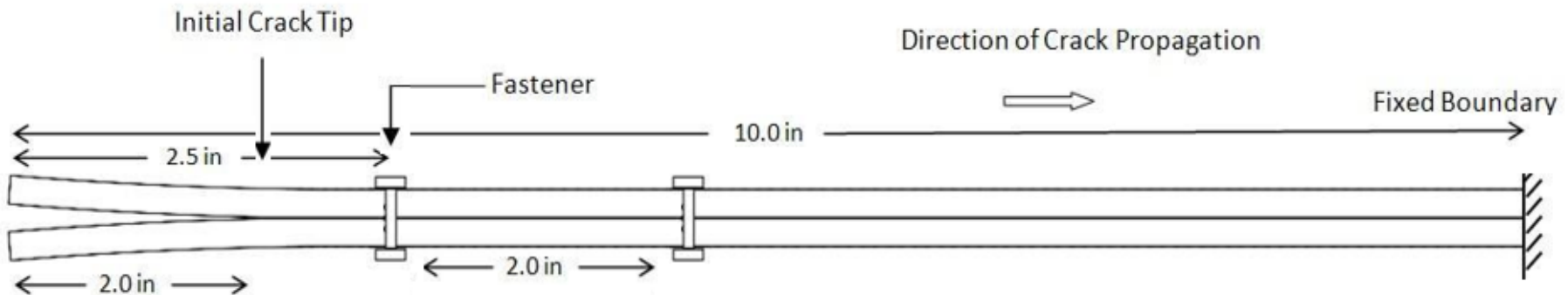
- Virtual Crack Closure Technique (VCCT) used for crack propagation
- Fracture parameters, $G_{IC}=1.6$ lb/in, Nominal $G_{IIC}=G_{IIIC}=14$ lb/in
Measured G_{IIC} : 12 lb/in (BMS 8-276)
- Fixed boundary conditions, test figure not modeled
- Two Dimensional
 - Plane strain representing crack growth along centerline
 - Lamina properties utilized in the model
- One Dimensional
 - Plates represented as beam/bar segments
 - Laminate properties derived from CLT
- Fatigue
 - Paris law utilized for crack growth vs. number of cycles
 - Damage beyond delamination not considered

2-Plate Two-Fastener Finite Element Model

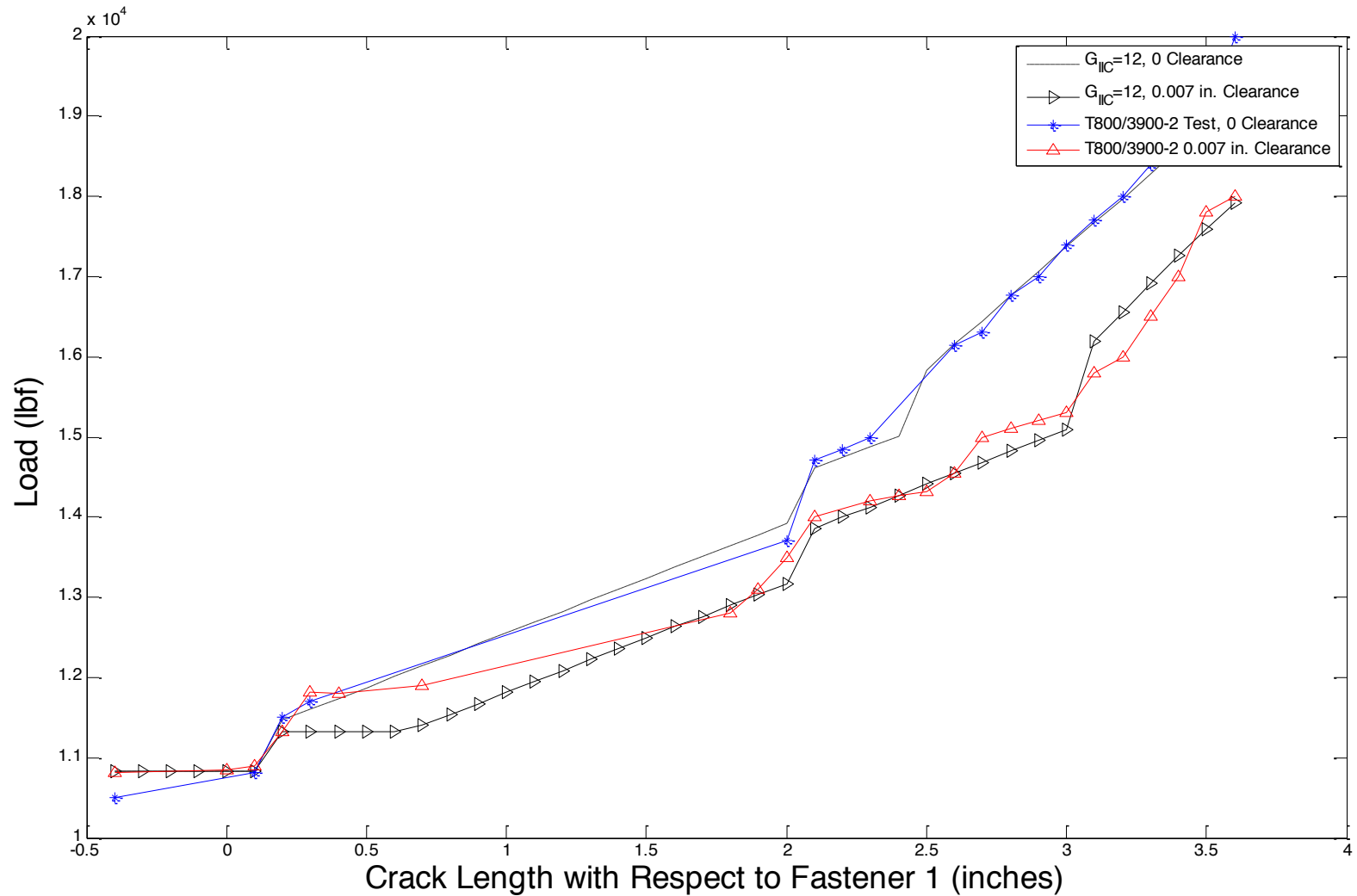
- Fastener flexibility (H. Huth, 1986) $C = \left(\frac{t_1+t_2}{2d}\right)^a \frac{b}{n} \left(\frac{1}{t_1 E_1} + \frac{1}{nt_2 E_2} + \frac{1}{2t_1 E_3} + \frac{1}{2nt_2 E_3}\right)$
 - Thickness $t_1=t_2=0.18$ in., diameter $d=0.25$ in., E_x = laminate stiffness
 - Single Lap, bolted graphite/epoxy joint, constants taken as; $a=2/3$, $b=4.2$, $n=1$
- Fastener joint stiffness $k_{slide} = \frac{1}{C}$, Fastener tensile stiffness $k_{clamp} = \frac{AE}{(t_1+t_2)}$

$$\left(\frac{G_I}{G_{IC}}\right)^\alpha + \left(\frac{G_{II}}{G_{IIC}}\right)^\beta + \left(\frac{G_{III}}{G_{IIIC}}\right)^\delta \leq 1$$

- Power Law fracture criterion
- Fixed boundary condition similar to test; grips not modeled
- Friction coefficient assumed to be fixed value or zero

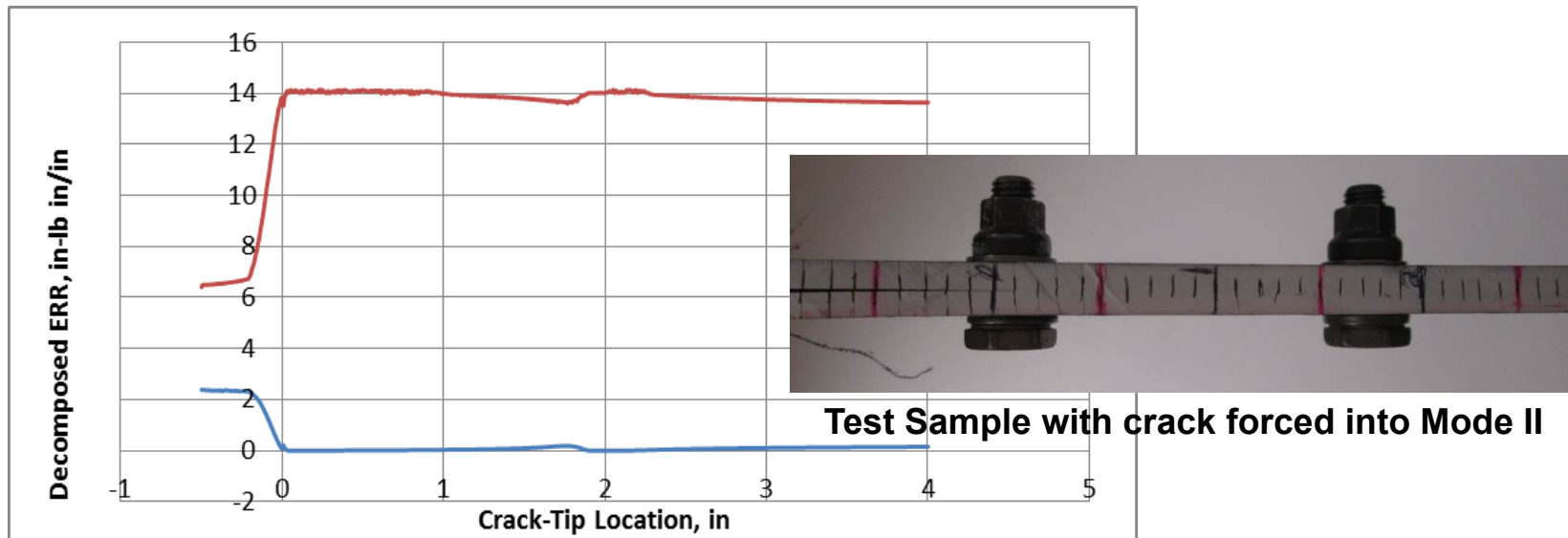


Static Test Results



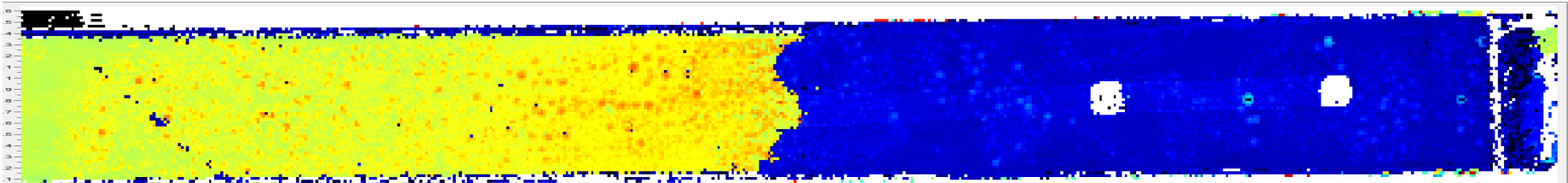
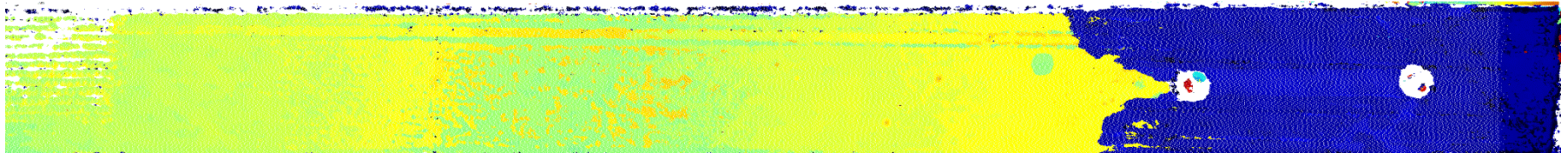
Mode I Suppression

- First fastener effectively suppresses Mode I
 - Mode I suppression regardless of clearance value
 - Propagation load increases as $G_{IIC} > G_{IC}$
 - Fastener size excessive for Mode I suppression
 - 6-32 fasteners ($D=0.1380$) found to suppress mode I



Friction and Crack Curvature

- O/O interface has minimum tested coefficient of static friction: 0.25
- Load transfer through friction is small compared to through fastener for static loading
 - 1000 lb preload results in 250 lb load transfer
 - Load transfer is non-negligible in fatigue loading
- Crack Curvature is extensive near fasteners but minimal outside the influenced zone



Fatigue Modeling

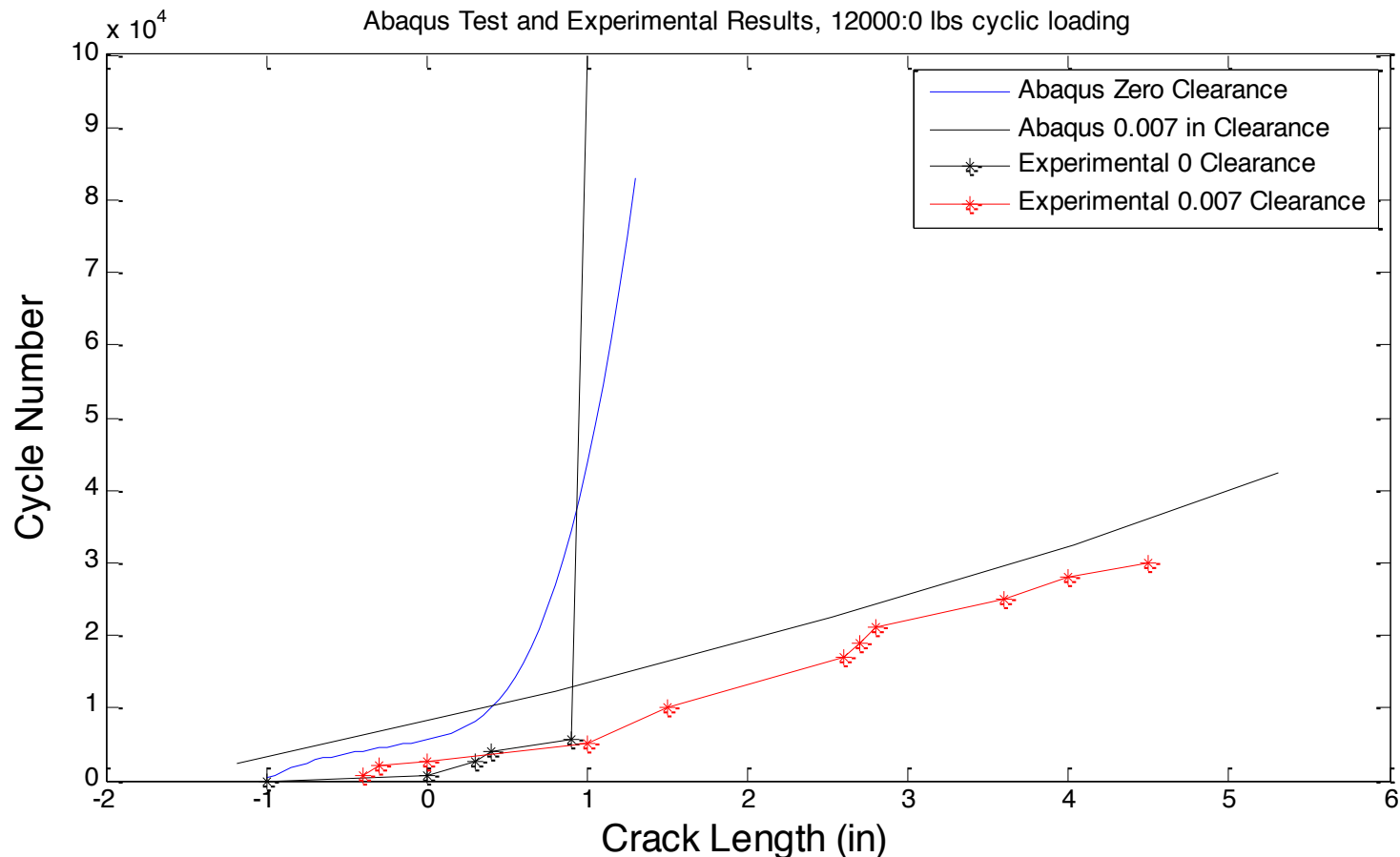
- Identical two and one dimensional models
 - Constant and Variable amplitude loading simulated
 - Paris Law and Miner's rule assumed to apply
 - Zero and positive clearance simulated
- Dramatic fatigue life difference due to clearance
 - Even 0.001 inch clearance shows dramatic simulated fatigue life difference
 - Consistent result both in tension-tension and tension-compression loading

Fatigue Testing

- Below fatigue threshold, fastener has no effect
- Fastener hole treatment has significant effect on low cycle fatigue
 - Crack arrest capability greatly reduced by the inclusion of clearance
- Loss of fastener clamping has arisen
 - Bending of specimen fatigues fastener head
- Hole damage may not be a critical factor
 - Visible on tested samples where crack growth did not occur

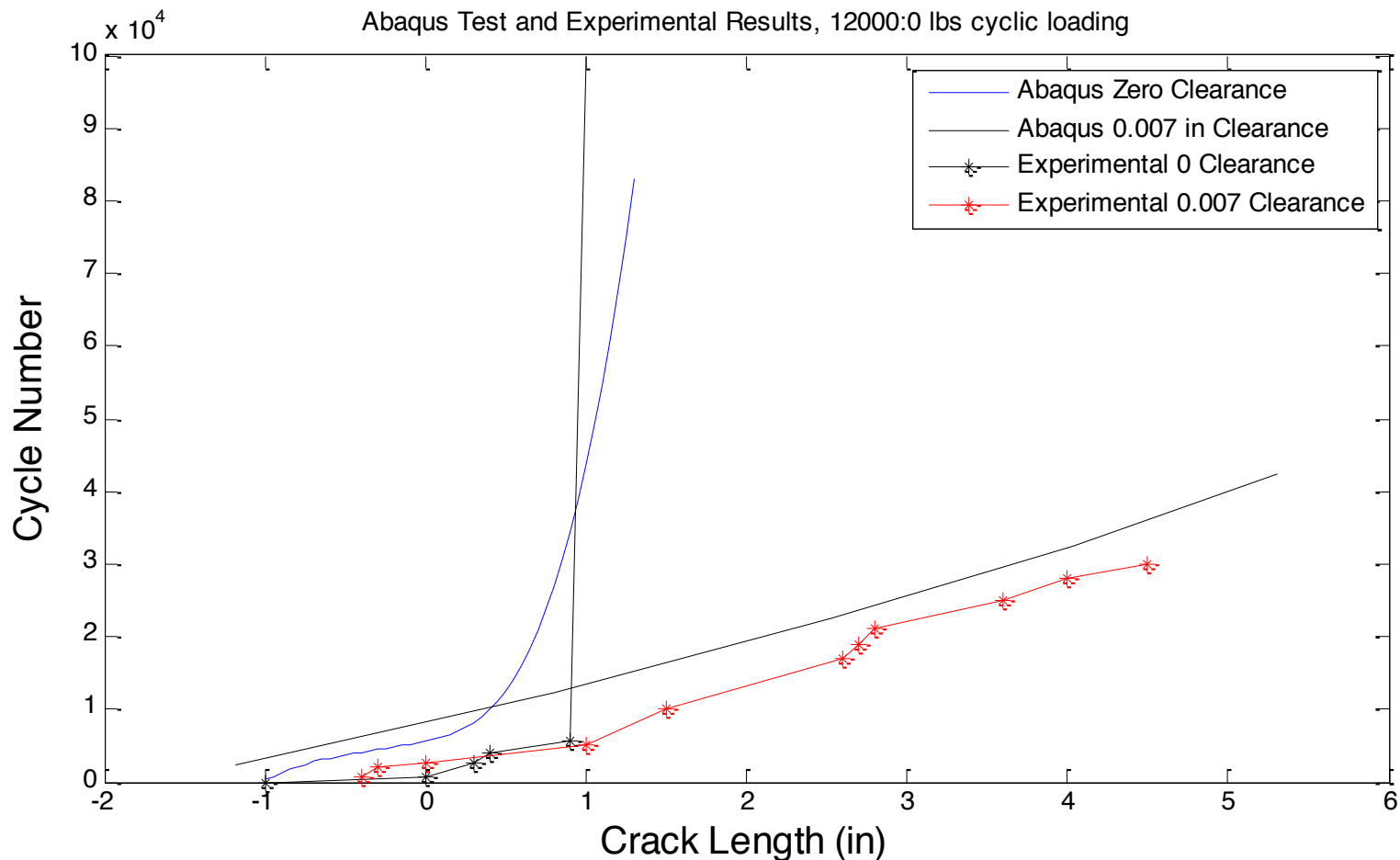
Fatigue Results (High Loading)

- Loads equal to or greater than static crack initiation load (9000 lbs)
- Distinct knee in zero-clearance hole
 - Fastener provides sufficient load alleviation so as to eliminate further crack propagation (below threshold)



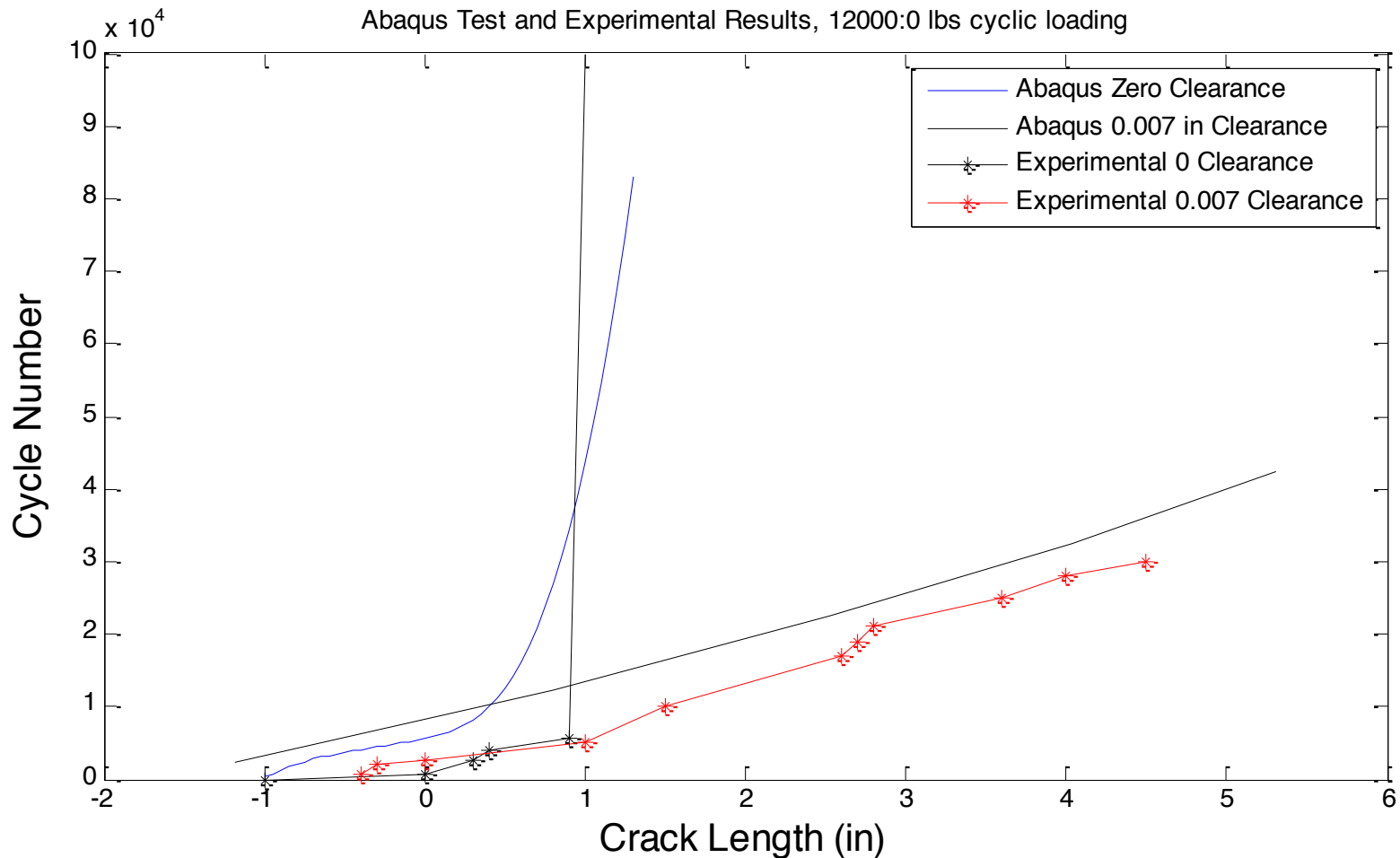
Fatigue Results (High Loading)

- Run-out (10^{17} cycles) did not occur
- Clearance drilled hole did not experience arrest, crack propagation is only slowed



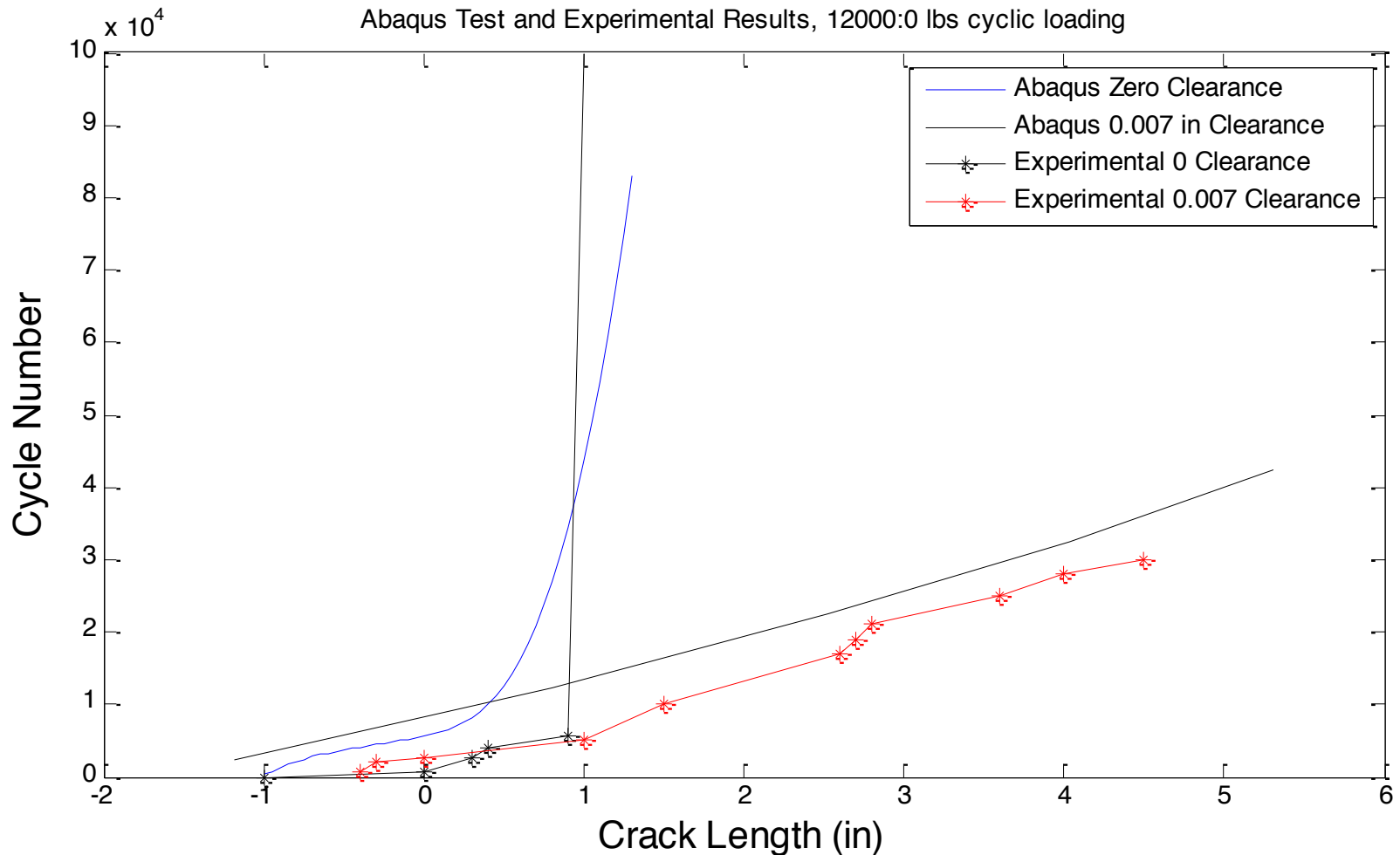
Fatigue Results (High Loading)

- Fatigue model and test results agree better when identical (quasi-isotropic) layup used for fatigue properties



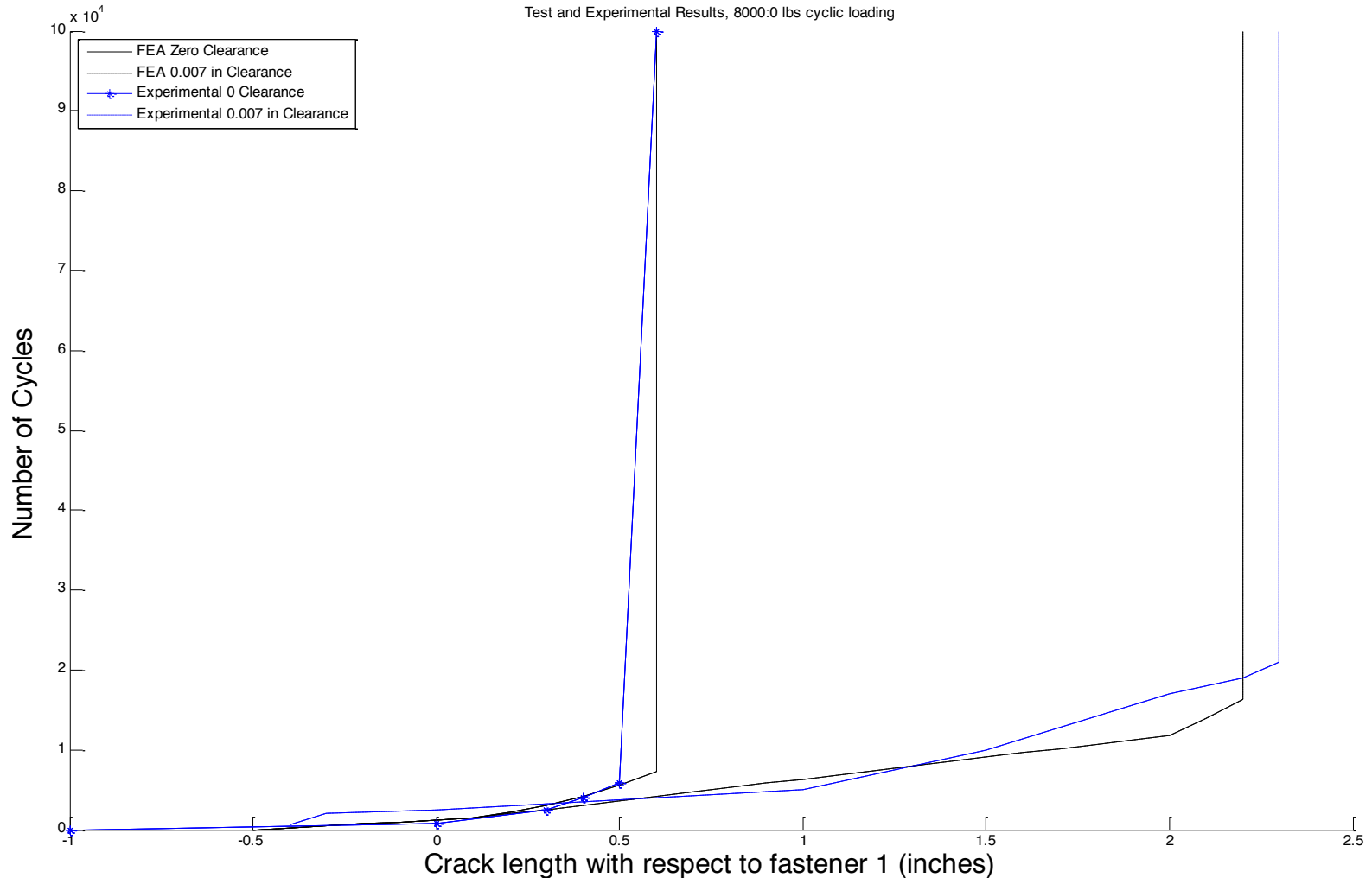
Fatigue Results (High Loading)

- 1D modeling provided better agreement
 - Fastener modeling becomes increasingly important



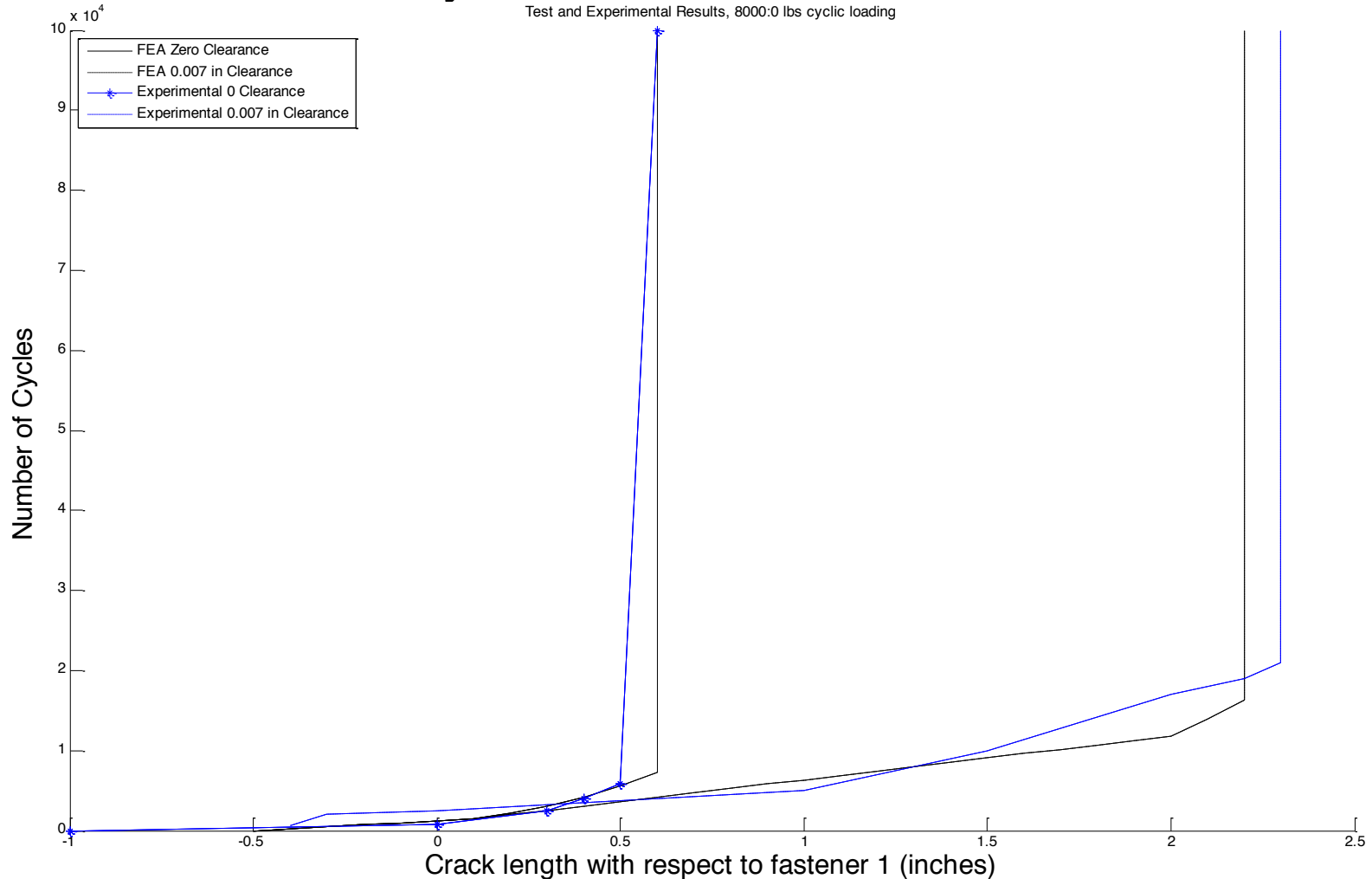
Fatigue Results (Low Loading)

- Loads equal to or less than crack initiation loading (9000 lbs)



Fatigue Results (Low Loading)

- Fastener friction clearly important
- Fastener Flexibility Critical



Future Work

- Friction Modeling
 - Lower load testing indicates critical influence of fastener friction
 - Loosening of second fastener (removing load transfer through preload) permits crack to continue to grow
- Countersinking of Fasteners
- Determine Critical Load Conditions
 - Establish scenarios where fastener is least effective
 - Determine conditions where hole damage affects propagation
- Documentation of a Final Report

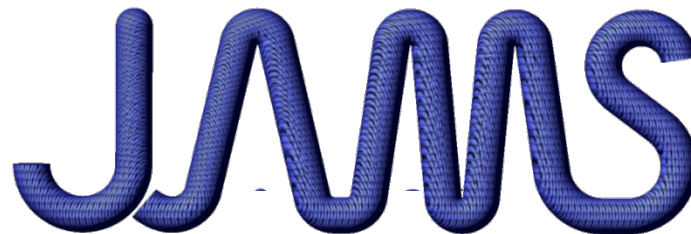


Looking Forward

- Benefit to Aviation
 - Tackle a crucial weakness of laminate composite structures
 - Improve analysis to prevent changes in schedule/cost due to a re-design associated with the delamination/disbond mode of failure in large integrated structures
 - Enhance structural safety by building a methodology for designing fail-safe co-cured/bonded structures
- Future needs
 - Further fatigue testing to better establish parameters
 - Initiate investigation of crack propagation through fastener arrays
 - Industry/regulatory agency inputs related to the application, design, and certification of this type of crack arrest feature

Question and comments?

Thank you.



JOINT ADVANCED MATERIALS & STRUCTURES
CENTER OF EXCELLENCE

