

DEVELOPMENT AND EVALUATION OF FRACTURE MECHANICS TEST METHODS FOR SANDWICH COMPOSITES

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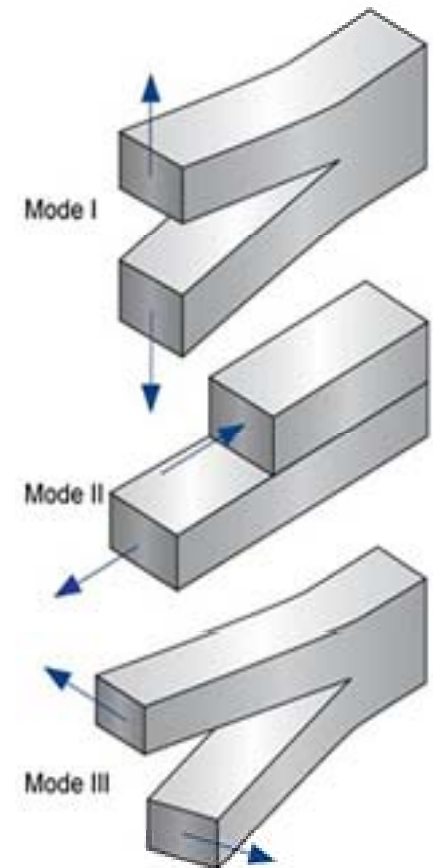
FAA Sponsored Project Information

- **Principal Investigator: Dr. Dan Adams**
- **Graduate Student Researchers:**
 Ryan Braegger Zach Bluth
- **FAA Technical Monitor**
 – Curt Davies David Westlund
- **Collaborators:**
 NASA Langley NIAR
 Boeing Learjet
 Airbus UTC Aerospace Systems

RESEARCH OBJECTIVES:

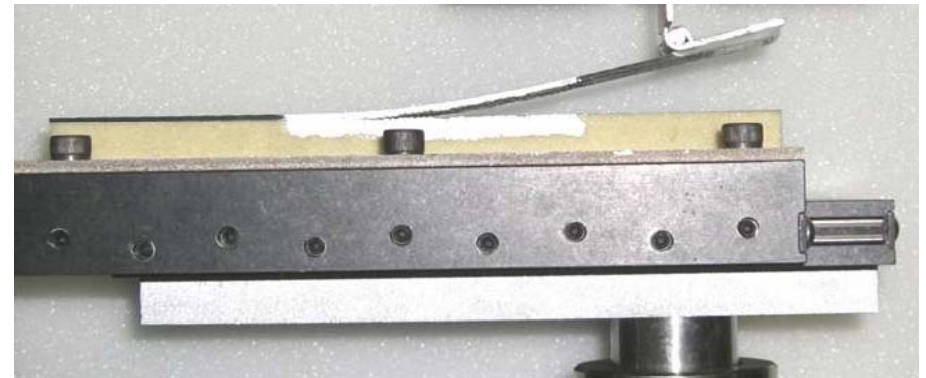
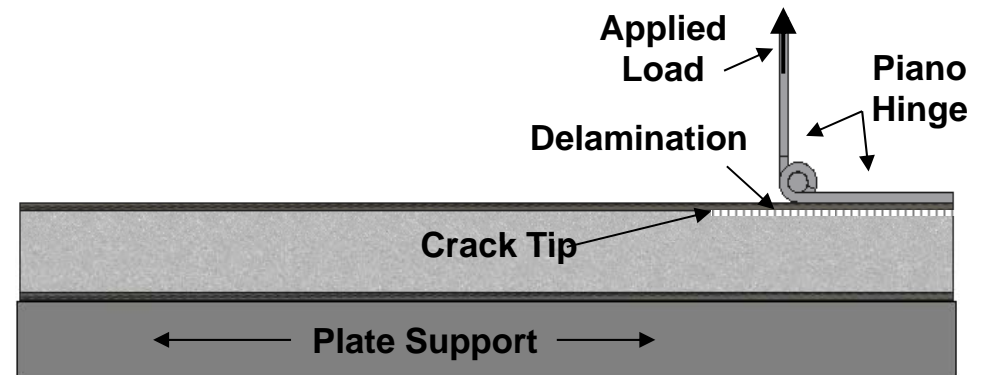
Fracture Mechanics Test Methods for Sandwich Composites

- Focus on facesheet-core debonding
- Mode I and Mode II
 - Identification and initial assessment of candidate test methodologies
 - Selection and optimization of best suited Mode I and Mode II test methods
 - Development of draft ASTM standards



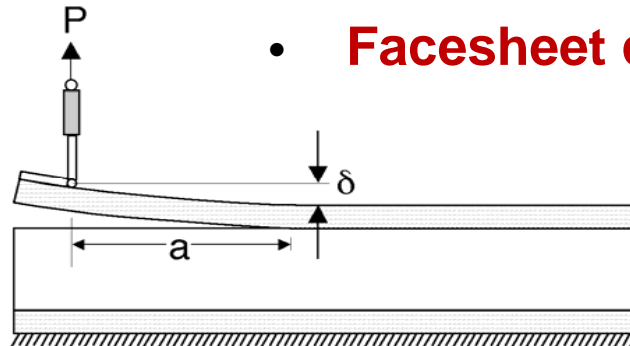
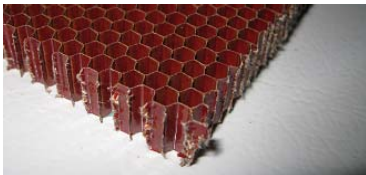
MODE I TEST CONFIGURATION: Single Cantilever Beam (SCB)

- Elimination of bending of sandwich specimen
- Minimal crack “kinking” observed
- Mode I dominant - independent of crack length
- *Appears to be suitable for standardization*



PARAMETERS INVESTIGATED: Single Cantilever Beam (SCB) Test

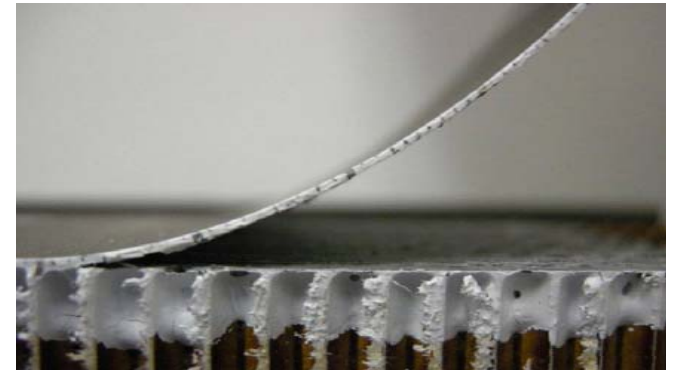
- Specimen geometry
 - Length
 - Width
 - Initial crack length
- Facesheet properties
 - Thickness
 - Flexural stiffness
 - Flexural strength
- Core properties
 - Thickness
 - Density
 - Stiffness
 - Strength
- Mode mixity
 - Variations across specimen width
 - Variations with crack length
- Data reduction methods
- Thru-thickness crack placement
- Anticlastic curvature & curved crack front
- Large rotations of facesheet
- Use of facesheet doublers
- Facesheet curvature effects



SCB TEST METHOD DEVELOPMENT: Sandwich Configurations with Thin Facesheets

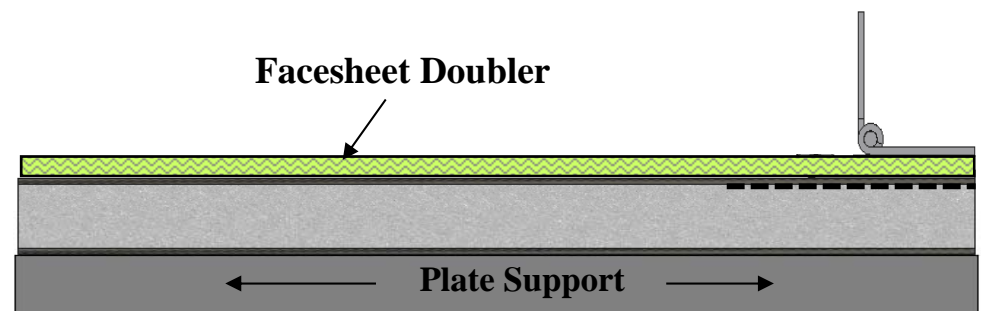
Concern: Excessive facesheet rotation

- Not representative of disbond in actual sandwich structures
- Geometric nonlinearity causes errors when using conventional data reduction method



Possible Solution: Use of facesheet doublers

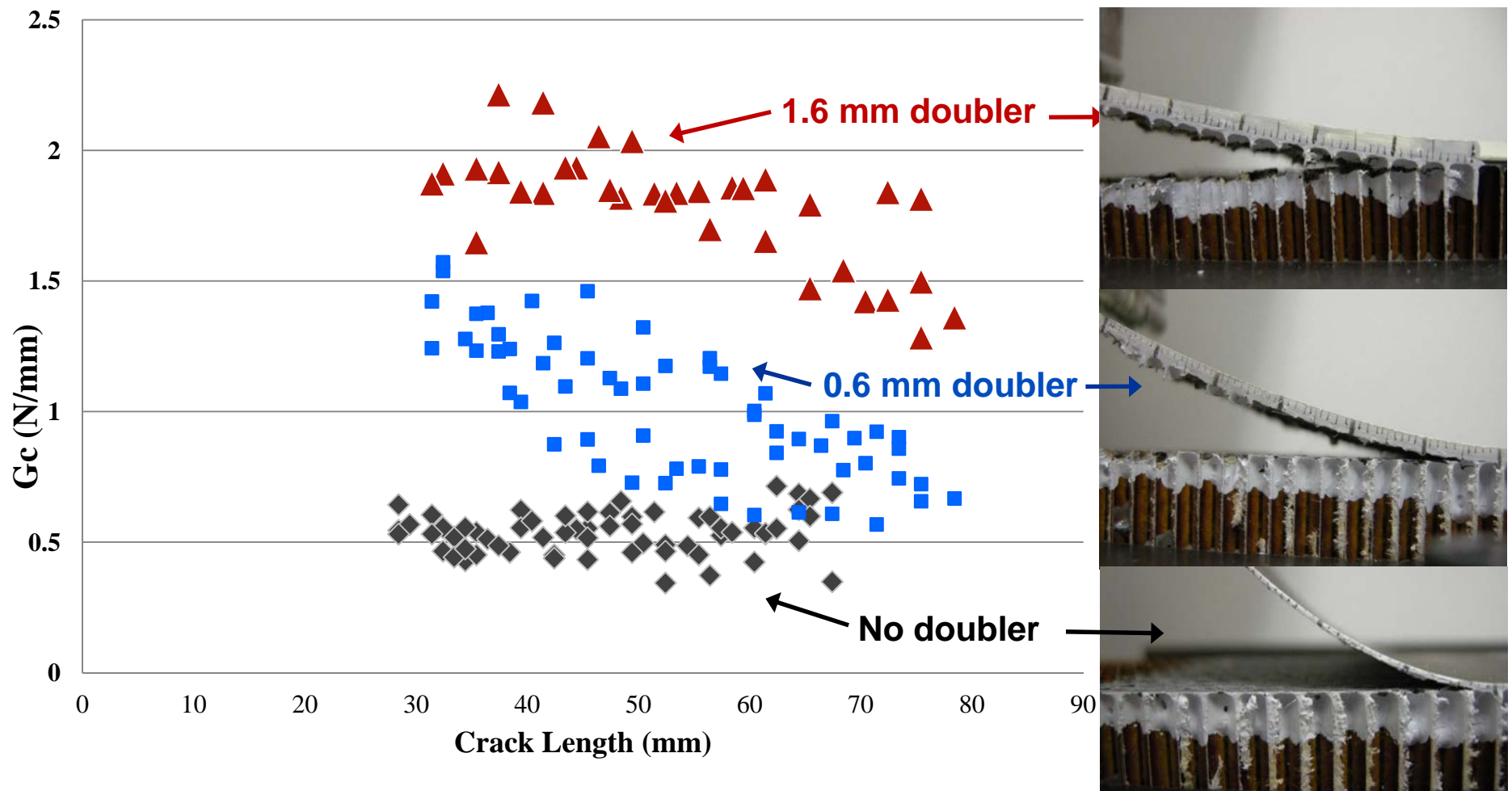
- Reduce facesheet rotation required for disbonding
- Allow use of compliance calibration method of data reduction



EFFECTS OF FACESHEET DOUBLER:

Different Doubler Thicknesses Produce Different G_c Values...

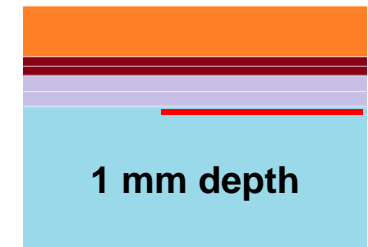
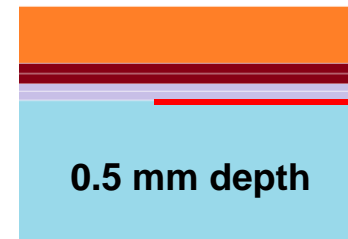
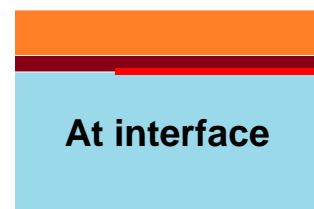
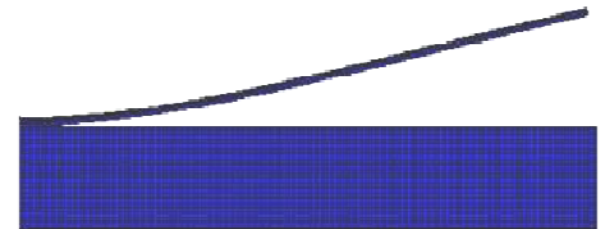
...and different thru-thickness fracture locations!



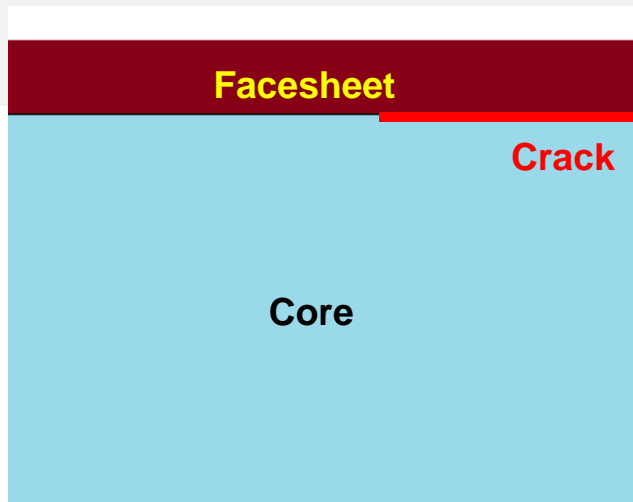
NUMERICAL INVESTIGATION

Effects of Thin Facesheets & Facesheet Doublers

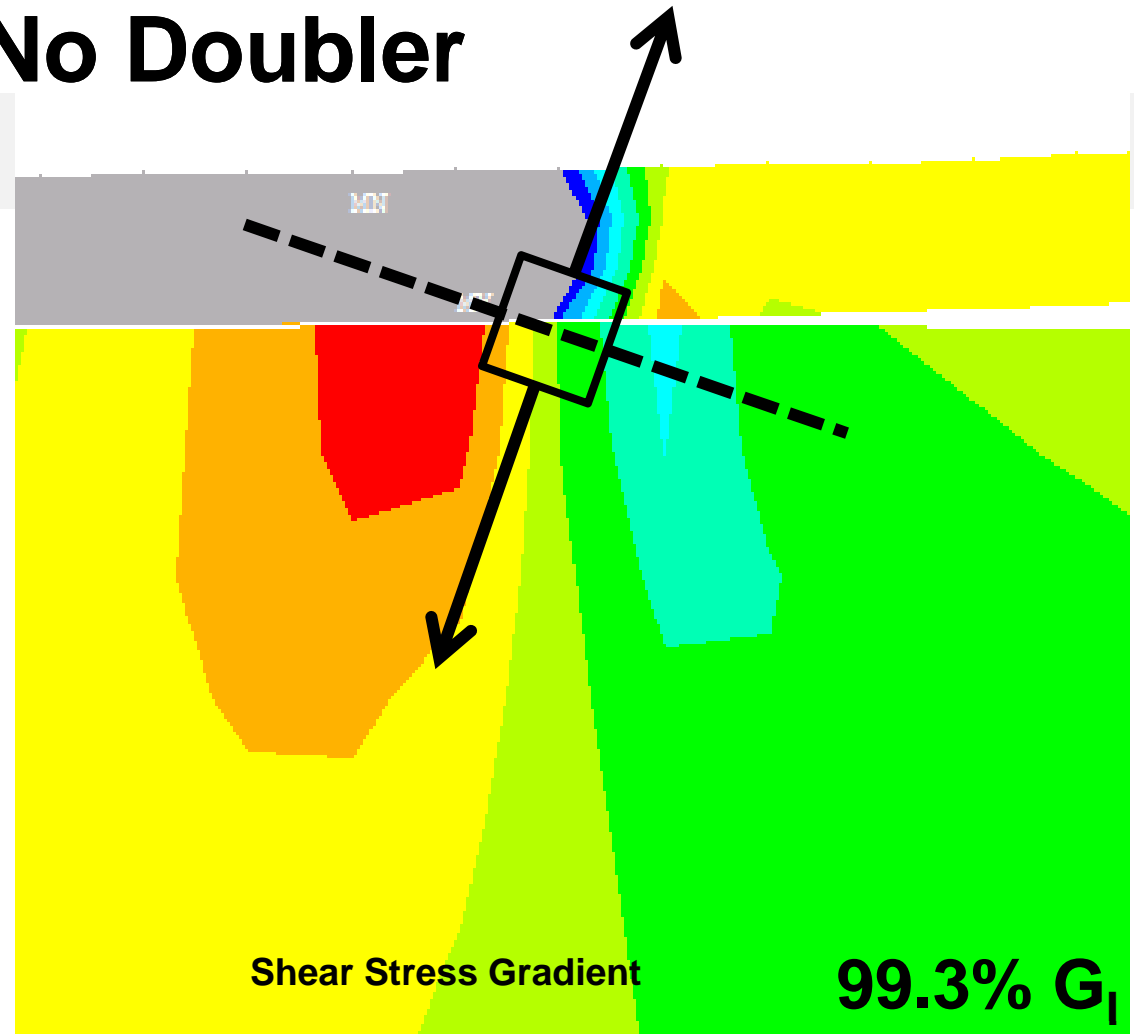
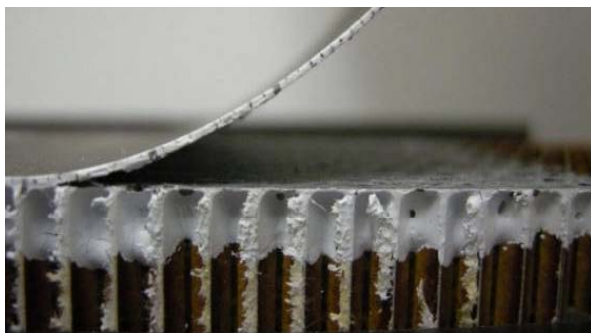
- Load applied in each model to produce same G_T value
 - No doubler, “thin” doubler, “thick” doubler
- Consider crack growth at three through-the-thickness locations
- Investigate mode mixity (% G_I)
- Investigate orientation of max. principal stress for expected crack growth direction



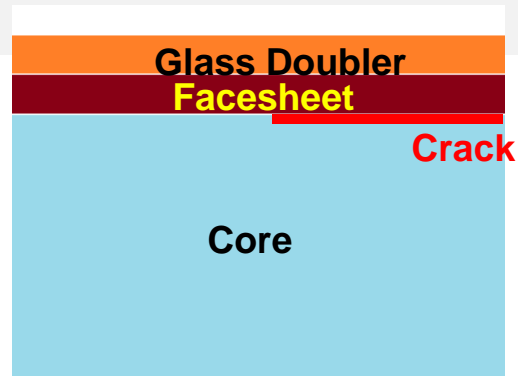
FACESHEET DOUBLER EFFECTS: No Doubler



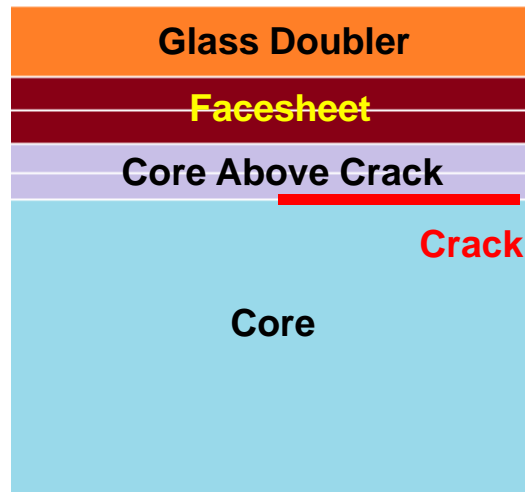
Crack at interface



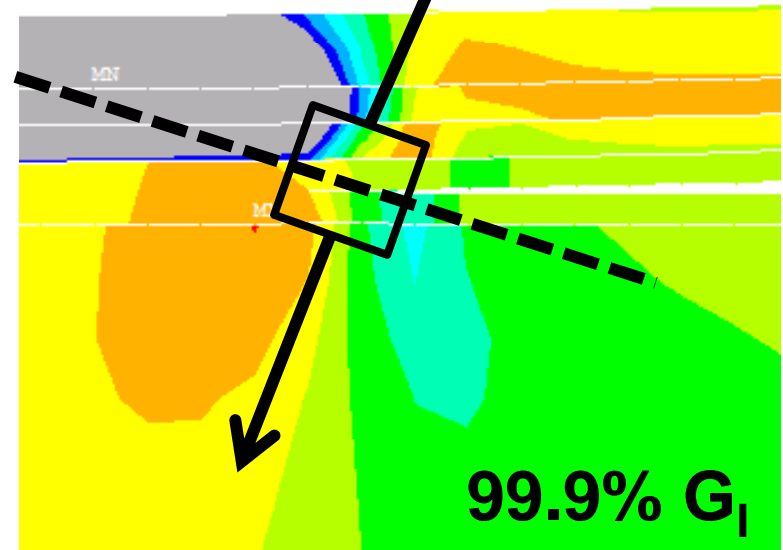
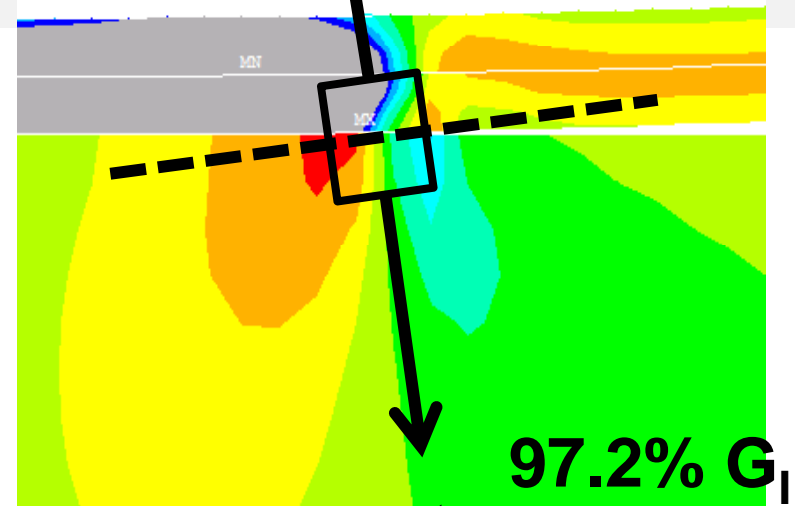
FACESHEET DOUBLER EFFECTS: Thin Doubler



At interface



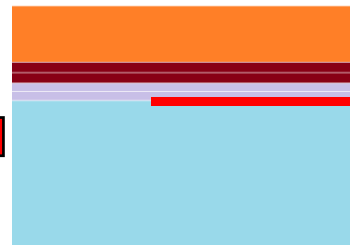
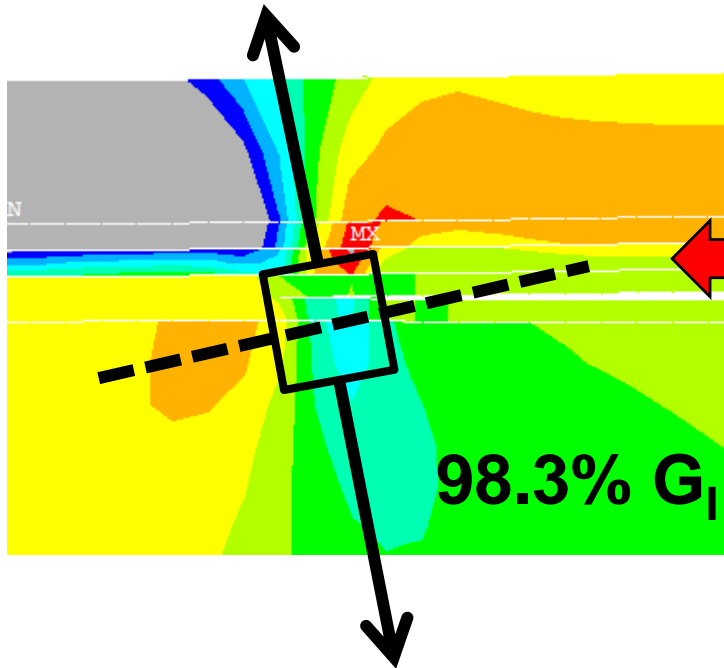
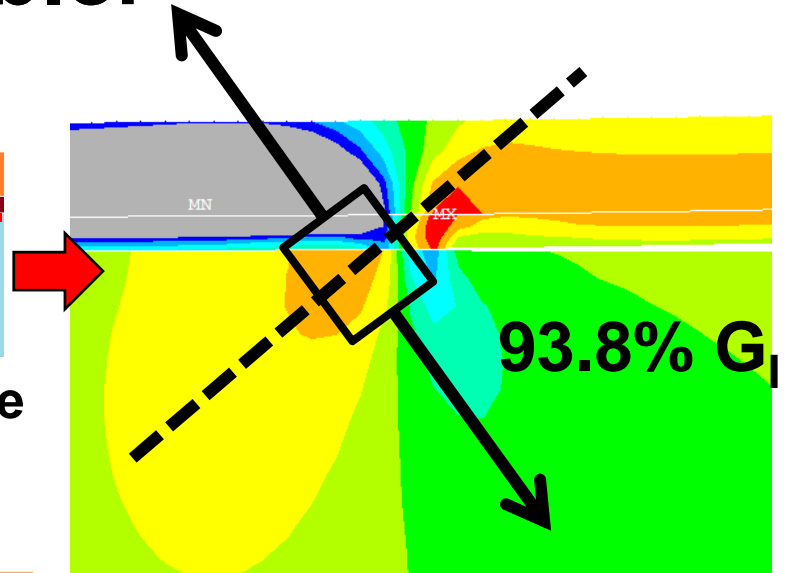
0.5 mm depth



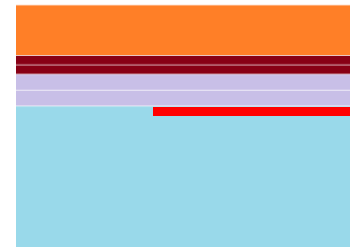
FACESHEET DOUBLER EFFECTS: Thick Doubler



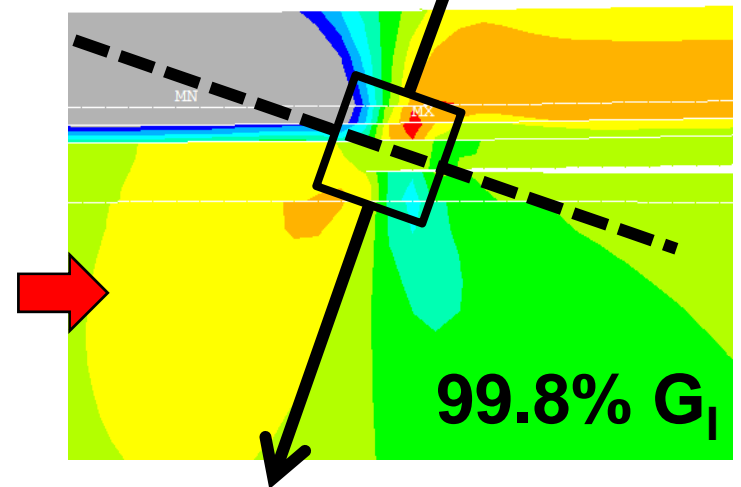
At interface



0.5 mm depth

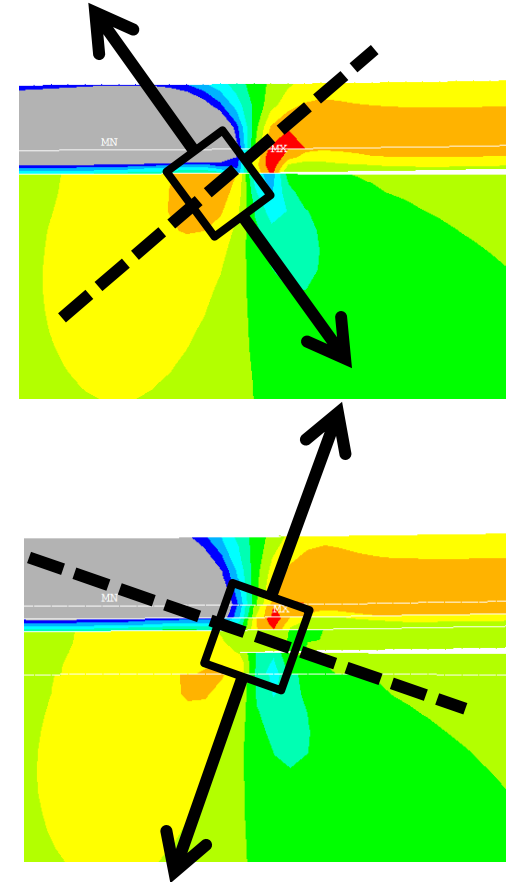


1 mm depth



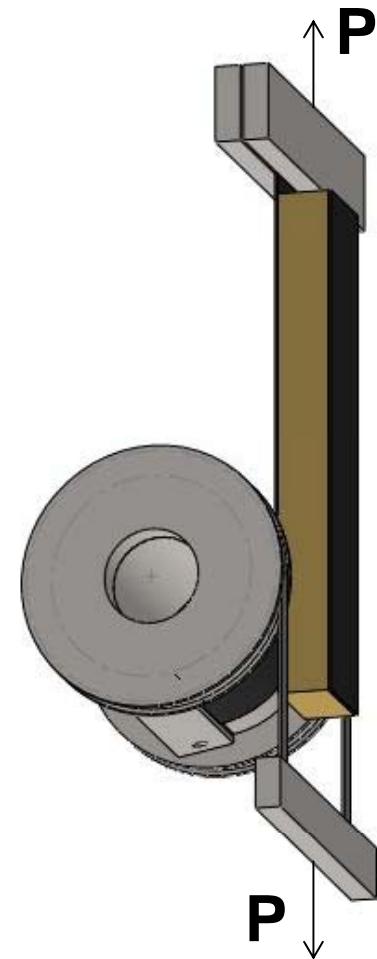
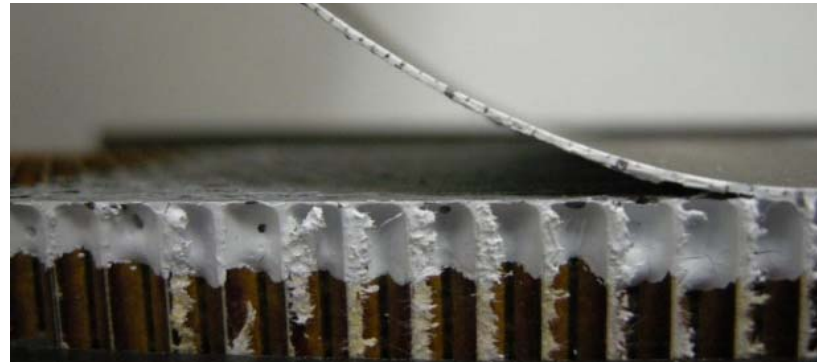
SUMMARY OF FINDINGS: Numerical Investigation

- SCB test appears to be Mode I dominant for all cases considered
- Mode II component produced by shear stresses in vicinity of crack tip
- Sign of shear stresses change as a function of:
 - Thickness of facesheet
 - Crack location in core
- Crack predicted to propagate closer to facesheet/core interface for thinner facesheets
- Use of doublers to reduce facesheet rotation is not recommended



EFFECTS OF FACESHEET CURVATURE: Use of Climbing Drum Peel (CDP) Test

- Facesheet curvature during SCB testing is dependent on facesheet thickness
- High curvature produced with thin facesheets not representative of that seen in sandwich structures with disbonds
- Use of Climbing Drum Peel test permits testing with prescribed facesheet curvature



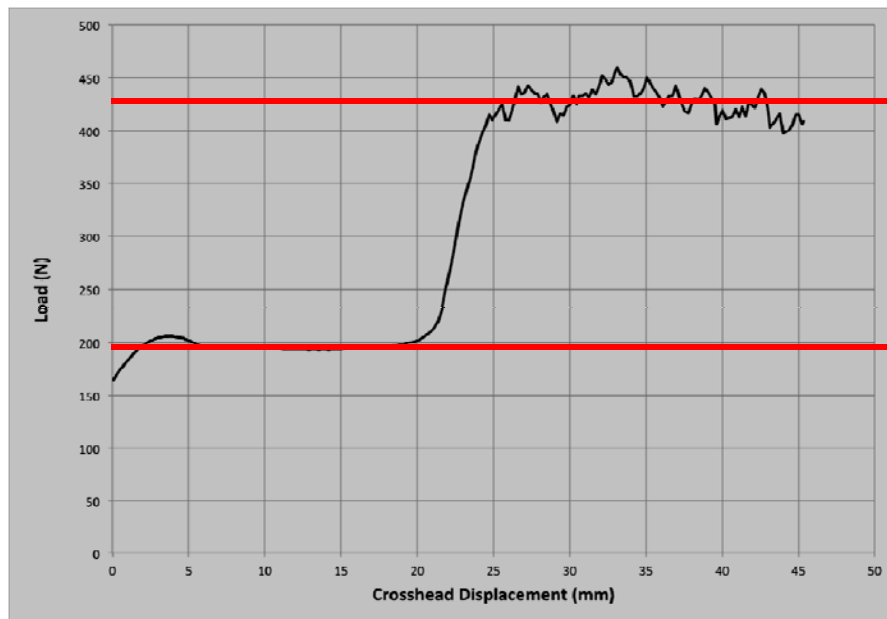
DETERMINATION OF ENERGY RELEASE RATE, G_C : Climbing Drum Peel (CDP) Test

Energy Release Rate, G_{IC} :
$$G_{IC} = \frac{(P_2 - P_1)(r_2 - r_1)}{w r_1}$$

r_2 = flange radius

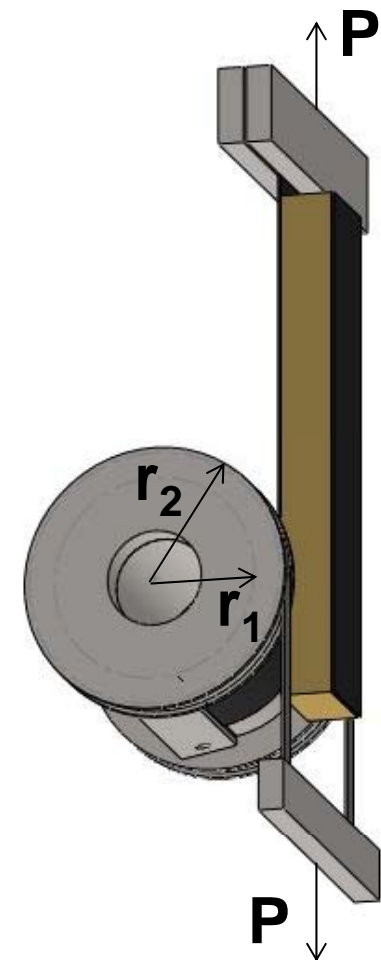
r_1 = drum radius + facesheet thickness

w = specimen width



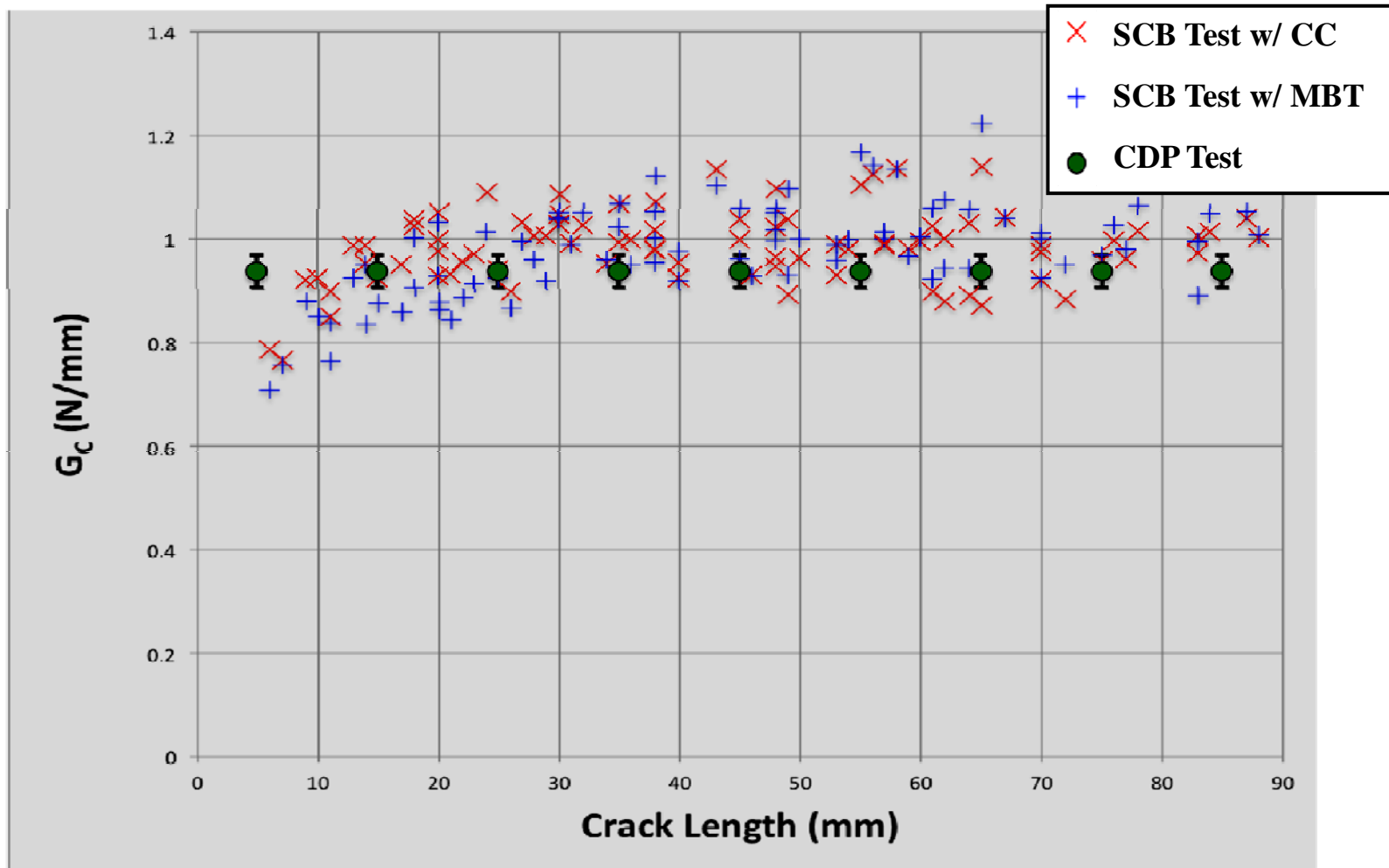
P_2

P_1



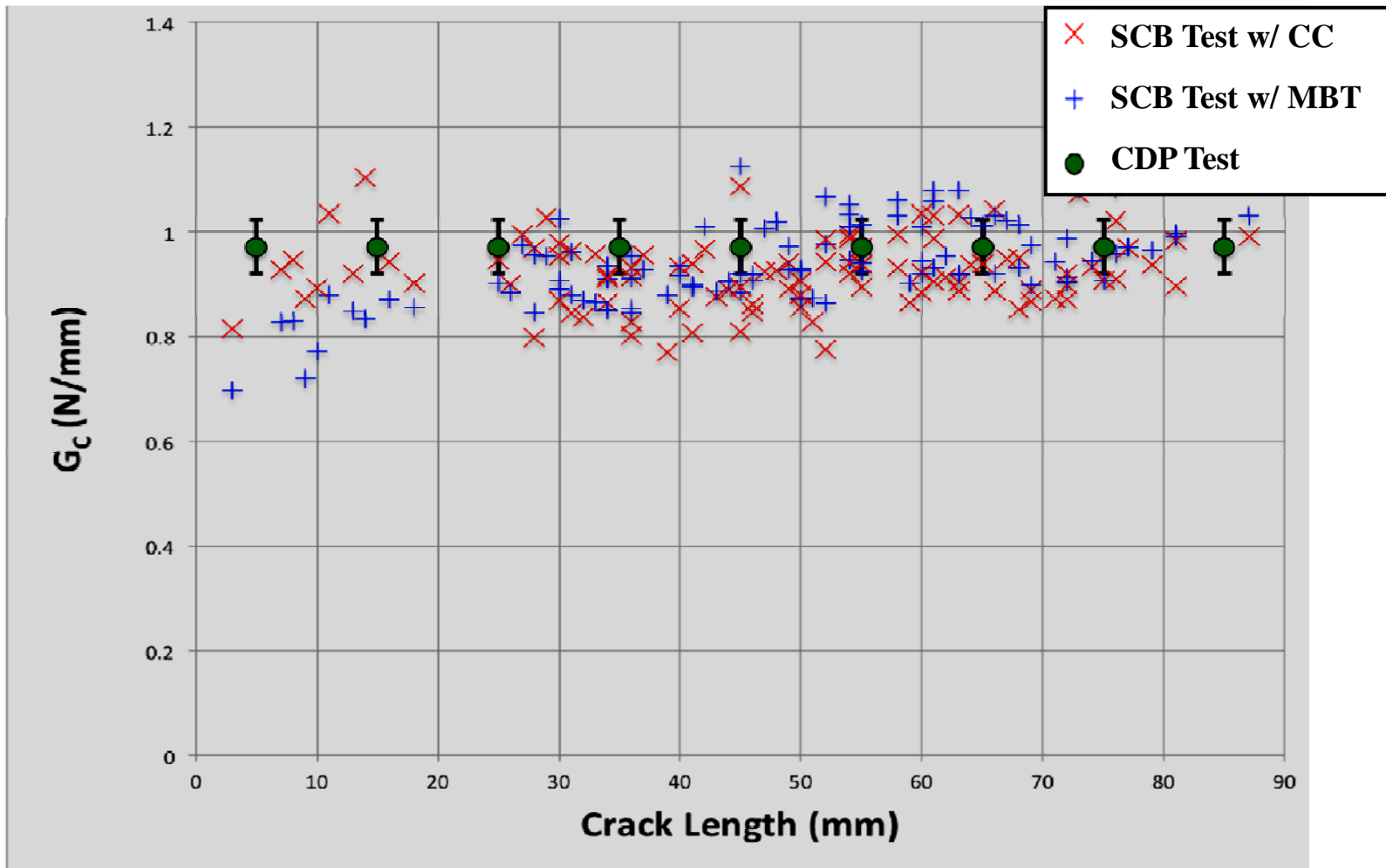
Single Cantilever Beam (SCB) Versus Climbing Drum Peel (CDP)

9 Ply ("Thick") Facesheet



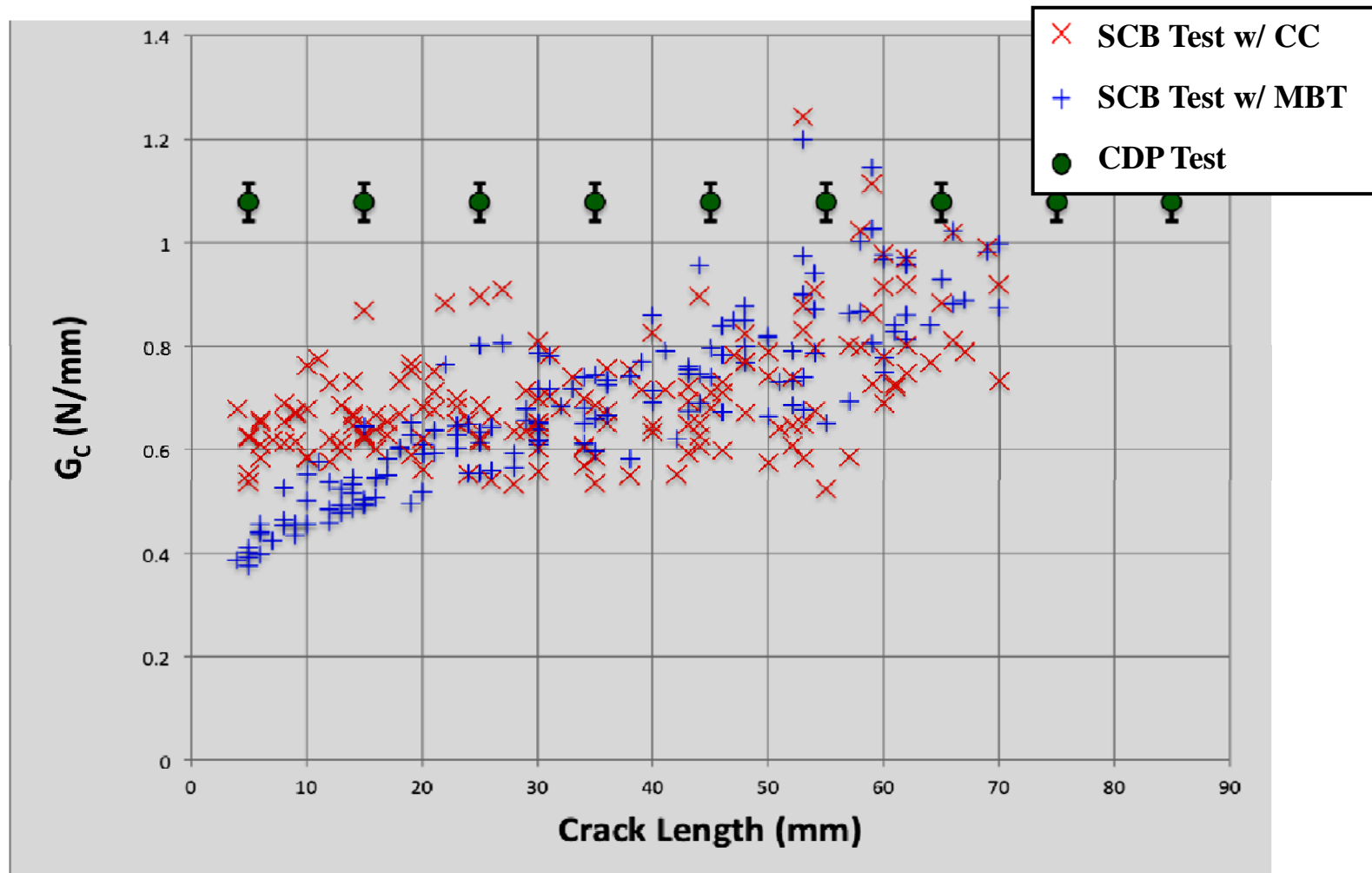
Single Cantilever Beam (SCB) Versus Climbing Drum Peel (CDP)

6 Ply ("Medium") Facesheet



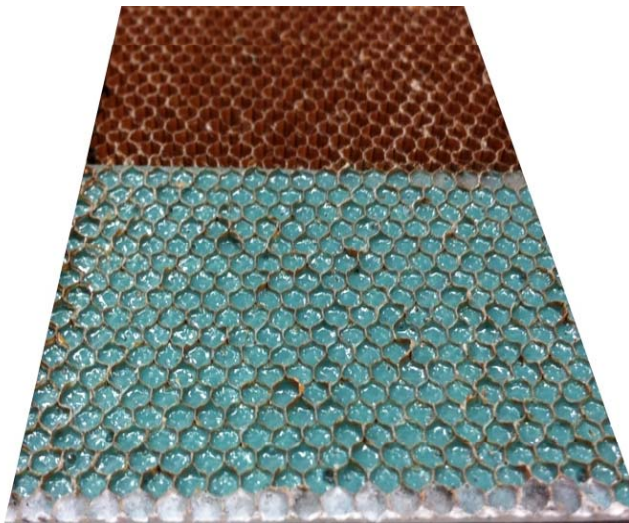
Single Cantilever Beam (SCB) Versus Climbing Drum Peel (CDP)

3 Ply ("Thin") Facesheet

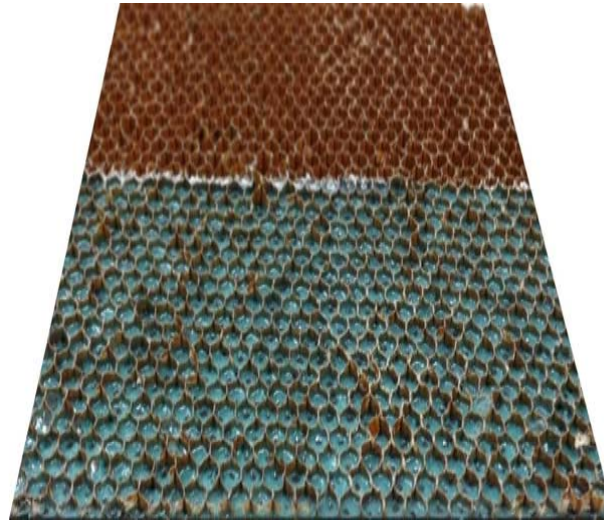


Effect of Facesheet Thickness: Single Cantilever Beam (SCB) Specimens

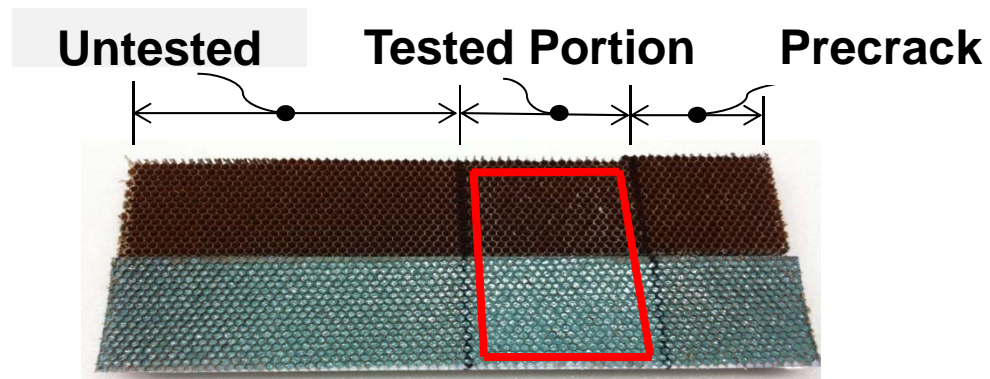
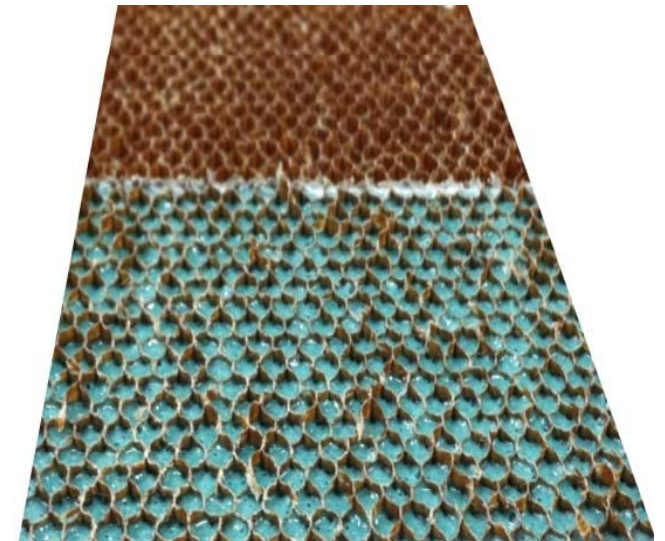
3 Ply Facesheet



6 Ply Facesheet

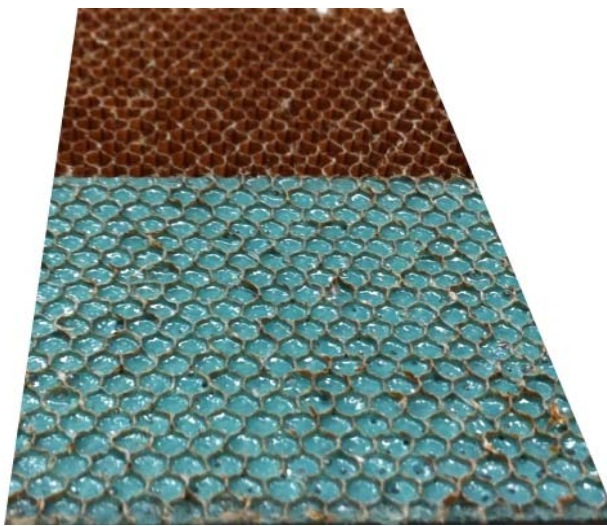


9 Ply Facesheet

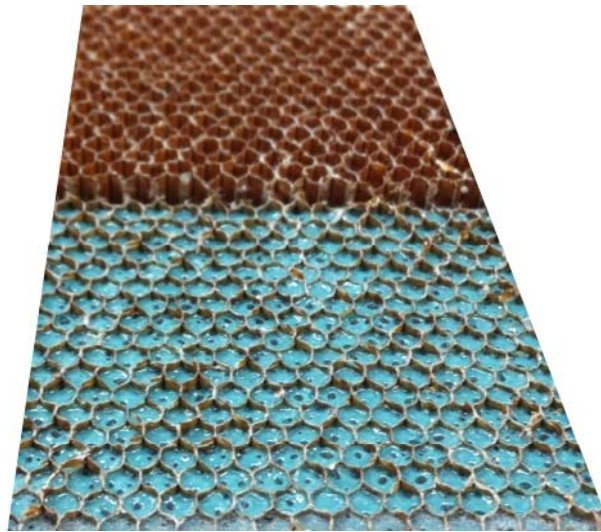


Effect of Facesheet Thickness: Climbing Drum Peel (CDP) Specimens

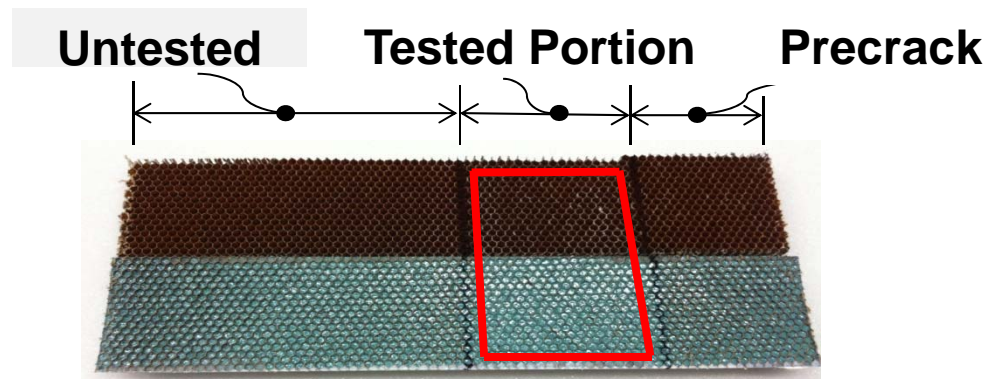
3 Ply Facesheet



6 Ply Facesheet



9 Ply Facesheet

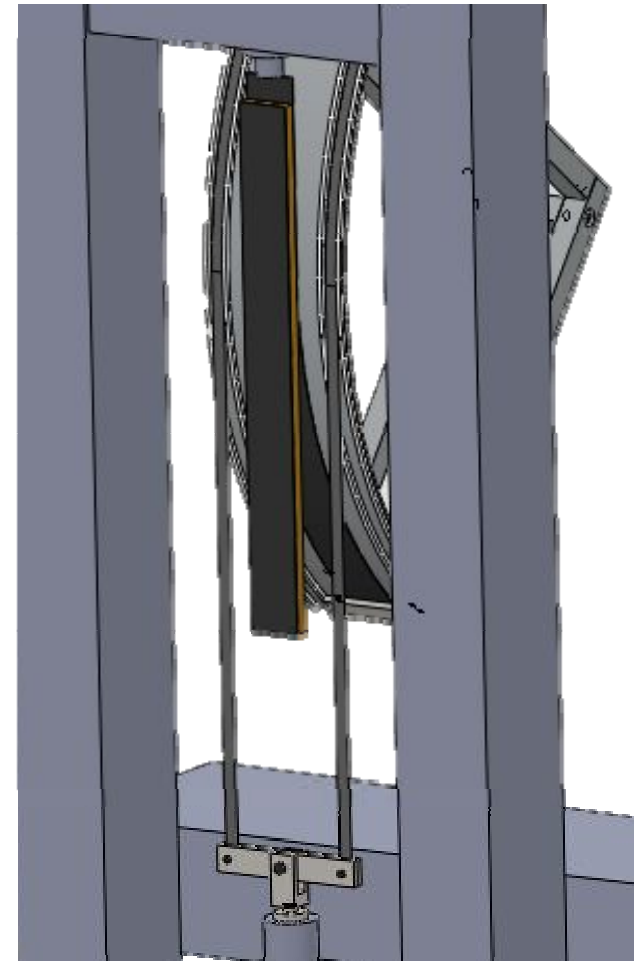
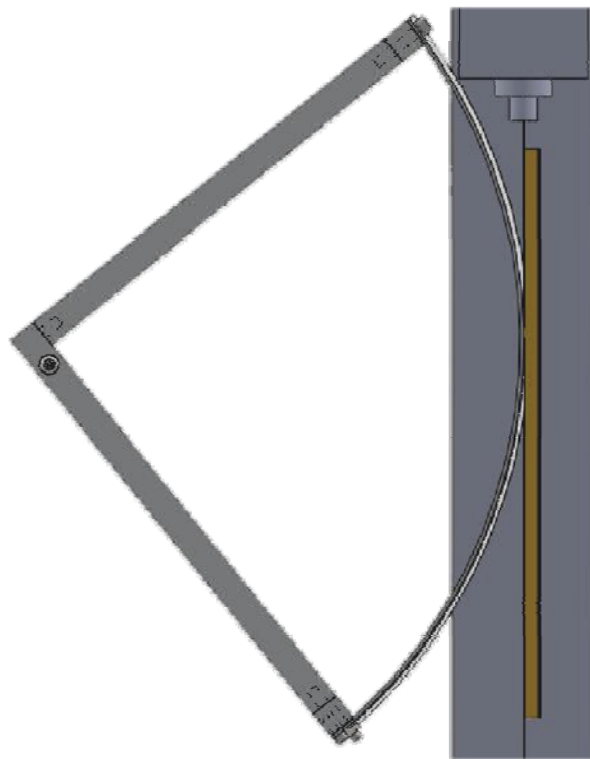


SUMMARY OF PRELIMINARY FINDINGS: Climbing Drum Peel Testing

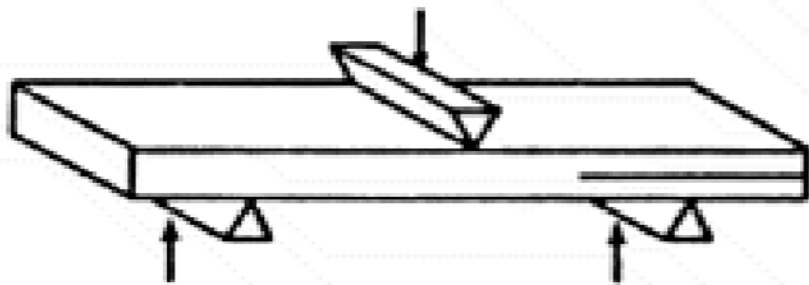
- G_C measurements from Climbing Drum Peel and Single Cantilever Beam tests in agreement for thicker facesheets
- G_C measurements from Single Cantilever Beam tests are reduced for thin facesheets
- Slight through-thickness difference in fracture location with facesheet thickness for both test methods

CURRENT FOCUS: Effects of Facesheet Curvature on Apparent G_c

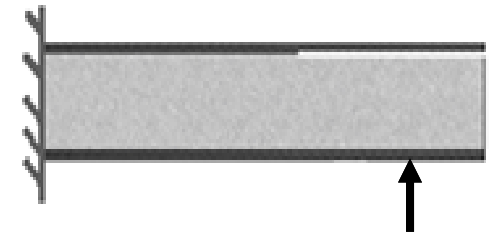
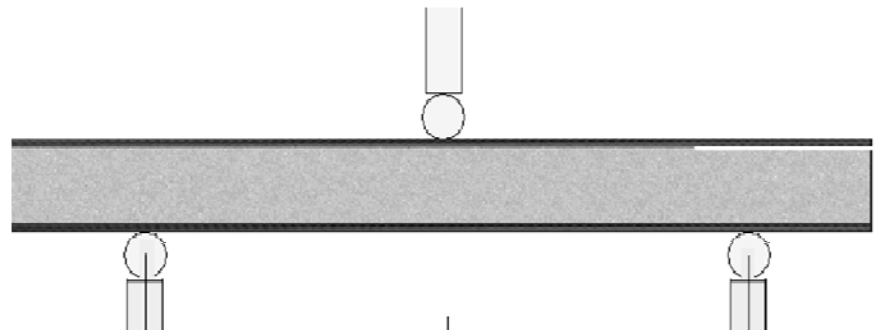
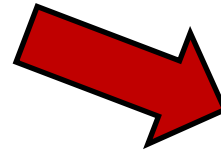
Preliminary design of a large radius
Climbing Drum Peel fixture



MODE II TEST CONFIGURATION: Edge-Notched Sandwich Configurations



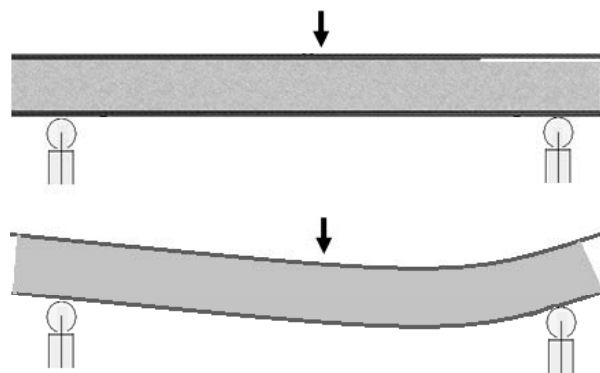
Monolithic Composites:
3 Point End Notch Flexure (3ENF)
(Currently proposed for ASTM
standardization)



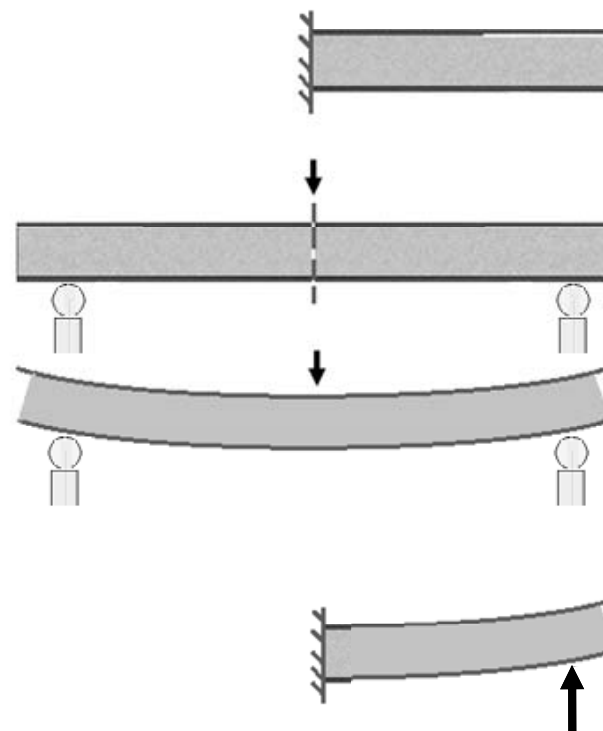
Sandwich Composites:
End Notch Cantilever (ENC)

MODE II END NOTCHED CANTILEVER TEST: Symmetrical Bending Version of 3-ENF

End Notched Flexure (Unsymmetric bending)



End Notched Cantilever (Symmetric bending)



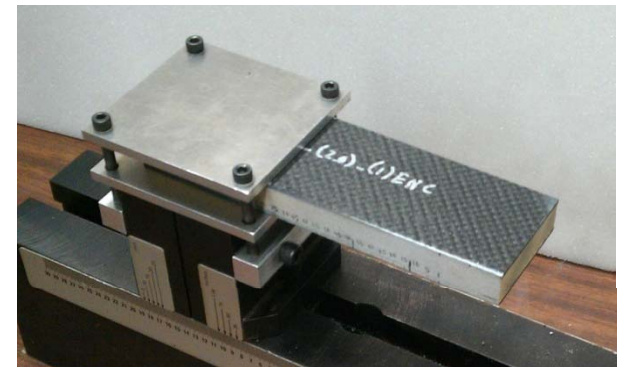
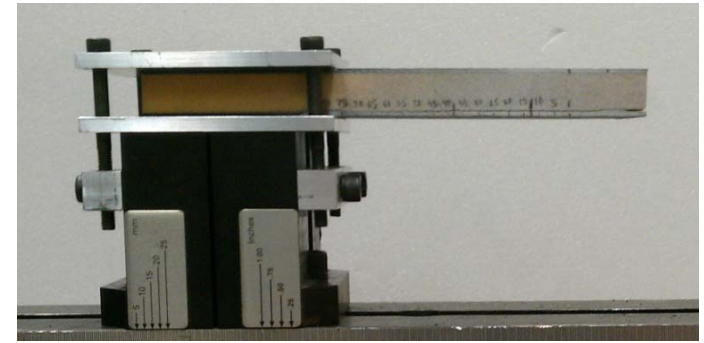
PROPOSED MODE II CONFIGURATION

End Notched Cantilever (ENC) Test

- Cantilever beam configuration
- Can be loaded upward (tension) or downward (compression)
- Predicted performance meets or exceeds that of 3-ENF configuration for all sandwich configurations considered to date

➔ Improved crack growth stability

- *Appears to be suitable for a standard Mode II test method*



SUMMARY

Benefits to Aviation

- Standardized fracture mechanics test methods for sandwich composites
 - Mode I fracture toughness, G_{IC}
 - Mode II fracture toughness, G_{IIC}
- Test results used to predict disbond growth in composite sandwich structures

