



# DEVELOPMENT AND EVALUATION OF FRACTURE MECHANICS TEST METHODS FOR SANDWICH COMPOSITES

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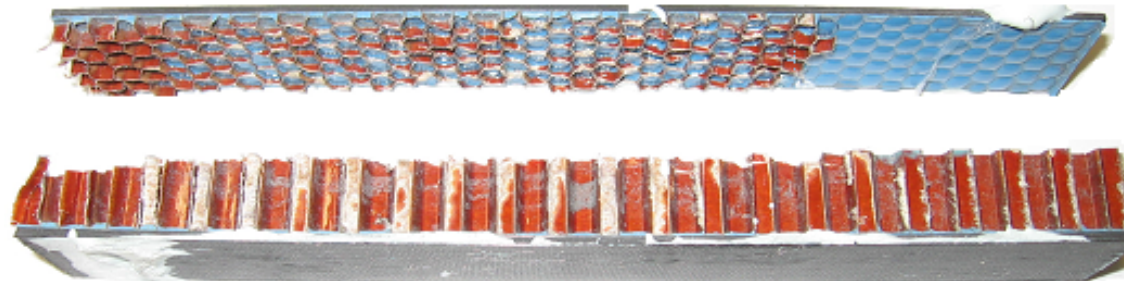
# FAA Sponsored Project Information



- **Principal Investigator: Dr. Dan Adams**
- **Graduate Student Researchers:**
  - Chris Weaver
  - Andy Gill
  - Brad Kuramoto
  - Josh Bluth
- **FAA Technical Monitor**
  - Curt Davies

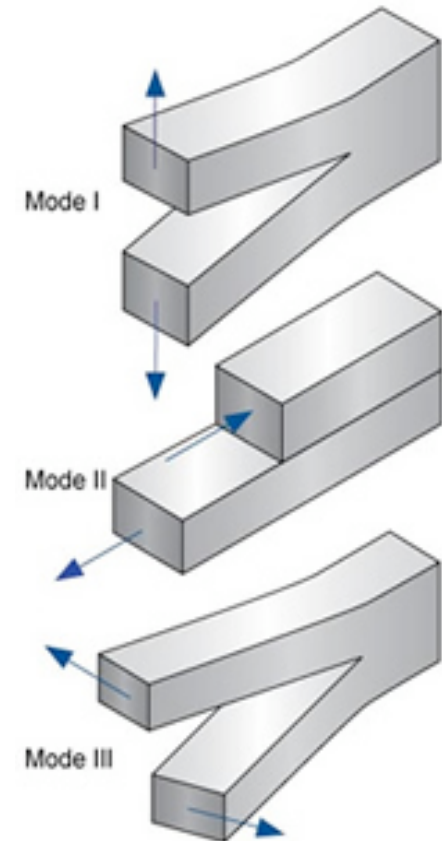
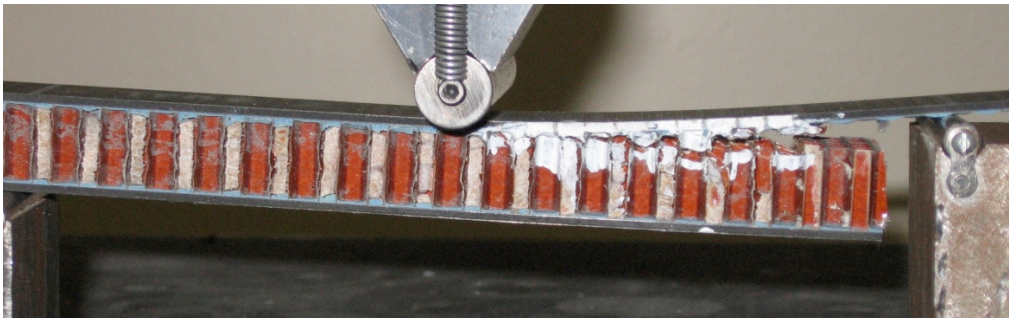
## BACKGROUND: FRACTURE MECHANICS TEST METHODS FOR SANDWICH COMPOSITES

- Fracture mechanics test methods for composites have reached a high level of maturity
- Less attention to sandwich composites
  - Focus on particular sandwich materials
  - Focus on environmental effects
  - No consensus on a suitable test configuration or specimen geometry for Mode I or Mode II fracture toughness testing



# RESEARCH OBJECTIVE

- **Develop fracture mechanics test methods for sandwich composites**
  - Focus on facesheet core delamination
  - Both Mode I and Mode II
  - Suitable for ASTM standardization





# RESEARCH APPROACH: THREE PHASE PROGRAM



- **PHASE I: Identification and initial assessment of candidate test methodologies**
- **PHASE II: Selection and optimization of best suited Mode I and Mode II test methods**
- **PHASE III: Development of draft ASTM standards**

# PHASE I (REVIEW):

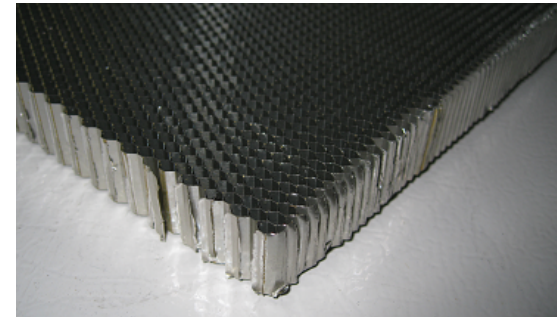
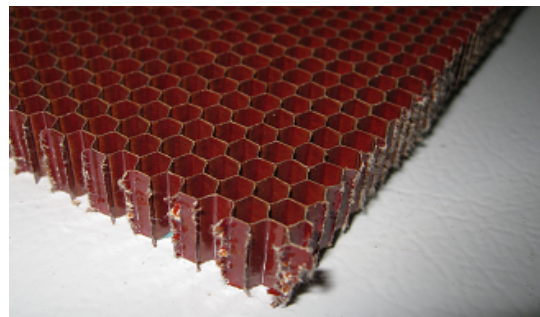
## Identification and initial assessment of candidate test methodologies

- **Identify candidate Mode I and Mode II test methodologies**
  - Literature review- Lead to five Mode I and eight Mode II configurations
  - Modifications from adhesive and composite laminate tests
  - Original concepts were also created
- **Identification of materials and geometries currently in use for structural sandwich composites**
- **Assessment of candidate test configurations using finite element analysis**
- **Select promising configurations for mechanical testing**

# PHASE I CONTINUED

## Identification and initial assessment of candidate test methodologies

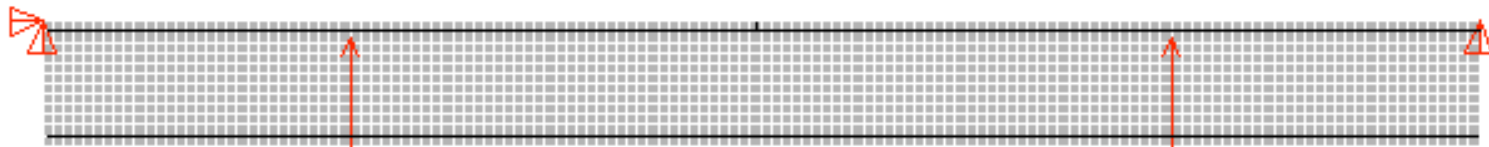
- **Three core materials (12-14 mm thickness)**
  - Polyurethane foam core with density of 160 kg/m<sup>3</sup> (10 lb/ft<sup>3</sup>)
  - Nomex honeycomb core
  - Aluminum honeycomb core
  
- **Two facesheet materials (1.3-1.5 mm thickness each)**
  - Woven carbon/epoxy, VARTM processed
  - Unidirectional carbon/epoxy, secondary bonding





## PHASE I CONTINUED:

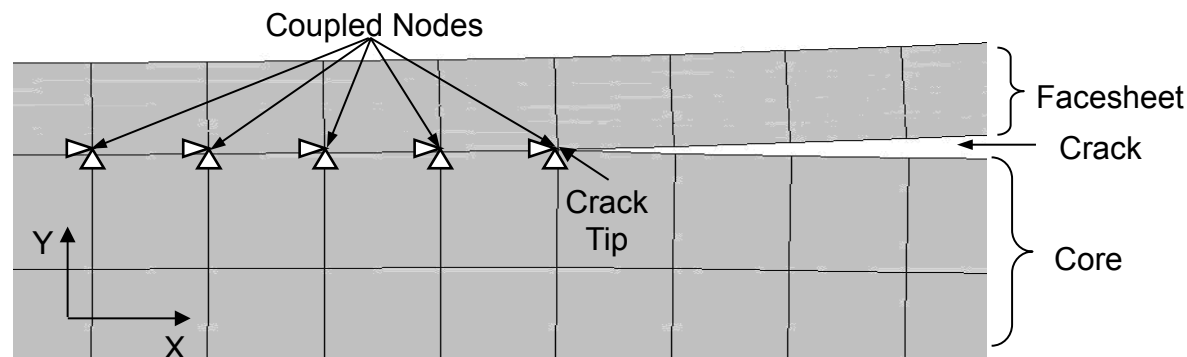
- **Finite element analysis of initial test configurations**
  - Evaluate fracture mode mixity (i.e. Mode I vs. Mode II)
  - Analyze stress state within specimen
  - Monitor crack opening after load application (Mode II)
  - Determine suitable loading geometries
  - Select promising Mode I and Mode II test configurations for mechanical testing





## ■ Finite element modeling

- ANSYS 8.0 software
- Two-dimensional, plane strain, geometrically nonlinear analyses
- Crack path created with a row of overlapping nodes, coupled beyond crack tip
- Crack closure method used to calculate energy release rates,  $G_I$  and  $G_{II}$



# PHASE I MECHANICAL TEST RESULTS:

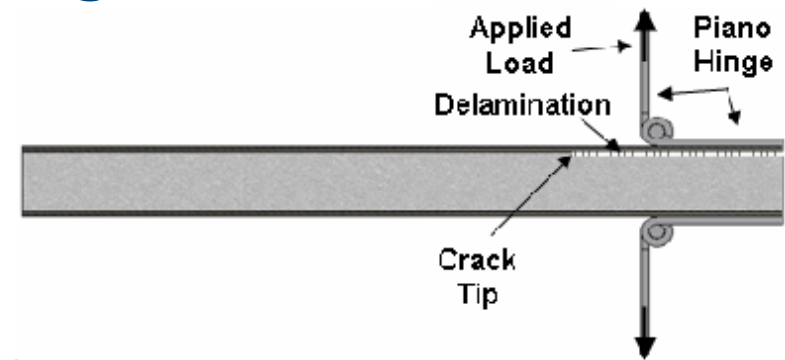
## Mode I Investigation

### ■ Identification of Mode I test configurations



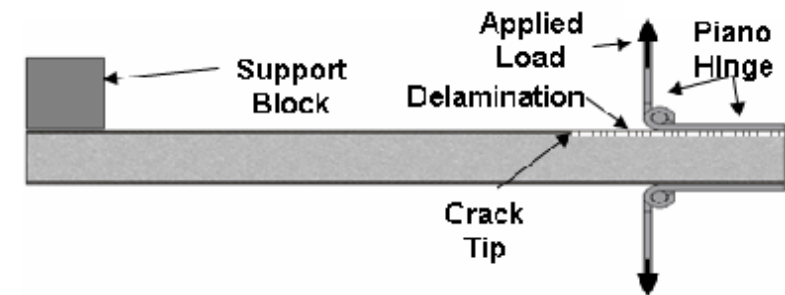
#### □ Double Cantilever Beam (DCB)

- Significant Mode II component
- Significant bending stresses in core
- Crack “kinking” for Nomex honeycomb core
- Specimen rotation due to off axis loading
- Determined to be unsuitable for a standard test method



#### □ Modified DCB (MDCB)

- Significant Mode II component
- Crack “kinking” for Nomex honeycomb core
- Determined to be unsuitable for a standard test method

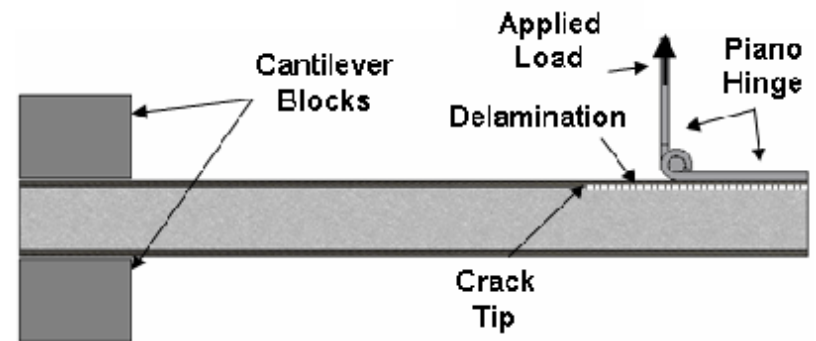


# PHASE I MECHANICAL TEST RESULTS:

## Mode I Investigation

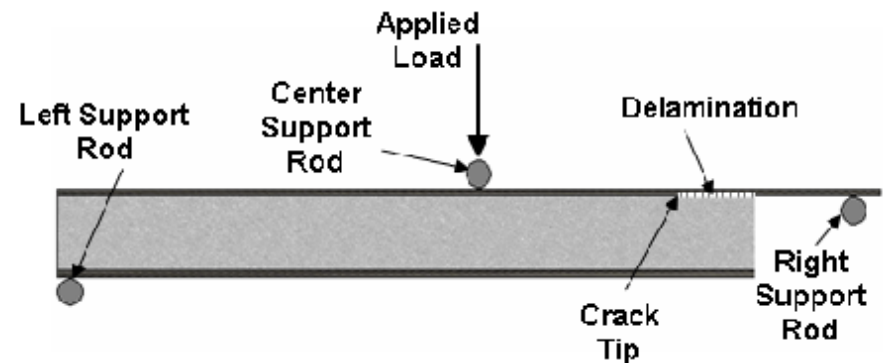
### ❌ □ Single Cantilever Beam (SCB) with cantilever beam support

- Significant Mode II component
- Crack “kinking” for Nomex honeycomb core
- Determined to be unsuitable for a standard test method



### ❌ □ Three Point Flexure (TPF)

- Significant bending stresses in core
- Extra machining operations required for specimen
- Determined to be unsuitable for a standard test method



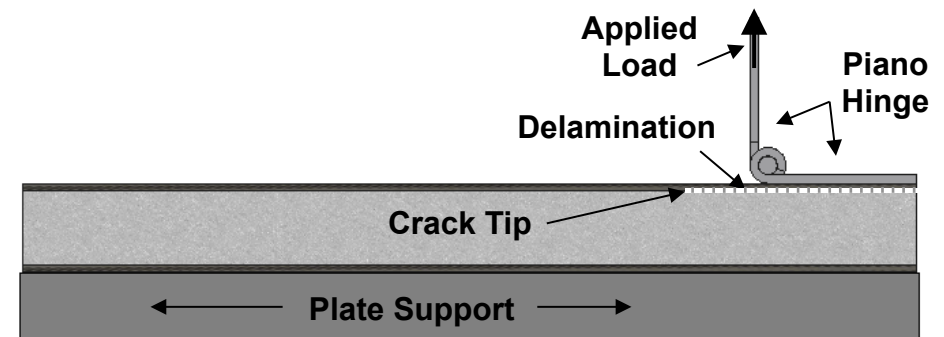
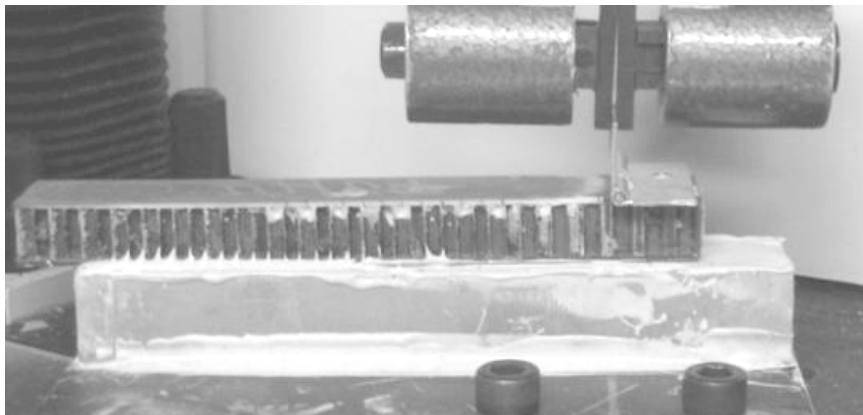
# PHASE I MECHANICAL TEST RESULTS:

## Mode I Investigation



### □ Plate-Supported SCB (MSCB)

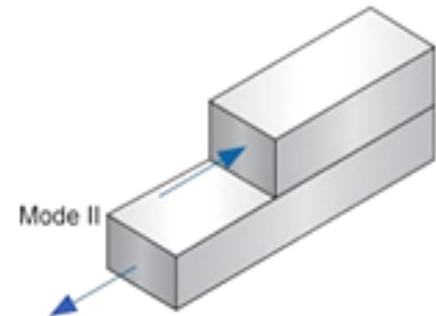
- Elimination of bending of sandwich specimen
- Minimal Mode II component (less than 5%)
- No significant bending stresses in core
- No crack “kinking” observed
- *Appears to be suitable for a standard test method*



# PHASE I RESULTS:

## Mode II Investigation

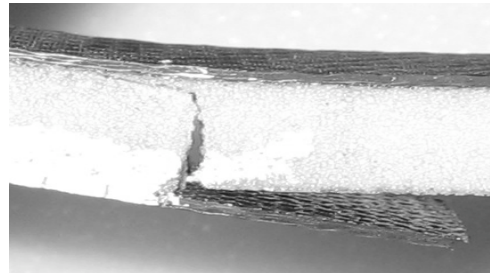
- **Identification of Mode II test configuration**
  - Three-point End Notch Flexure (3ENF)
  - Mixed Mode Bending (MMB)
  - End Load Split (ELS)
  - Four-point delamination test
  - Cracked Sandwich Beam (CSB) with hinge
  - Modified CSB
  - Facesheet delamination test
  - DCB with uneven bending moments
  - Three-point cantilever
  - Double sandwich test



# PHASE I RESULTS:

## Mode II Investigation

- **Challenges in developing a suitable Mode II test**
  - Maintaining Mode II dominated crack growth with increasing crack lengths
  - Obtaining crack opening during loading
  - Obtaining stable crack growth along facesheet/core interface
  - Only two of the ten investigated test configurations produced any form of interlaminar stable crack growth
    - Modified CSB (MCSB)
    - Mixed Mode Bending (MMB)
  - Seven test configurations experienced crack “kinking”, the other unstable

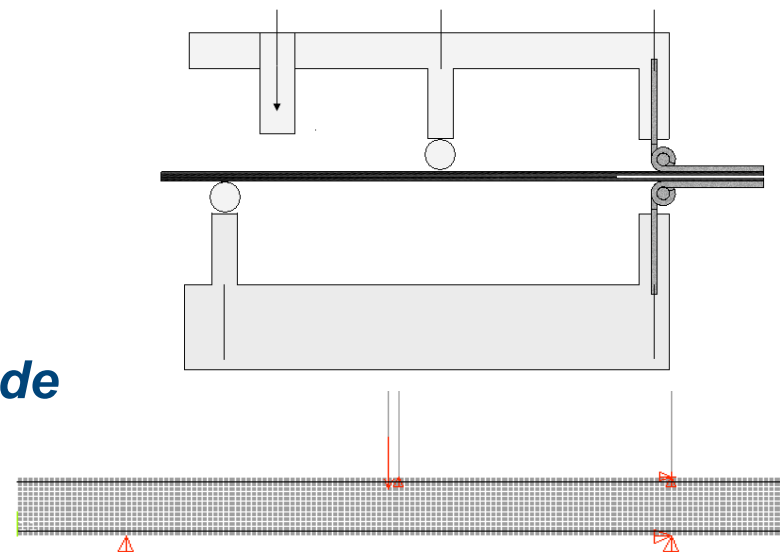
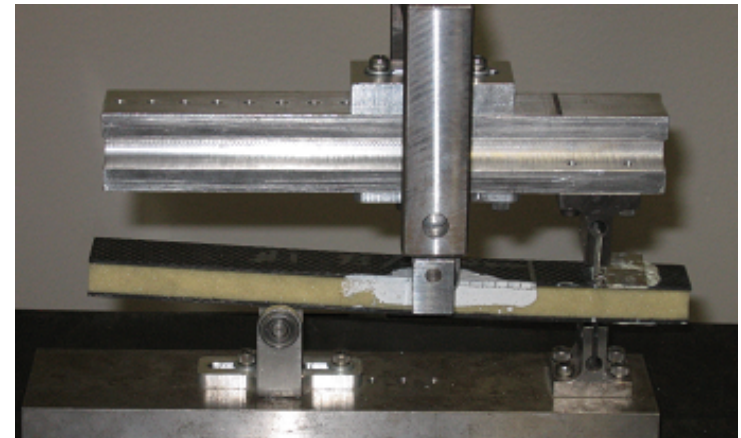


# PHASE I MECHANICAL TEST RESULTS:

## Mode II Investigation

- ✗ ■ **Mixed Mode Bending (MMB)**
  - Crack opening as delamination propagates for foam core
  - Possible to achieve high percentage Mode II (>90%) using short lever arm lengths
  - Semi-stable crack growth for foam core
  - Crack “kinking” for Nomex honeycomb core
  - Core crushing for aluminum honeycomb core

*Not well suited for a standard Mode II test method*



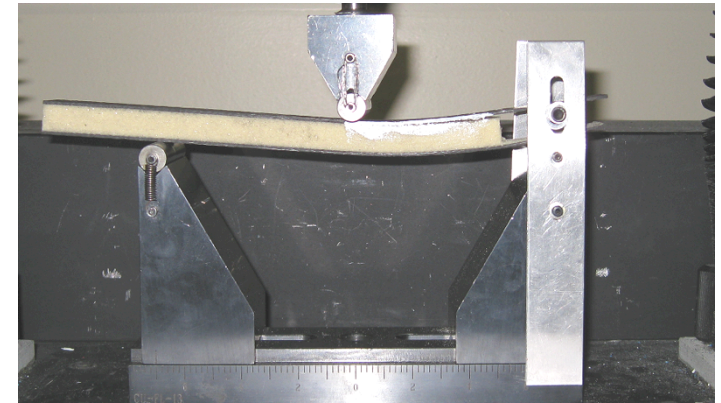
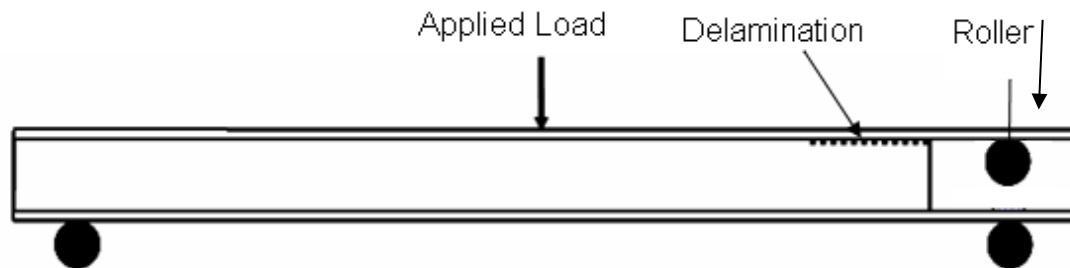


# PHASE I MECHANICAL TEST RESULTS:

## Mode I Investigation

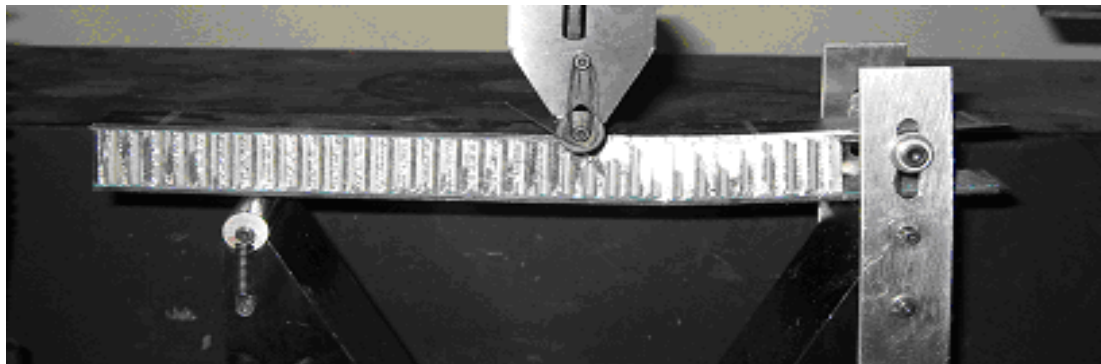
- ✓ **Modified Cracked Sandwich Beam with Hinge**
  - Creates crack opening as delamination propagates
  - High percentage Mode II (>80%) for all materials investigated
  - Semi-stable crack growth along facesheet/core interface

*Appears to be suitable for a standard Mode II test method*



## PHASE II ACTIVITIES: Further Development of Mode I and Mode II Test Methods

- ➔ ■ **Sensitivity study – determination of acceptable range of specimen parameters**
- ➔ ■ **Development of suitable test fixturing**
  - **Development of suitable test procedures**
  - **Development of suitable data analysis methods**

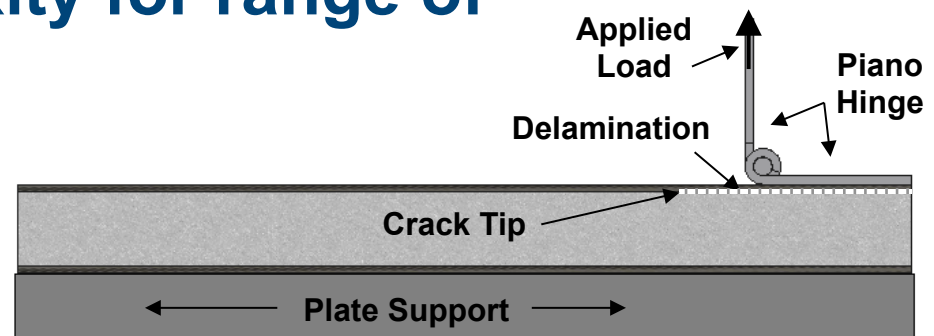


# SENSITIVITY STUDIES: Determination of Acceptable Ranges of Specimen Parameters

- **Facesheet parameters**
  - Thickness, flexural stiffness, flexural strength
- **Core parameters**
  - Thickness, density, stiffness, strength
- **Specimen and delamination geometry**

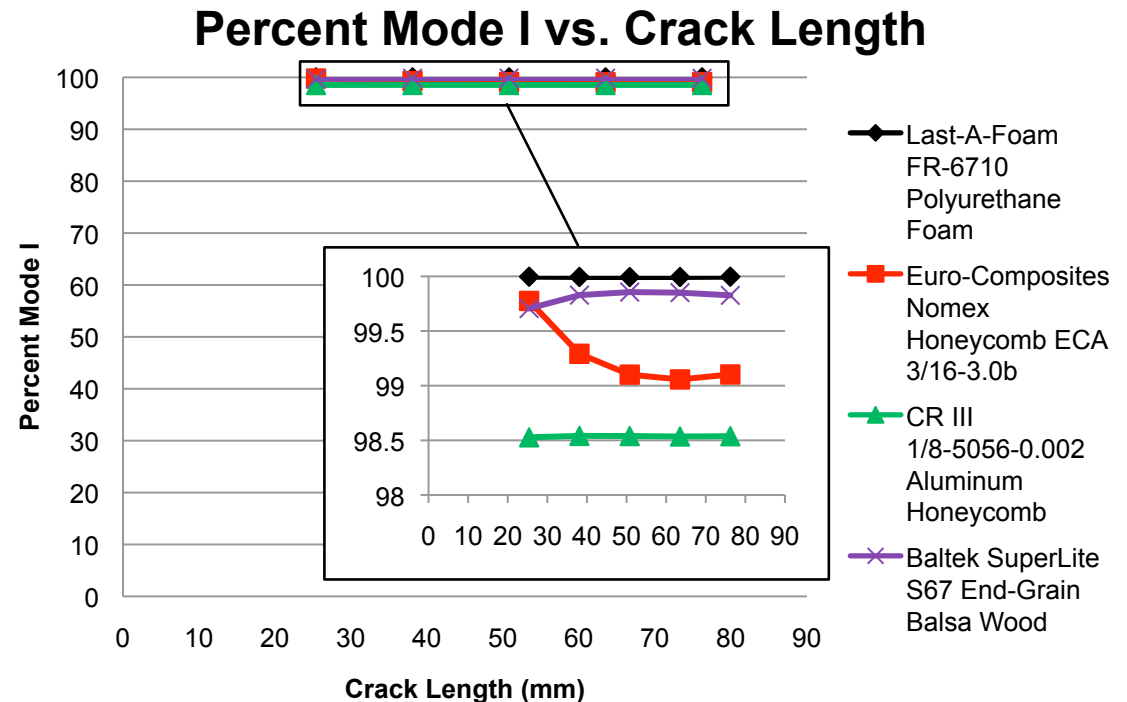
# CURRENT FOCUS: Mode I Sensitivity Study

- Use of plate-supported Single Cantilever Beam (SCB) test
- Focus on two parameters of concern
  - Sandwich core material
  - Facesheet thickness
- Investigate mode mixity for range of delamination lengths



# MODE I SENSITIVITY STUDY: Effect of Core Material on %Mode I

- Mode I dominant over range of cores considered
- Minimal variability among materials and crack lengths
- Test appears suitable for a wide range of common core materials

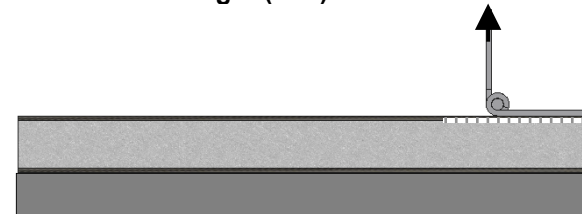
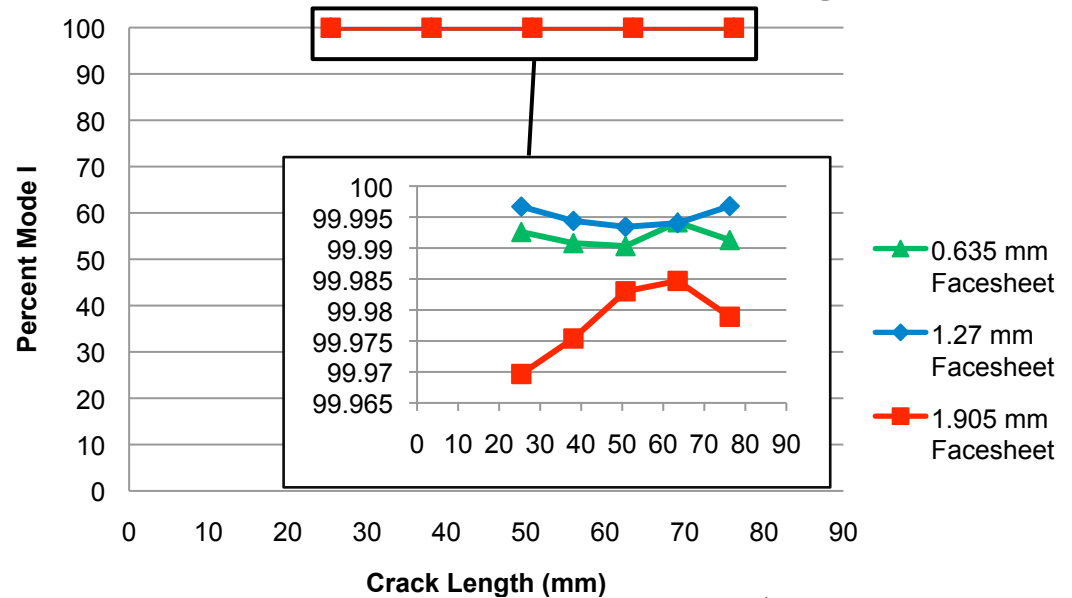


# MODE I SENSITIVITY STUDY: Effect of Facesheet Thickness

*Woven carbon/epoxy facesheets, polyurethane foam core*

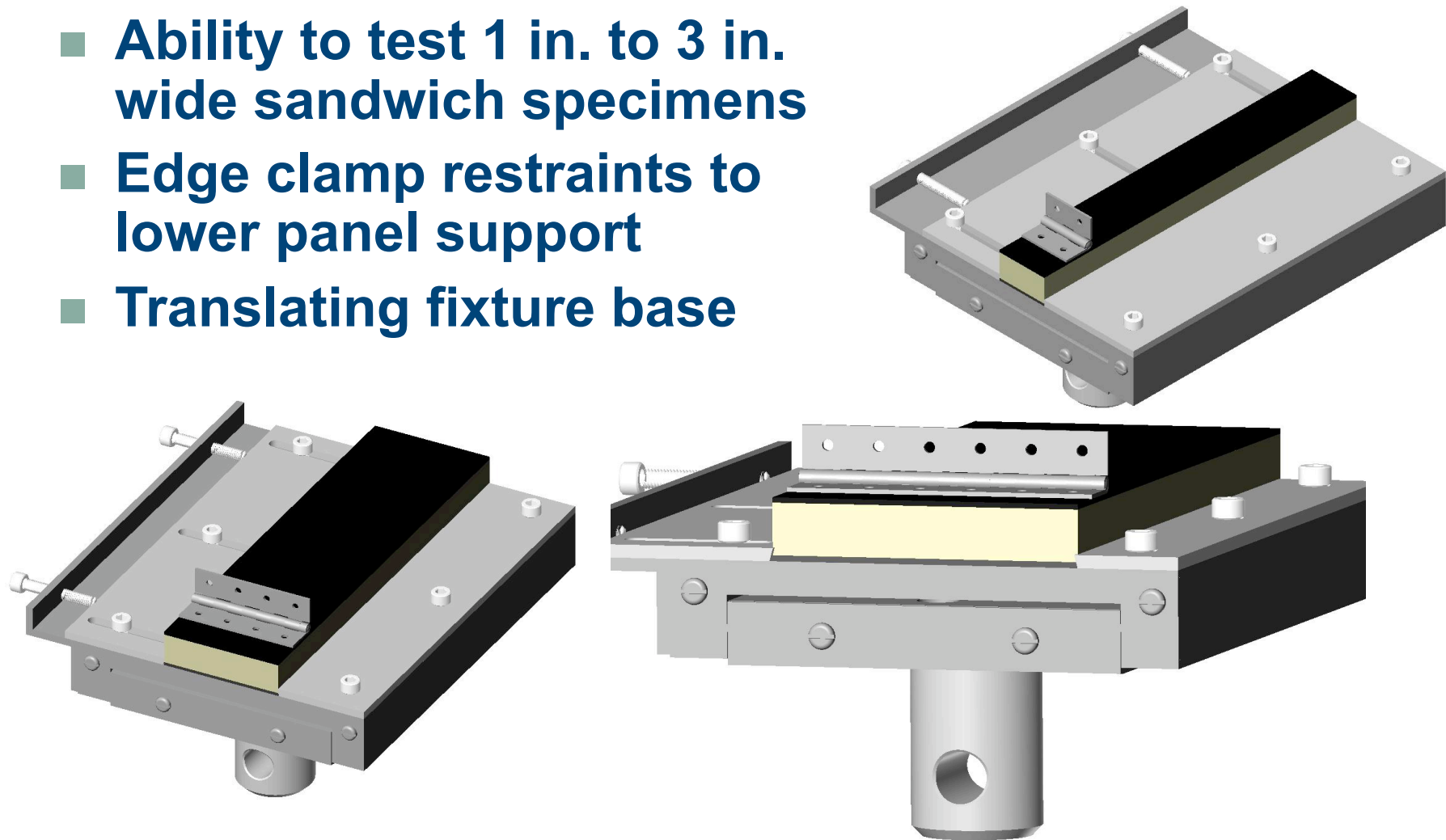
- Mode I dominant over range of facesheet thicknesses considered

Percent Mode I vs. Crack Length



# CURRENT FOCUS: Mode I Test Fixture Development

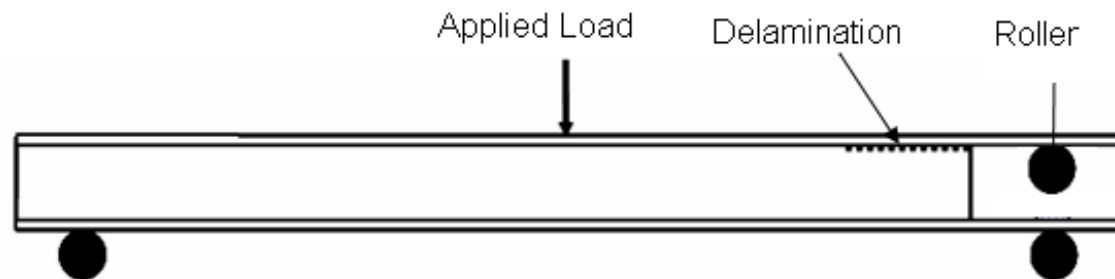
- Ability to test 1 in. to 3 in. wide sandwich specimens
- Edge clamp restraints to lower panel support
- Translating fixture base





## CURRENT FOCUS: Mode II Sensitivity Study

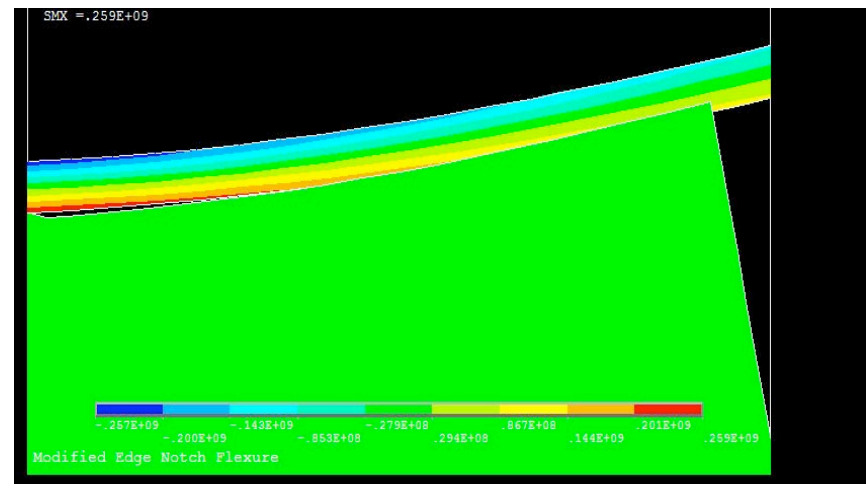
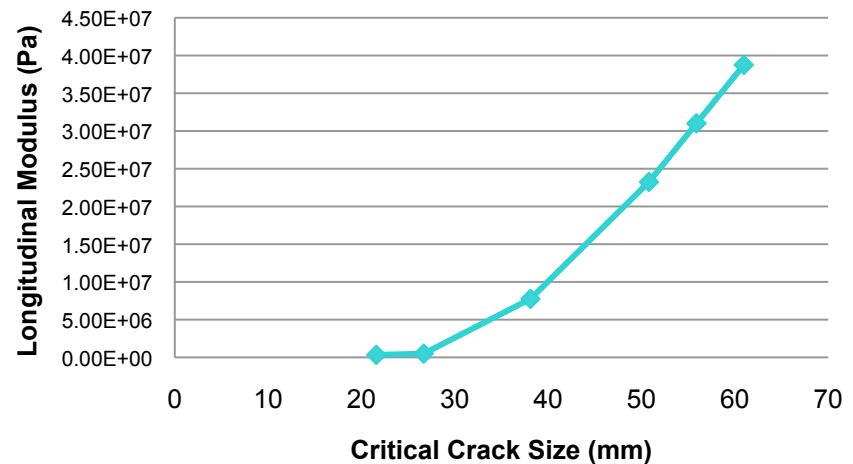
- **Use of Modified Cracked Sandwich Beam**
- **Determination of acceptable range of specimen parameters**
  - Core thickness, stiffness
  - Facesheet flexural stiffness
- **Investigate mode mixity and crack opening for range of delamination lengths**



# MODE II SENSITIVITY STUDY: Effect of Core Material

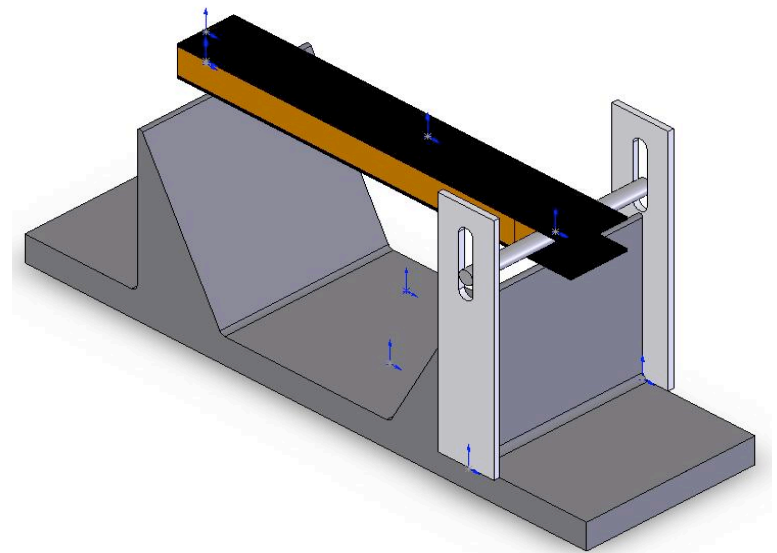
- Varying the cores in plane modulus has little affect on % Mode II
  - Foam, Nomex, and aluminum honeycomb all remained above 90%
- Failure of test decided when there is core/face-sheet interaction
- In plane modulus of core affects crack length at which interaction begins
- Use trend line to develop MCSB core material test limits

Longitudinal Direction Modulus of Core vs. Critical Crack Size



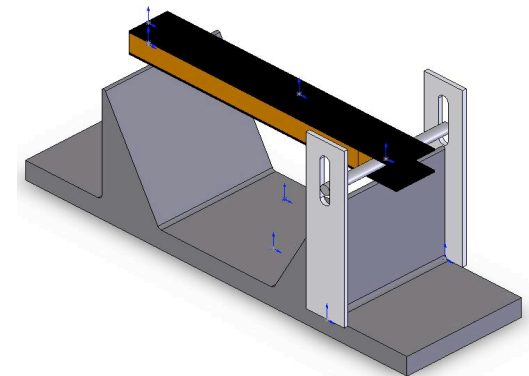
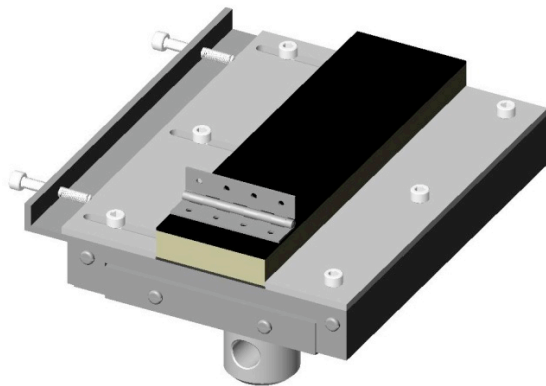
# CURRENT FOCUS: Mode II Test Fixture Development

- **Modified three-point flexure configuration**
- **Emphasis on minimizing specialized specimen preparation-core removal**
- **Proposed design would support top face sheet without need of core removal**



## UPCOMING ACTIVITIES: Further Development of Mode I and Mode II Test Methods

- **Sensitivity study – determination of acceptable range of specimen parameters**
  - Computational simulations to determine limits
  - Experimental validation of limits
- **Fabrication and evaluation of test fixturing**
- **Development of suitable test procedures**
- **Development of suitable data analysis methods**





**Thank You For Your Time**  
**Any Questions**