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Delamination/Disbond Arrest Features in Aircraft Composite Structures

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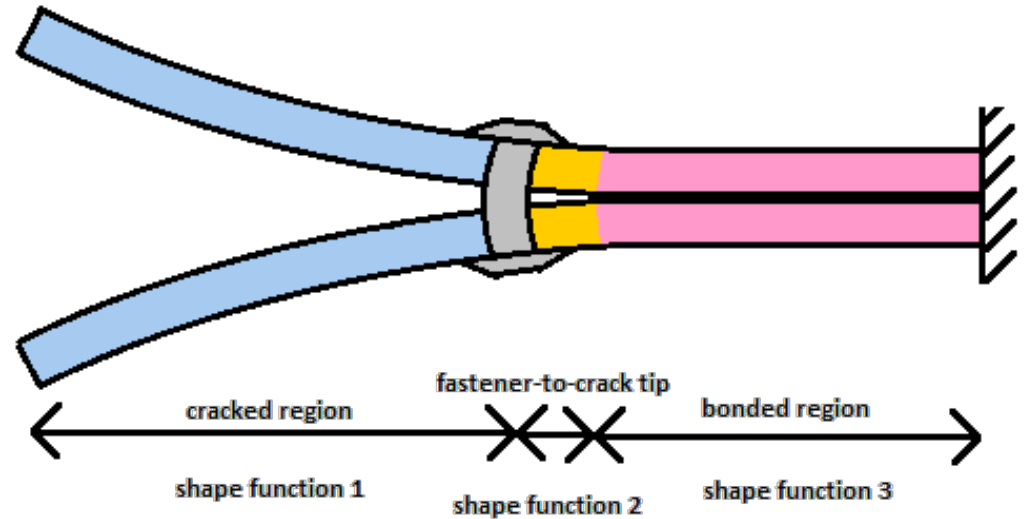
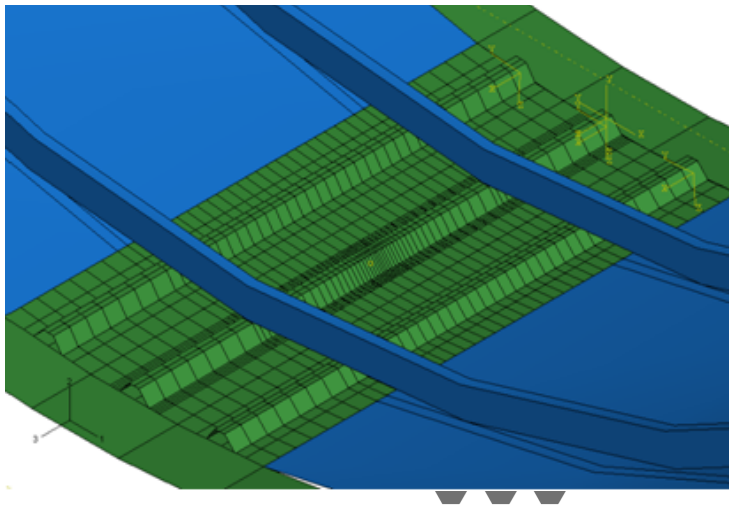
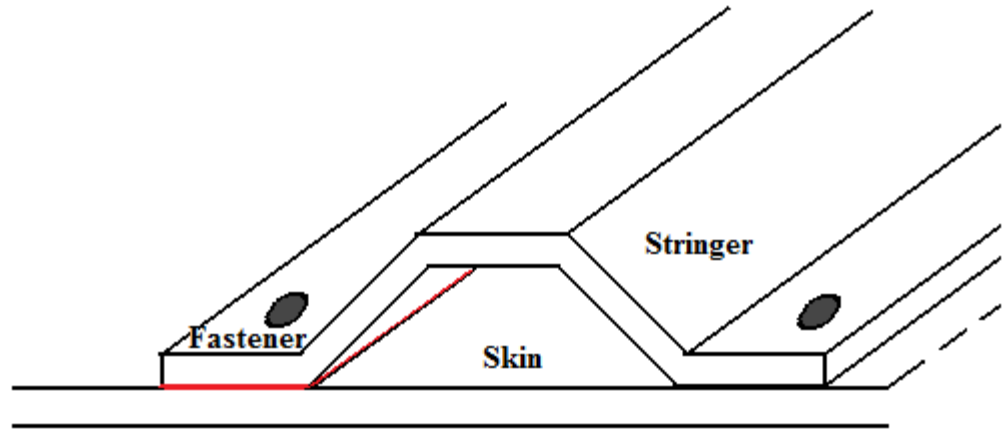
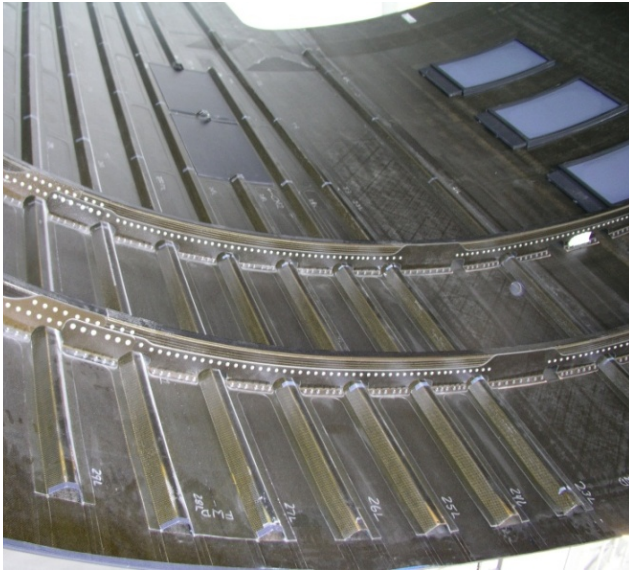
Sponsored Project Information

- **Principal Investigator:**
 - Dr. Kuen Y. Lin, Aeronautics and Astronautics, UW
- **Research Assistants:** Luke Richard, Wenjing Liu, UW
- **FAA Technical Monitor:** Lynn Pham
- **Other FAA Personnel:** Curtis Davies, Larry Ilcewicz
- **Industry Participants:**
 - **Boeing:** Marc Piehl, Gerald Mabson, Eric Cregger, Matthew Dilligan, Caihua Cao, Eric Sager
 - **Toray:** Kenichi Yoshioka, Dongyeon Lee, Masahiro Hashimoto, Felix Nguyen
- **Industry Sponsors:** Toray and Boeing

Research Objectives

- Enhance accuracy of crack arrest capability predictions for varying laminate and fastener configurations
 - Develop understanding of crack propagation and arrest by multiple fasteners under static and fatigue loading
 - Develop knowledge of how crack propagation varies with different laminate configurations

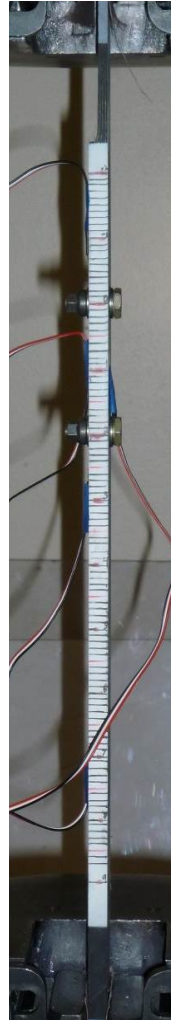
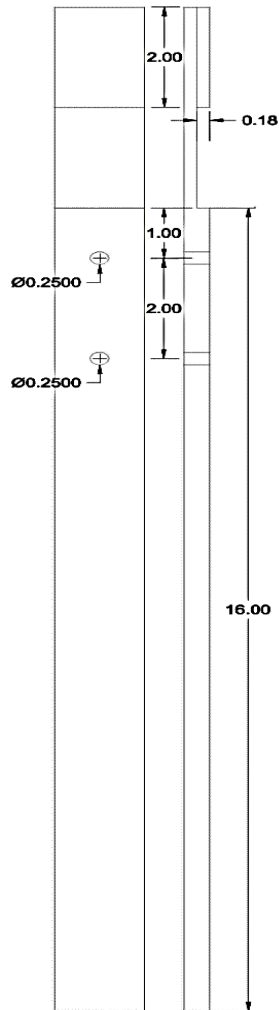
Crack Arrest Mechanism by Fastener



Background

- Motivation and Key Issues
 - Delamination is a critical damage type for laminated and bonded composite structures
 - Bolted joint design methodology is inefficient
- Objective
 - To understand the arrest process of delamination/disbond arrest features, particularly in novel configurations
 - To develop analysis tools for design and optimization
- Approach
 - Perform FEM analyses in ABAQUS with VCCT
 - Conduct sensitivity studies on fastener effectiveness
 - Conduct coupon-level experiments using novel specimens

Two Fastener Experimental Work



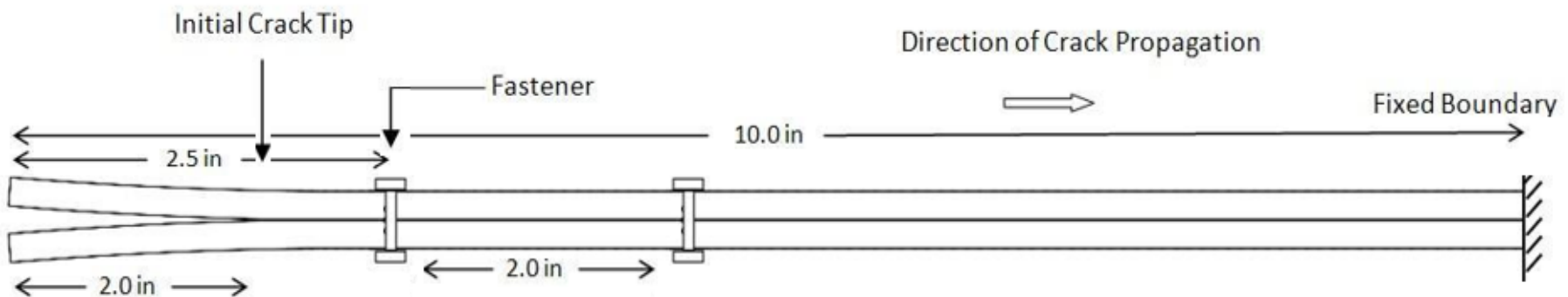
- T800S/3900-2B unidirectional pre-preg tape
- BMS 9-17 surplus unidirectional pre-preg tape
- 0.25 Inch titanium fasteners
- $(0/45/90/-45)_{3S}$
- Load rate 0.1 mm/min
- Crack tip tracked visually
- 0.1 in Scale

2-Plate Two-Fastener Finite Element Model

- Fastener flexibility (H. Huth, 1986) $C = \left(\frac{t_1 + t_2}{2d} \right)^a \frac{b}{n} \left(\frac{1}{t_1 E_1} + \frac{1}{nt_2 E_2} + \frac{1}{2t_1 E_3} + \frac{1}{2nt_2 E_3} \right)$
 - Thickness $t_1 = t_2 = 0.18$ in., diameter $d = 0.25$ in., $E_x =$ laminate stiffness
 - Single Lap, bolted graphite/epoxy joint, constants taken as; $a = 2/3$, $b = 4.2$, $n = 1$
- Fastener joint stiffness $k_{slide} = \frac{1}{C}$, Fastener tensile stiffness $k_{clamp} = \frac{AE}{(t_1 + t_2)}$
- Fracture parameters, $G_{IC} = 1.6$ lb/in, Nominal $G_{IIC} = G_{IIIC} = 14$ lb/in
Measured: 12 lb/in (BMS 8-276) 10 BMS 9-17)

- Power Law fracture criterion $\left(\frac{G_I}{G_{IC}} \right)^\alpha + \left(\frac{G_{II}}{G_{IIC}} \right)^\beta + \left(\frac{G_{III}}{G_{IIIC}} \right)^\delta \leq 1$
 $\alpha = \beta = \delta = 1$ linear mode mixture assumed

- Fixed boundary condition similar to test; grips not modeled
- Friction coefficient assumed to be fixed value or zero



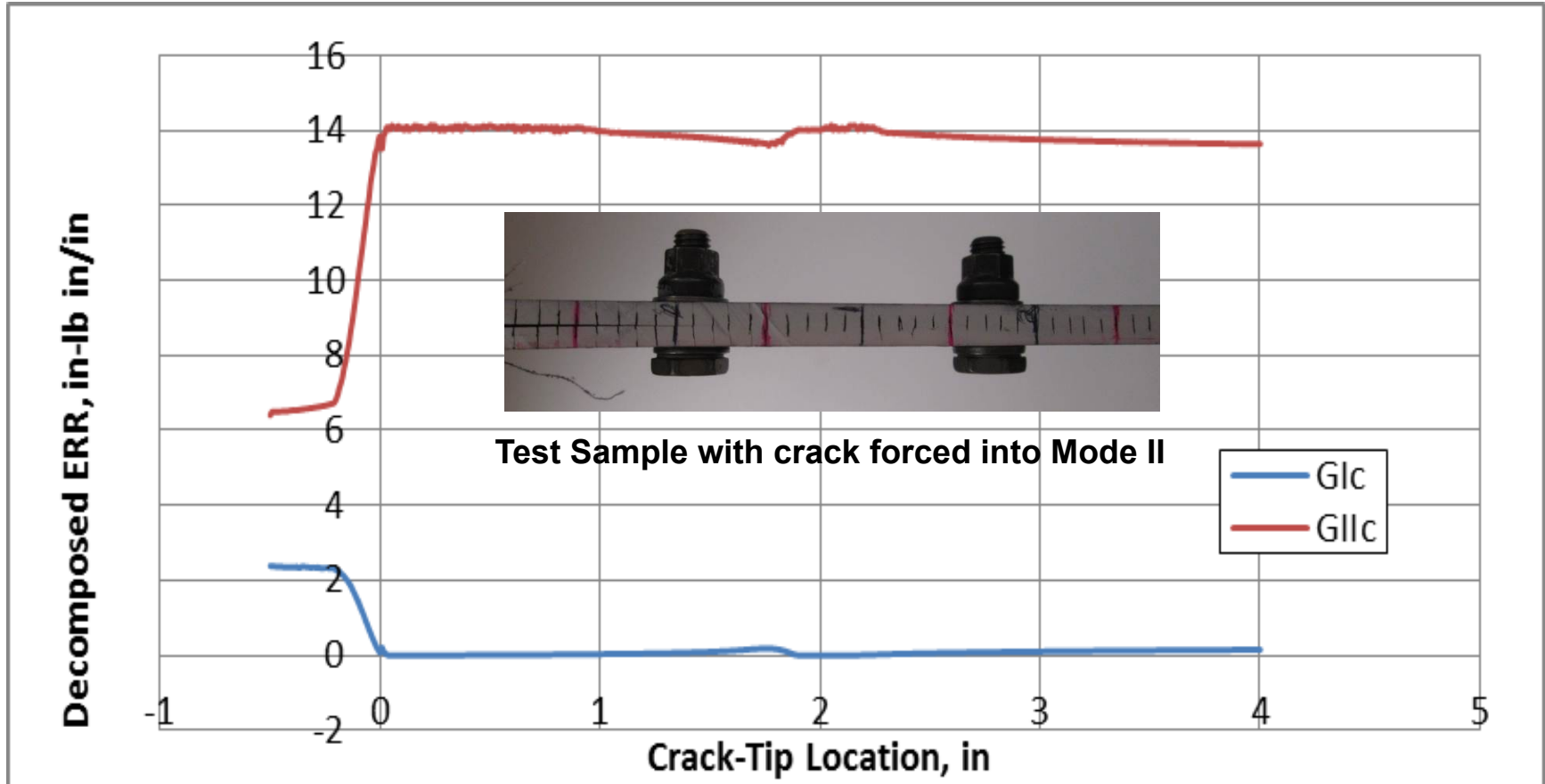
Clearance

- Typical ¼ inch bolt clearance 0.007-0.016 in.
 - Previous single and multiple fastener research utilized zero clearance (tight fitting hole)
- Bolt clearance and fracture toughness varied
 - Fastener stiffness set as zero over ± 0.007 -0.016 inch span
 - Fracture toughness varied from 5 to 14 lb/in to capture two different material systems

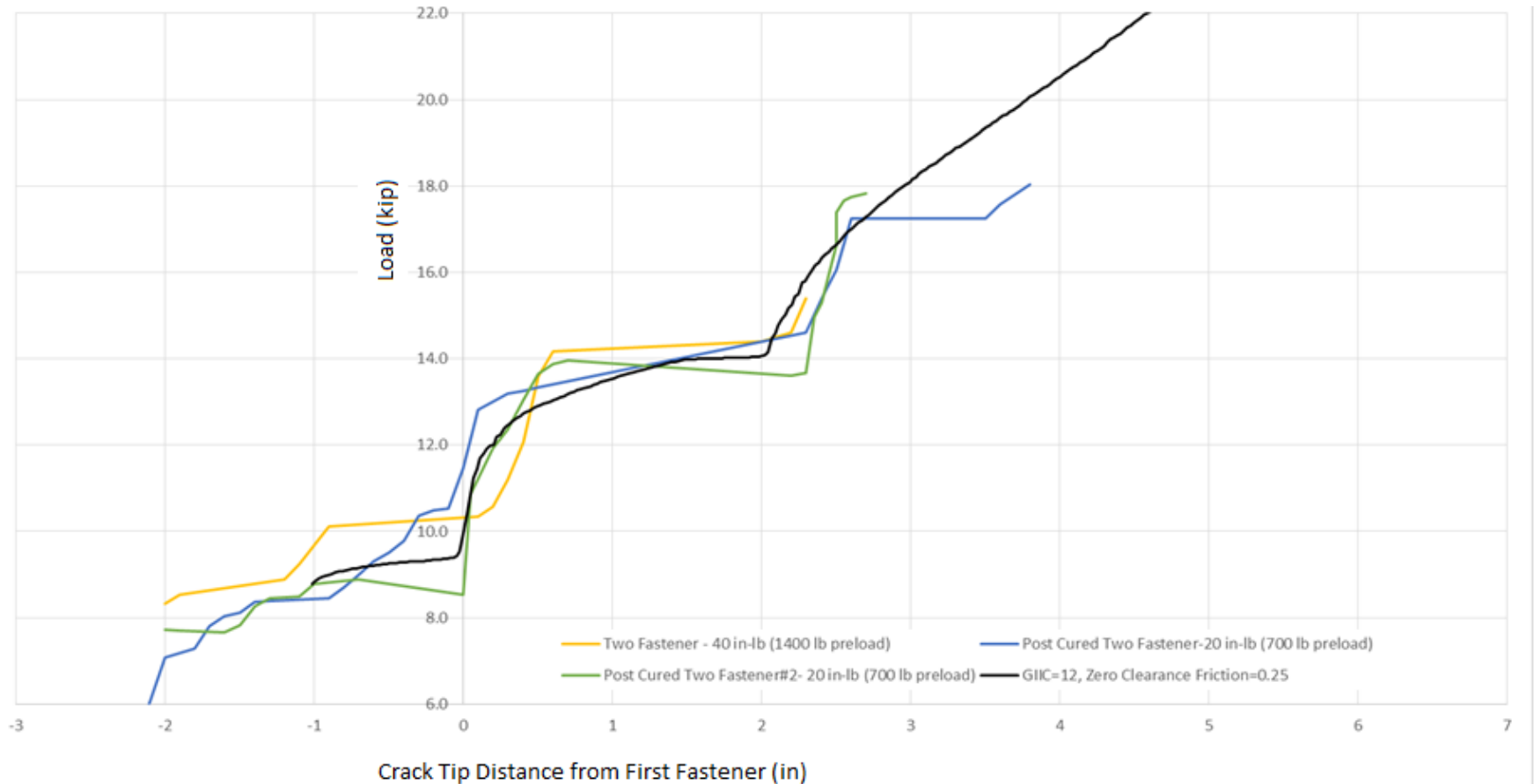
Results

- Delamination Arrest Mechanism
 - Mode I suppression
 - Propagation load increases as $G_{IIC} > G_{IC}$
 - Fastener flexibility is a major driver of arrest
 - Clearance greatly influences arrest capability by delaying fastener engagement
 - Crack-face friction slows propagation
- Limitations
 - Delamination can steer around the fastener's grip
 - Friction is poorly understood

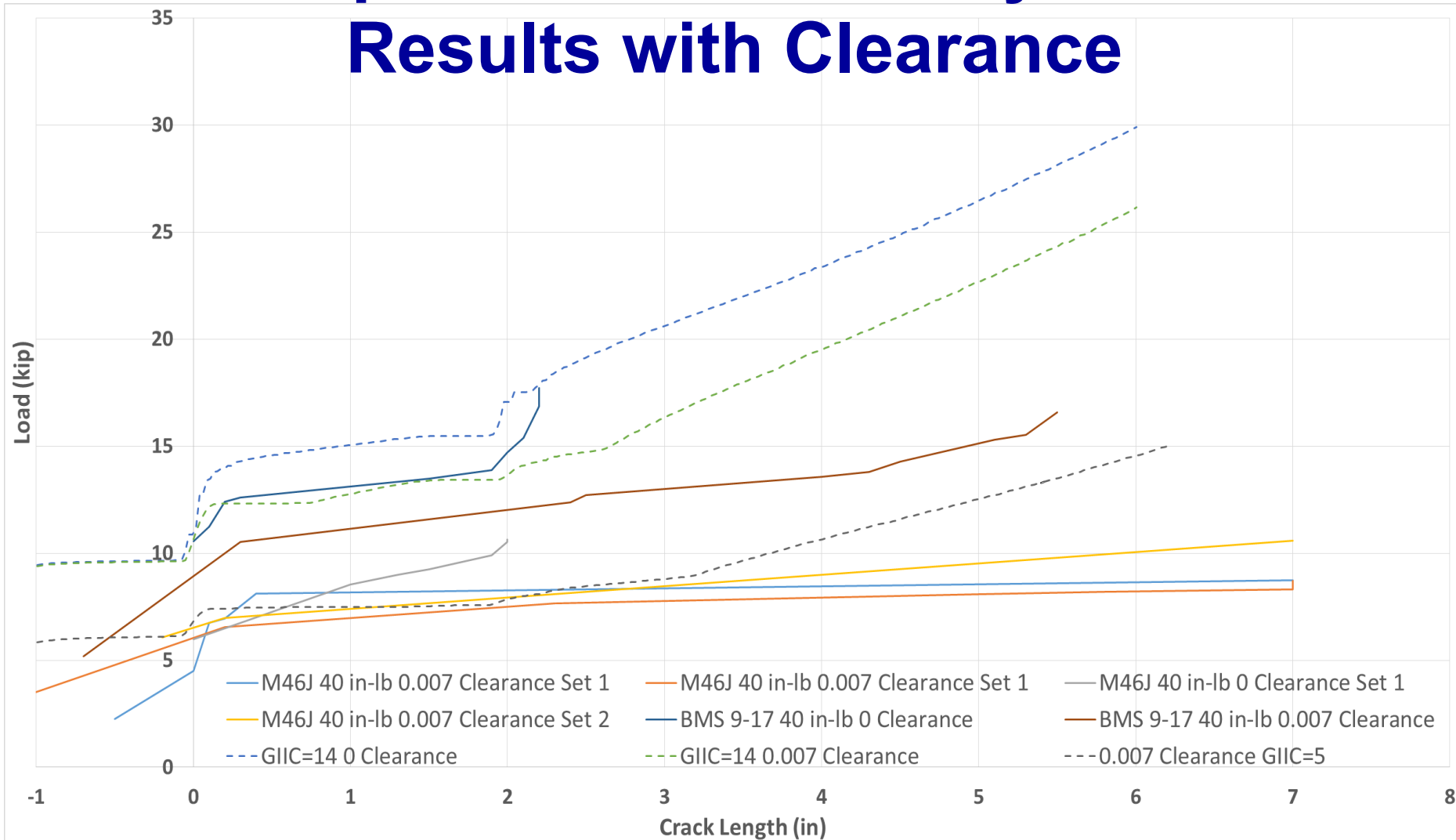
Two-Fastener Analysis of SERR vs. Crack Tip Location



Experimental vs. Analytical Results 0 Clearance



Experimental vs. Analytical Results with Clearance



Co-Cured Vs. Secondary Bonded

- All Test results shown are for cocured structures
 - Delamination resistance is governed by matrix properties
 - Structural adhesives typically have higher fracture toughness
- Previously delaminated samples re-bonded
 - Hysol EA9309 structural adhesive
 - Chosen for advertised shear properties
 - Secondary bonded structures failed prior to crack propagation
 - Crack driven off bondline and into laminate
 - Effective Mode II fracture toughness increased

Current Tasks

- Further Develop Analysis for Multiple Fasteners
 - Develop multi-dimensional modeling capability
 - Accurately model propagation with varying levels of detail
 - Conduct sensitivity studies
 - Fracture toughness shifts curve vertically
 - Optimize fastener pitch and pattern
- Fatigue Studies
 - Two fastener quasi-static modeling demonstrated
 - Fatigue predictions and performance unverified
 - Establish hybrid bolted/bonded joint performance in fatigue
 - Develop predictive capability based on pristine fatigue properties

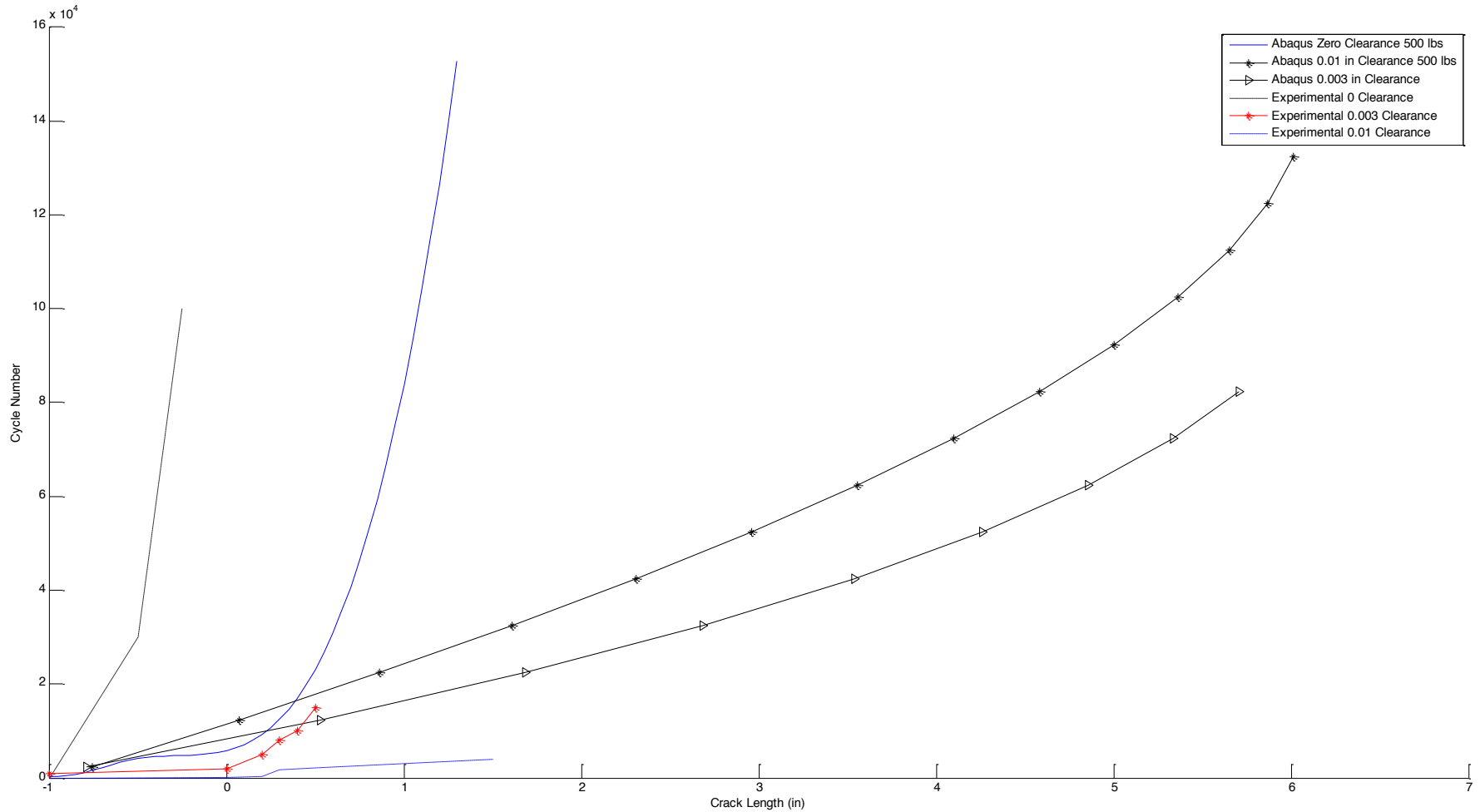
Fatigue Modeling

- Identical two dimensional model
 - Fatigue properties currently sourced from literature
 - Sinusoidal and triangular loading simulated
 - Zero and positive clearance simulated
 - Hole damage not currently modeled
- Dramatic fatigue life difference due to clearance
 - Consistent result both in tension-tension and tension-compression loading
- Hole damage may be critical factor
 - Even 0.001 in clearance results in lower fatigue life

Fatigue Testing

- Fastener has no effect on high cycle fatigue
 - No crack propagation to suppress
- Fastener hole treatment has significant effect on low cycle fatigue
 - Crack arrest capability greatly reduced by the inclusion of clearance
 - Poorly drilled clearance holes performed better than well drilled clearance holes
 - Effective clearance reduced
- Hole damage may be critical factor
 - Not visible on tested samples

Fatigue Results



Work in Progress

- Evaluate fatigue performance
 - Establish Da/Dn curves of unfastened structure
 - Establish relation between unfastened and fastened performance
- Establish boundaries of arrest capability
 - Asymmetric laminates experience greater crack growth
 - Can non-uniform fastener patterns be more efficient
- Investigate alternative or supplementary arrest features
 - Fastener tensile strength is excessive for configuration
 - Clearance minimization is key
 - Secondary or co-bonding may increase effective fracture toughness

Future Work

- Predict fatigue performance
 - Develop predictive abilities based on fatigue performance of coupon testing
 - Understand critical differences between static and fatigue performance of bolted bonded/joints
 - Hole damage not visible in quasi-static testing
 - Use knowledge developed from quasi-static work to predict fatigue performance of varying layup
- Predict limitations of fastener arrest
 - Analytically determine damage scenarios where multi-fastener arrest features are insufficient for full crack arrest

Future Work

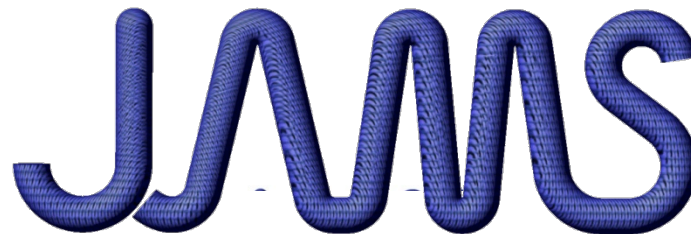
- Establish security of bond assisted joints
 - Demonstrate sufficient fastener quantity for debonds to be considered arrested
 - Reduce structural weight with load transfer through bondline as well as fasteners
- Develop alternative/supplementary arrest features
 - Can crack arrest fasteners be modified for improved arrest at lower weight?
 - Reduce/eliminate hole clearance without sacrificing manufacturability

Looking Forward

- Benefit to Aviation
 - Tackle a crucial weakness of laminate composite structures
 - Reduce risks (analysis, schedule/cost, re-design, etc.) associated with delamination/disbond mode of failure in large integrated structures
 - Enhance structural safety by building a methodology for designing fail-safe co-cured/bonded structures
- Future needs
 - Further fatigue testing to establish parameters
 - Initiation investigation of crack propagation through fastener arrays
 - Industry/regulatory agency inputs related to the application, design, and certification of this type of crack arrest feature

**Question and comments
are strongly encouraged.**

Thank you.



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